

**NATIONAL EXAMINATIONS**

**DECEMBER 2018**

**16-MEC-B3 ENERGY CONVERSION AND POWER GENERATION**

**Three hours duration**

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**Notes to Candidates**

1. This is a **Closed Book** examination.
2. Examination paper consists of two Sections. **Section A is Calculative** with five (5) questions and **Section B is Descriptive** with three (3) questions. Note that Question 5 is on two pages.
3. **Do four (4) questions (including all parts of each question) from Section A (Calculative) and two (2) questions from Section B (Descriptive).**
4. **Six questions constitute a complete paper.** (Total 60 marks).
5. **All questions are of equal value.** (Each 10 marks).
6. If doubt exists as to the interpretation of any question or in the event of missing data, the candidate is urged to submit, with the answer paper, a clear statement of any assumptions made.
7. If any initial parts of a multi-part question cannot be solved the remaining parts may be worked by making appropriate assumptions for the first parts from the technical data given.
8. **Read the entire question before commencing the calculations** and take note of any hints or recommendations given.
9. Candidates may use one of the approved **Casio** or **Sharp** calculators.
10. **Reference data** for particular questions are given on pages 10 to 12. **All pages used are to be returned with the answer booklet showing where data has been obtained.**
11. **Reference formulae and constants** are given on pages 13 to 16.
12. **Steam Tables** from "Thermodynamics and Heat Power" are provided.

## SECTION A CALCULATIVE QUESTIONS

*Show all steps in the calculations and state the units for all intermediate and final answers.*

### QUESTION 1 GAS TURBINE

A stationary gas turbine plant has the following technical and operating parameters:

Pressure ratio	$r$	=	12
Air flow rate	$M_{\text{air}}$	=	142 kg/s
Fuel flow rate	$M_{\text{fuel}}$	=	2.68 kg/s
Fuel heating value	CV	=	40 000 kJ/kg
Compressor efficiency	$\eta_{\text{comp}}$	=	90%
Turbine efficiency	$\eta_{\text{turb}}$	=	88%
Air inlet pressure	$p$	=	100 kPa
Air inlet temperature	$T$	=	15°C

- Sketch a T-s diagram of the system and identify by number all the points to be calculated. (1)
- Calculate the actual temperatures at the compressor exit, turbine inlet and turbine exhaust taking note of the changed gas conditions in the turbine (see note below). (7)
- Calculate the power output and efficiency of the gas turbine unit. (2)

Note: Take account of the change in mass flow rate and specific heat when calculating the conditions of the gas in the turbine. For the expansion of hot gas in a turbine use  $c_p = 1.148 \text{ kJ/kg}^\circ\text{C}$  and  $k = 1.333$ . For other processes use  $c_p$  and  $k$  for cold air as given in the table of constants on page 14.

[ 10 marks ]

**QUESTION 2 HEAT RECOVERY STEAM GENERATOR**

*This question assumes that the hot exhaust gas from the gas turbine in Question 1 is used to generate steam in a heat recovery steam generator which is then used to drive a steam turbine in a combined cycle plant. This question can be completed without having done Question 1 and without reference to it.*

Refer to the Examination Paper Attachments Page 10 **Steam Generator for Combined Cycle**. Return this page after completion of the required diagram for part (f).

A heat recovery steam generator provides steam for a steam turbine by utilising the heat from the exhaust gas of the gas turbine. This steam passing through the turbine increases the power output of the combined unit. The steam generator has the following terminal operating conditions:

Gas inlet temperature	T	=	560°C
Gas outlet temperature	T	=	130°C
Feedwater inlet temperature	T	=	30°C
Steam outlet temperature	T	=	540°C
Water and steam pressure	p	=	1.40 MPa
Gas mass flow rate	$M_{\text{gas}}$	=	125 kg/s (air plus fuel)

- (a) Sketch a temperature – path length diagram for both fluids over the length of the steam generator and identify the key temperature points by number. (1)
- (b) Determine the enthalpies of the water and steam at the key points. (2)
- (c) Calculate the mass flow rate of steam  $M_{\text{steam}}$ . (1)
- (d) Calculate the temperature difference between the hot and cold streams at the pinch point. (2)
- (e) Explain the significance of the pinch point in the design of a heat exchanger and how this affects plant performance. (2)
- (f) The figure on page 10 is purely diagrammatic. Below this figure sketch the actual arrangement of a heat recovery steam generator showing the economiser, evaporator, superheater and steam drum in their proper configuration. Label the sketch to correspond with the temperature – path length diagram in (a) above. (2)

[ 10 marks ]

**QUESTION 3 ENVIRONMENTAL IMPACT****PART I CARBON DIOXIDE EMISSIONS**

A coal fired power plant with an electrical output of 600 MW burns coal at a rate of 250 Mg/hour. The plant data and coal specifications are as follows:

Boiler efficiency	= 90%
Steam cycle efficiency	= 48%
Coal calorific value	= 30 MJ/kg
Coal ash content	= 10% (as received)
Coal carbon content	= 75% (as received)

- (a) Calculate the rate of coal consumption (Mg/hour). (3)
- (b) Calculate the rate of carbon dioxide release (Mg/hour). (2)

**PART II WATER CONSUMPTION**

Refer to the Examination Paper Attachments Page 11 **Cooling Tower Evaporative Loss**.

A coal fired power plant with an electrical output of 600 MW rejects 1500 MJ/s of heat to the atmosphere via a steam condenser and a wet natural draught cooling tower. Operating conditions are as follows:

Steam inlet (turbine exhaust) temperature	= 30°C
Cooling water inlet temperature	= 15°C
Cooling water outlet temperature	= 25°C
Ambient air temperature	= 30°C
Relative air humidity	= 40%

Determine the following:

- (a) Flow rate of cooling water ( $\text{m}^3/\text{s}$ ). (1)
- (b) Evaporative loss in cooling tower ( $\text{m}^3/\text{MJ}$  rejected) and ( $\text{m}^3/\text{s}$ ). (2)
- (c) Evaporative loss as a percentage of the cooling water flow rate. (1)
- (d) Consumption of water by cooling tower (L/kWh generated) (litres/unit generated). (1)

[ 10 marks ]

**QUESTION 4 STEAM PLANT DESIGN**

Consider the proposed construction of a new coal fired power plant where an estimate of the required resources (fuel and water) and costs are required. The basic parameters are as follows:

Capacity of power plant	500 MW MCR*
Capacity factor of plant**	0.80
Life expectancy of plant	40 years
Heat rate of whole plant***	10 550 kJ/kWh
Efficiency of boiler	90%
Capital cost of plant	2 500 \$/kW
Cost of capital repayments	10% of capital cost each year
Cost of administration and maintenance	8% of capital cost each year
Cost of coal	100 \$/Mg
Heating value of coal	24 000 kJ/kg
Capacity of one train car	50 Mg
Number of coal cars per train	60

Note: \*Maximum continuous rating

\*\*Capacity factor = actual electrical output / maximum possible electrical output

\*\*\*Heat rate is inversely proportional to thermal efficiency

Determine the following:

- Annual actual electrical production (kWh) and maximum possible electrical production (kWh). (2)
- Annual amount of coal required (Mg) and number of trains required per day. (3)
- Annual cost of coal (\$) and cost of coal per unit generated (cent/kWh). (1)
- Annual capital cost repayment (\$) and cost per unit generated (cent/kWh). (2)
- Annual administration and maintenance cost (\$) and cost per unit generated (cent/kWh). (1)
- Total power production cost per unit generated (cent/kWh). (1)

[ 10 marks ]

**QUESTION 5 COAL PULVERISER AIR FLOW**

Refer to the Examination Paper Attachments Page 12 **Vertical Spindle Roller Mill**.

This diagram shows the basic configuration and coal flow through a typical vertical spindle pulveriser. Coal enters at the top and air at the bottom. The air passing through the pulveriser entrains and dries the pulverised coal which, after classification to ensure proper particle size, leaves with the air at the top. Air entering at the bottom is tempered with cooler air to maintain proper temperatures with varying coal moisture content.

Consider a coal pulveriser of this type with a capacity of 18 MG/hour. The following boundary conditions exist:

Temperature of coal feed	30°C
Temperature of hot primary air from air heater	250°C
Temperature of cool tempering air bypassing air heater	40°C
Maximum permitted temperature of hot primary air	400°C
Temperature of pulverised coal-air mixture	70°C
Air-fuel ratio by mass	2

Note that an appropriate amount of cool tempering air is mixed with the hot primary air prior to entering the pulveriser so as to obtain the desired pulveriser outlet temperature. The pulveriser can be treated as a heat exchanger with the hot and cold air and coal and moisture streams exchanging heat with one another. Use specific heats as follows as well as steam tables.

Specific heat of air  $c_p = 1.0 \text{ kJ/kg}^\circ\text{C}$  (for ease of calculation)  
 Specific heat of dry coal (no surface moisture)  $c = 1.25 \text{ kJ/kg}^\circ\text{C}$

Prior to doing the calculations sketch the individual flow streams passing through the pulveriser and identify which streams lose and which gain heat.

***This question is continued on the next page***

**Question 5 continued.**

Determine the following when operating with coal having some surface moisture.

- (a) Mass flow rates of coal and air through the pulveriser as well as the moisture flow rate in terms of the coal flow rate (kg/s). (2)
- (b) Equations of heat gain and heat loss to quantify the primary and tempering air mass flow rates as well as coal flow rate through the pulveriser to give the specified air-fuel ratio and to define the moisture flow rate. (5)
- (c) By solving the equations above, calculate the maximum surface moisture on the coal that the pulveriser can handle and still operate under the specified normal conditions. Note that under these conditions (exit temperature 70°C) there would be no tempering air admitted. (2)
- (d) Should the coal have a lower moisture content than that determined in (c) above, state with reasons what would be done to maintain effective drying of the coal and maintaining normal operating conditions. (1)

*Hint: Assume a moisture mass flow rate of  $m$  and solve for  $m$ .*

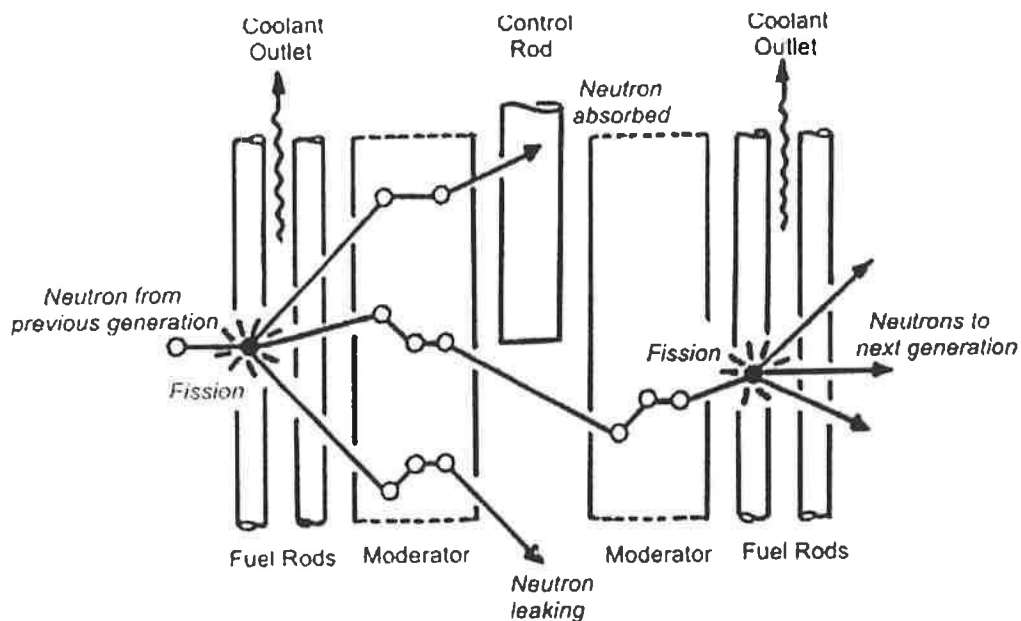
[10 marks]

## SECTION B DESCRIPTIVE QUESTIONS

*Descriptive questions should be answered in essay form, with sketches if appropriate, and taking approximately one full page for every 5 marks. A full page means approximately 250 words unless diagrams take the place of some words. The mark allocation for the individual parts will vary depending upon the extent of the answer.*

### QUESTION 6 NUCLEAR REACTOR PRINCIPLES

The following diagram shows the basic principles of the operation of a nuclear reactor.



- Explain the process illustrated. Write an equation to describe the process. Explain how and where energy is released in the process.
- Explain the functions of the four main components of the reactor. Explain why the reactor is configured as shown.
- Consider a typical CANDU OR PWR reactor system. Describe the material and construction or arrangement of each of the four main components of the selected reactor.

[ 10 marks ]



## QUESTION 7 COAL COMBUSTION

Consider the combustion of coal in a large coal fired boiler in a power plant.

- (a) Explain why the coal is ground to a fine power before combustion in the furnace.
- (b) Explain why excess air is required in the combustion process.
- (c) Explain what is meant by a proximate analysis and what is measured in such an analysis.
- (d) Explain what is meant by an ultimate analysis and what is measured in such an analysis.
- (e) Explain what is measured in a flue gas analysis. Clarify the difference between a wet gas analysis and a dry gas analysis. Explain why one or the other would be used in combustion calculations.

[ 10 marks ]

## QUESTION 8 ENERGY STORAGE

Electrical energy required by consumers must be produced instantaneously by power plants which must then operate with a constantly varying output. The demand for electricity is high during the day and low at night. It is therefore advantageous to store energy on a large scale in a different form.

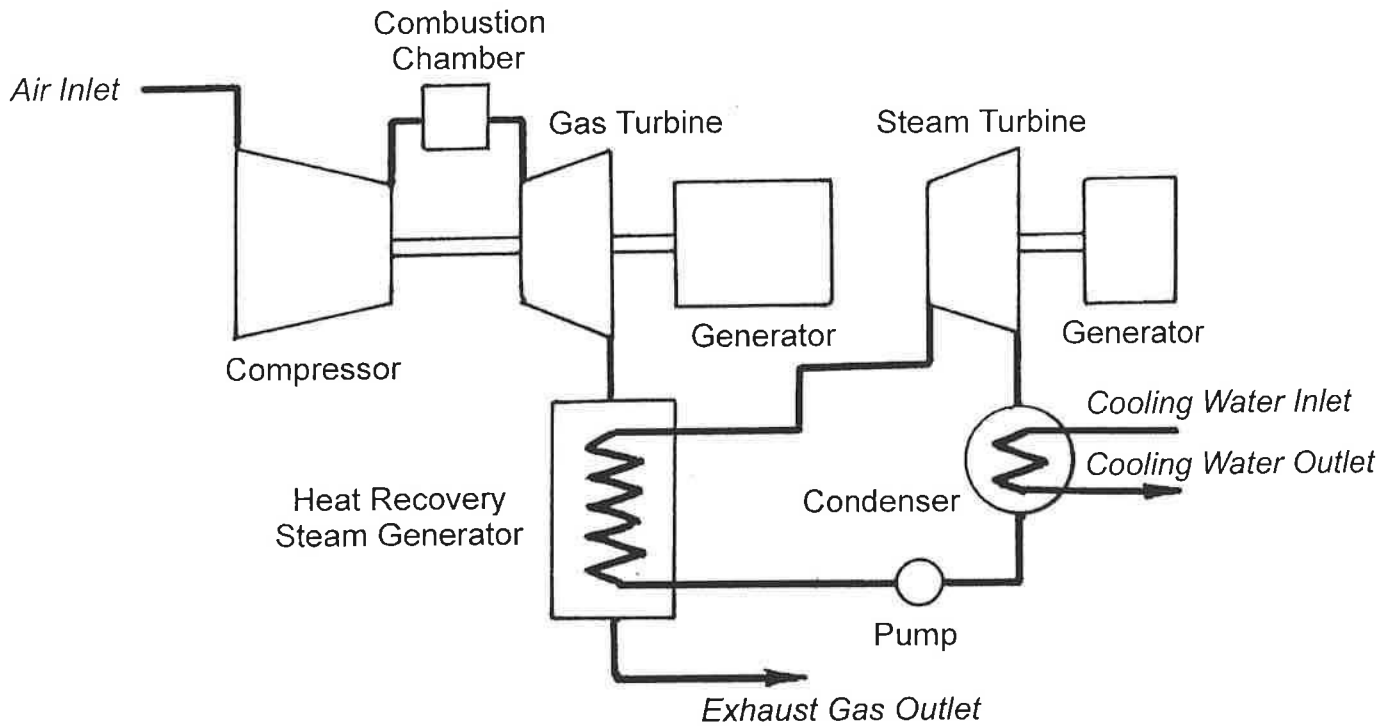
Describe TWO different methods for storing energy on a large scale for later use. Clarify in what form is this energy. Explain limitations to these methods of storage. Indicate likely levels of efficiency in the recovery of this energy. Explain what would determine the economic viability of these energy storage methods.

[ 10 marks ]

EXAMINATION PAPER ATTACHMENTS

NAME .....

QUESTION 2 STEAM GENERATOR FOR COMBINED CYCLE



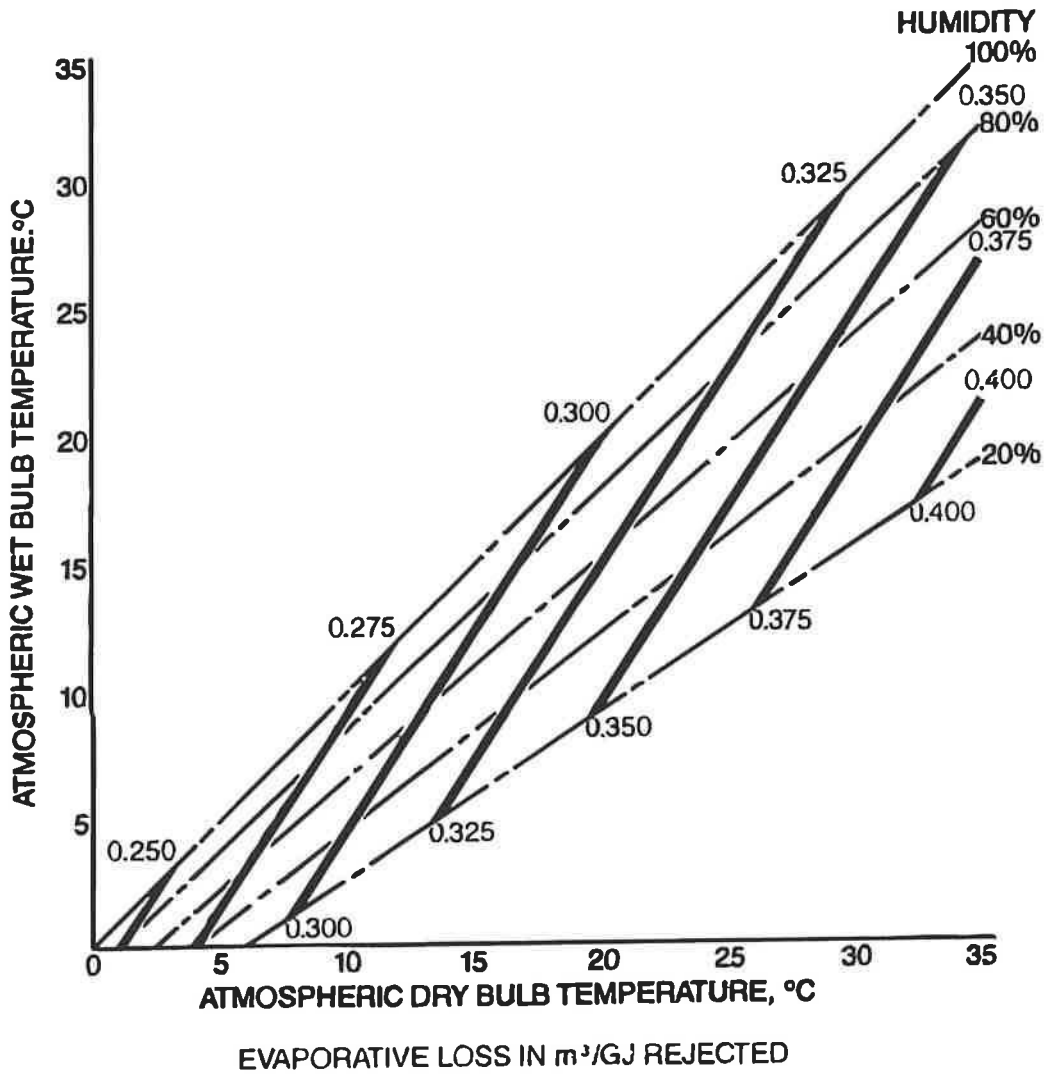
Part (f) Heat recovery steam generator configuration

Sketch the actual arrangement of a heat recovery steam generator showing the economiser, evaporator, superheater and steam drum in their proper configuration.

EXAMINATION PAPER ATTACHMENTS

NAME .....

QUESTION 3 PART II COOLING TOWER EVAPORATIVE LOSS

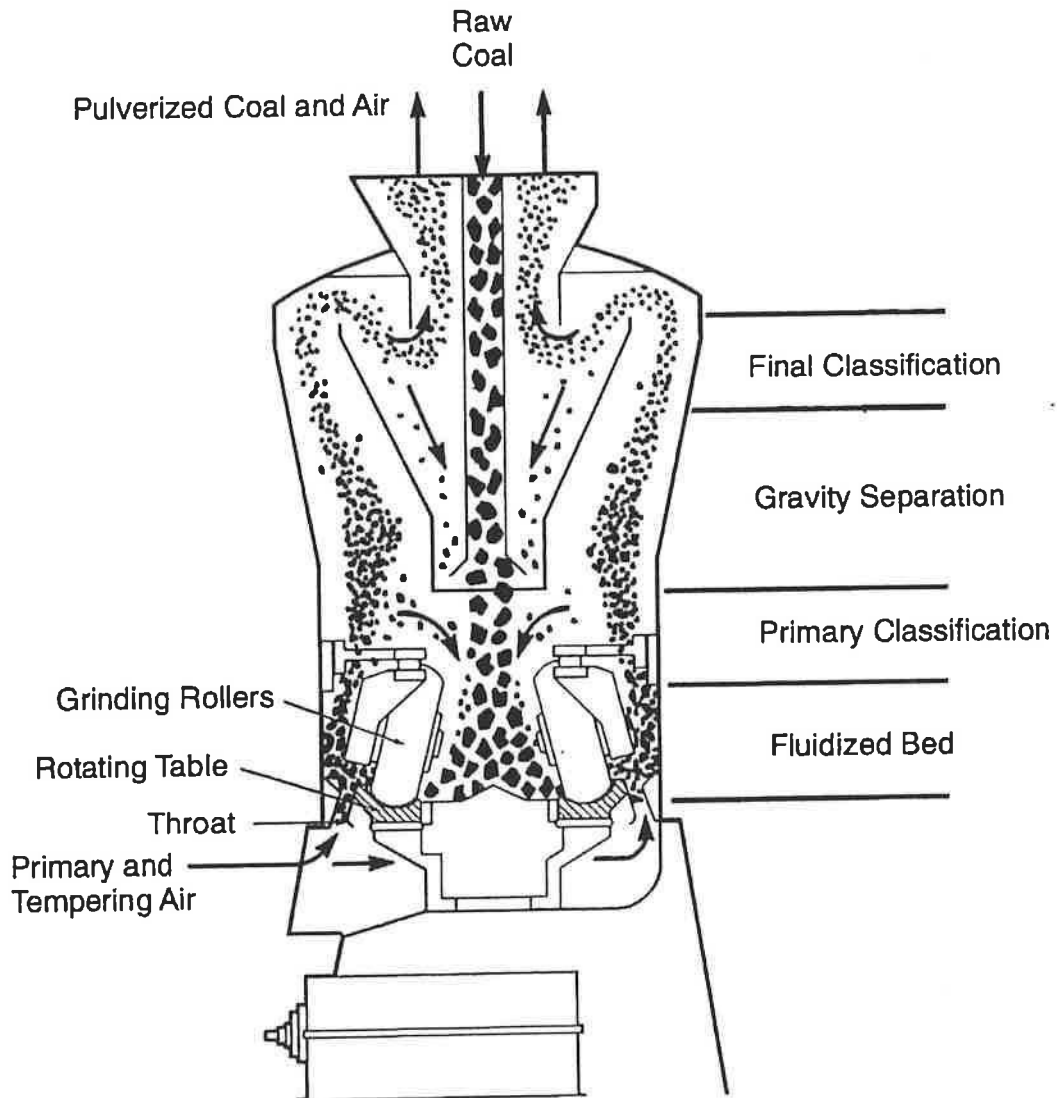


Evaporative loss from natural draught cooling towers

The chart is used to estimate the evaporative loss in m<sup>3</sup>/GJ of heat rejected.

## EXAMINATION PAPER ATTACHMENTS

### QUESTION 5 VERTICAL SPINDLE ROLLER MILL



**Vertical spindle roller mill (courtesy of Babcock & Wilcox)**

## EXAMINATION REFERENCE MATERIAL

### NOMENCLATURE FOR REFERENCE EQUATIONS (SI UNITS)

a	Acceleration	$m/s^2$
A	Flow area, Surface area	$m^2$
$c_p$	Specific heat at constant pressure	$J/kg^\circ C$
$c_v$	Specific heat at constant volume	$J/kg^\circ C$
D	Diameter	m
E	Energy	J
$E_f$	Energy release per fission of one atom	
h	Specific enthalpy	$J/kg$
H	Enthalpy	J
F	Force	N
g	Gravitational acceleration	$m/s^2$
k	Ratio of specific heats	
L	Length	m
m	Mass	kg
$\dot{m}$	Fractional mass flow rate	
M	Mass flow rate	$kg/s$
M	Molecular weight	
N	Number of nuclei	number/g
$N_A$	Avogadro's number	
$N_f$	Number of fissile nuclei	number/ $m^3$
n	Gas expansion index	
p	Pressure	Pa
P	Power	W
q	Heat transferred	$J/kg$
$q^*$	Heat release rate	$J/m^3$
Q	Heat	J
Q	Volume flow rate	$m^3/s$
R	Specific gas constant	$J/kg^\circ K$
$R_0$	Universal gas constant	$J/kg\text{-mole}^\circ K$
s	Specific entropy	$J/kg^\circ K$
S	Entropy	$J^\circ K$
t	Time	s
T	Temperature	$^\circ C$
T	Absolute temperature	$^\circ K$
u	Specific internal energy	$J/kg$
U	Internal energy	J
v	Specific volume	$m^3/kg$
V	Volume	$m^3$
V	Velocity	$m/s$
w	Specific work	$J/kg$
W	Work	J

x	Length	m
z	Elevation	m
$\gamma$	Fuel enrichment	
$\eta$	Efficiency	
$\phi$	Neutron flux	neutrons/m <sup>2</sup> s
$\sigma_f$	Cross section	barn
$\mu$	Dynamic viscosity	Ns/m <sup>2</sup>
$\nu$	Kinematic viscosity	m <sup>2</sup> /s
$\rho$	Density	kg/m <sup>3</sup>
$\tau$	Thrust	N
$\tau$	Torque	Nm
$\Omega$	Heat transfer rate	J/s

## CONSTANTS

For consistency in calculations the following constants should be used:

Gravitational Acceleration	$g = 9.81 \text{ m/s}$
Atmospheric Pressure	$p = 100 \text{ kPa}$
Universal Gas Constant	$R_o = 8.314 \text{ kJ/kg mole}^\circ\text{K}$
Density of Water	$\rho = 1000 \text{ kg/m}^3$
Specific Heat of Water	$c_p = 4.19 \text{ kJ/kg}^\circ\text{C}$
Specific Heat of Air	$c_p = 1.005 \text{ kJ/kg}^\circ\text{C}$
Specific Heat of Air	$c_v = 0.718 \text{ kJ/k}^\circ\text{C}$
Specific Heat of Helium	$c_p = 5.193 \text{ kJ/kg}^\circ\text{C}$
Specific Heat of Helium	$c_v = 3.116 \text{ kJ/kg}^\circ\text{C}$
Specific Gas Constant for Air	$R = 0.287 \text{ kJ/kg}^\circ\text{K}$
Avogadro's Number	$N_A = 0.602 \times 10^{24} \text{ atoms/mole}$
Nuclear Cross Section	$1 \text{ barn} = 10^{-28} \text{ m}^2$

## GENERAL REFERENCE EQUATIONS

### Ideal Gas Relationships

Gas Law:	$pv = RT$
Gas Law:	$pV = mRT$
Specific Heat at Constant Pressure:	$c_p = \Delta h/\Delta T$
Specific Heat at Constant Volume:	$c_v = \Delta u/\Delta T$
Gas Constant:	$R = c_p - c_v$
Specific Heat Ratio:	$k = c_p/c_v$

Constant Volume:	$T_1/T_2 = p_1/p_2$
Constant Pressure:	$T_1/T_2 = v_1/v_2$
Constant Temperature:	$p_1v_1 = p_2v_2$
Constant Entropy:	$p_1v_1^k = p_2v_2^k$
Isentropic Relations:	$p_1/p_2 = (v_2/v_1)^k = (T_1/T_2)^{k/(k-1)}$
	$T_1/T_2 = (v_2/v_1)^{k-1} = (p_1/p_2)^{(k-1)/k}$

### Work in Non-Flow Processes

Constant Pressure:	$w = p (v_2 - v_1)$
Constant Temperature:	$w = p_1v_1 \ln(v_2/v_1)$
Constant Entropy:	$w = (p_2v_2 - p_1v_1) / (1 - k)$
	$w = (T_2 - T_1) R / (1 - k)$

### Work in Flow Processes

Constant Temperature:	$w = p_1v_1 \ln(v_2/v_1)$
Constant Volume:	$w = (p_2 - p_1) v$
Constant Entropy:	$w = (p_1v_1 - p_2v_2) k / (k - 1)$

### Thermodynamics

First Law:	$dE = \delta Q - \delta W$
Enthalpy:	$h = u + pv$
Enthalpy Change	$\Delta h = \Delta u + \Delta(pv)$
Continuity:	$\rho VA = \text{constant}$
Flow Work:	$w = \Delta(pv)$
Energy Equation:	$zg + V^2/2 + u + pv + \Delta w + \Delta q = \text{constant}$
Entropy:	$\Delta s = q/T$ (reversible conditions)

### Fluid Mechanics

Continuity Equation:	$\rho_1V_1A_1 = \rho_2V_2A_2 = M$
Energy Equation:	$z_1g + V_1^2/2 + u_1 + p_1v_1 + W_{in} + Q_{in}$
	$= z_2g + V_2^2/2 + u_2 + p_2v_2 + W_{out} + Q_{out}$
Bernoulli's Equation:	$p_1/\rho g + z_1 + V_1^2/2g = p_2/\rho g + z_2 + V_2^2/2g$
Momentum Equation:	$F = p_1A_1 - p_2A_2 - \rho VA(V_2 - V_1)$
	(one dimensional)

### Internal Combustion Engines

Power Output	$P = 2\pi N\tau / 60$
Engine Capacity	$V_{total} = 1000 (\pi D^2/4) LN_{cylinders}$
Mean Effective Pressure	$MEP = \text{Work} / (V_1 - V_2)$

**Steam Turbines**

Nozzle Equation:  $h_1 - h_2 = (V_2^2 - V_1^2) / 2$   
 Work:  $W = [(V_1^2_{\text{absolute}} - V_2^2_{\text{absolute}}) + (V_2^2_{\text{relative}} - V_1^2_{\text{relative}})] / 2$

**Gas Turbines**

Isentropic Equation:  $(T_2/T_1) = (p_2/p_1)^{(k-1)/k}$   
 Enthalpy Change:  $h_1 - h_2 = c_p (T_1 - T_2)$  (ideal gas)  
 Nozzle Equation:  $h_1 - h_2 = (V_2^2 - V_1^2) / 2$

**Jet Propulsion**

Thrust:  $T = M (V_{\text{jet}} - V_{\text{aircraft}})$   
 Thrust Power:  $T V_{\text{aircraft}} = M (V_{\text{jet}} - V_{\text{aircraft}}) V_{\text{aircraft}}$   
 Jet Power:  $P = M (V_{\text{jet}}^2 - V_{\text{aircraft}}^2) / 2$   
 Propulsion Efficiency:  $\eta_p = 2V_{\text{aircraft}} / (V_{\text{jet}} + V_{\text{aircraft}})$

**Wind Turbines**

Maximum Ideal Power:  $P_{\text{max}} = 8 \rho A V_1^3 / 27$

**Nuclear Energy**

Number of nuclei per gram of material:  $N = N_A / M$   
 Number of fissile nuclei per cm<sup>3</sup> of material:  $N_f = \gamma (N_A / M) \rho$   
 Heat release rate in nuclear fuel:  $q^* = \phi N_f \sigma_f E_f$

**Cycle Efficiencies**

$\eta_{\text{cycle}} = W_{\text{out}} / q_{\text{in}} = W_{\text{out}} / Q_{\text{in}} = P_{\text{out}} / \Omega_{\text{in}}$   
 $\eta_{\text{Carnot}} = (T_{\text{hot}} - T_{\text{cold}}) / T_{\text{hot}}$   
 $\eta_{\text{Rankine}} = (\Delta h_{\text{turbine}} - \Delta h_{\text{pump}}) / \Delta h_{\text{boiler}}$   
 $\eta_{\text{Brayton}} = (\Delta T_{\text{turbine}} - \Delta T_{\text{Compressor}}) / \Delta T_{\text{combustion}}$

**Component Efficiencies**

$\eta_{\text{boiler}} = \Omega_{\text{out}} / \Omega_{\text{in}}$   
 $\eta_{\text{boiler}} = (\Omega_{\text{in}} / \Omega_{\text{lost}}) / \Omega_{\text{in}}$   
 $\eta_{\text{turbine}} = \Delta h_{\text{actual}} / \Delta h_{\text{isentropic}}$   
 $\eta_{\text{nozzle}} = \Delta h_{\text{actual}} / \Delta h_{\text{isentropic}}$   
 $\eta_{\text{gas turbine}} = \Delta T_{\text{actual}} / \Delta T_{\text{isentropic}}$   
 $\eta_{\text{pump}} = \Delta h_{\text{isentropic}} / \Delta h_{\text{actual}}$   
 $\eta_{\text{compressor}} = \Delta T_{\text{isentropic}} / \Delta T_{\text{actual}}$



# Thermodynamics and Heat Power

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SIXTH EDITION

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**Irving Granet, P.E.**

*late, Queensborough Community College of City University of New York*

**Maurice Bluestein, Ph.D.**

*Indiana University-Purdue University, Indianapolis*

PRENTICE HALL

*Upper Saddle River, New Jersey Columbus, Ohio*

TABLE A.1 (SI)  
Saturation: Temperature (Steam)

Temp. °C T	Press. kPa P	Specific Volume (m <sup>3</sup> /kg)		Internal Energy (kJ/kg)				Enthalpy (kJ/kg)				Entropy (kJ/kg · °K)	
		Sat. Liquid $v_f$	Sat. Vapor $v_g$	Sat. Liquid $u_f$	Evap. $u_{fg}$	Sat. Vapor $u_g$	Sat. Liquid $h_f$	Evap. $h_{fg}$	Sat. Vapor $h_g$	Sat. Liquid $s_f$	Evap. $s_{fg}$	Sat. Vapor $s_g$	
0.01	0.6113	0.001 000	206.14	.00	2375.3	2375.3	.01	2501.3	2501.4	.0000	9.1562	9.1562	9.1562
5	0.8721	0.001 000	147.12	20.97	2361.3	2382.3	20.98	2489.6	2510.6	.0761	8.9496	9.0257	8.9496
10	1.2276	0.001 000	106.38	42.00	2347.2	2389.2	42.01	2477.7	2519.8	.1510	8.7498	8.9008	8.7498
15	1.7051	0.001 001	77.93	62.99	2333.1	2396.1	62.99	2465.9	2528.9	.2245	8.5569	8.7814	8.5569
20	2.339	0.001 002	57.79	83.95	2319.0	2402.9	83.96	2454.1	2538.1	.2966	8.3706	8.6672	8.3706
25	3.169	0.001 003	43.36	104.88	2304.9	2409.8	104.89	2442.3	2547.2	.3674	8.1905	8.5580	8.1905
30	4.246	0.001 004	32.89	125.78	2290.8	2416.6	125.79	2430.5	2556.3	.4369	8.0164	8.4533	8.0164
35	5.628	0.001 006	25.22	146.67	2276.7	2423.4	146.68	2418.6	2565.3	.5053	7.8478	8.3531	7.8478
40	7.384	0.001 008	19.52	167.56	2262.6	2430.1	167.57	2406.7	2574.3	.5725	7.6845	8.2570	7.6845
45	9.593	0.001 010	15.26	188.44	2248.4	2436.8	188.45	2394.8	2583.2	.6387	7.5261	8.1648	7.5261
50	12.349	0.001 012	12.03	209.32	2234.2	2443.5	209.33	2382.7	2592.1	.7038	7.3725	8.0763	7.3725
55	15.758	0.001 015	9.568	230.21	2219.9	2450.1	230.23	2370.7	2600.9	.7679	7.2234	7.9913	7.2234
60	19.940	0.001 017	7.671	251.11	2205.5	2456.6	251.13	2358.5	2609.6	.8312	7.0784	7.9096	7.0784
65	25.03	0.001 020	6.197	272.02	2191.1	2463.1	272.06	2346.2	2618.3	.8935	6.9375	7.8310	6.9375
70	31.19	0.001 023	5.042	292.95	2176.6	2469.6	292.98	2333.8	2626.8	.9549	6.8004	7.7553	6.8004
75	38.58	0.001 026	4.131	313.90	2162.0	2475.9	313.93	2321.4	2635.3	1.0155	6.6669	7.6824	6.6669
80	47.39	0.001 029	3.407	334.86	2147.4	2482.2	334.91	2308.8	2643.7	1.0753	6.5369	7.6122	6.5369
85	57.83	0.001 033	2.828	355.84	2132.6	2488.4	355.90	2296.0	2651.9	1.1343	6.4102	7.5445	6.4102
90	70.14	0.001 036	2.361	376.85	2117.7	2494.5	376.92	2283.2	2660.1	1.1925	6.2866	7.4791	6.2866
95	84.55	0.001 040	1.982	397.88	2102.7	2500.6	397.96	2270.2	2668.1	1.2500	6.1659	7.4159	6.1659



TABLE A.1 (SI) (cont'd.)

Temp. °C T	Press. MPa P	Specific Volume (m <sup>3</sup> /kg)			Internal Energy (kJ/kg)			Enthalpy (kJ/kg)			Entropy (kJ/kg · °K)		
		Sat. Liquid $v_f$	Sat. Vapor $v_g$	Sat. Liquid $u_f$	Evap. $u_{fg}$	Sat. Vapor $u_g$	Sat. Liquid $h_f$	Evap. $h_{fg}$	Sat. Vapor $h_g$	Sat. Liquid $s_f$	Evap. $s_{fg}$	Sat. Vapor $s_g$	
250	3.973	0.001 251	0.050 13	1080.39	1522.0	2602.4	1085.36	1716.2	2801.5	2.7927	3.2802	6.0730	
255	4.319	0.001 263	0.045 98	1104.28	1496.7	2600.9	1109.73	1689.8	2799.5	2.8383	3.1992	6.0375	
260	4.688	0.001 276	0.042 21	1128.39	1470.6	2599.0	1134.37	1662.5	2796.9	2.8838	3.1181	6.0019	
265	5.081	0.001 289	0.038 77	1152.74	1443.9	2596.6	1159.28	1634.4	2793.6	2.9294	3.0368	5.9662	
270	5.499	0.001 302	0.035 64	1177.36	1416.3	2593.7	1184.51	1605.2	2789.7	2.9751	2.9551	5.9301	
275	5.942	0.001 317	0.032 79	1202.25	1387.9	2590.2	1210.07	1574.9	2785.0	3.0208	2.8730	5.8938	
280	6.412	0.001 332	0.030 17	1227.46	1358.7	2586.1	1235.99	1543.6	2779.6	3.0668	2.7903	5.8571	
285	6.909	0.001 348	0.027 77	1253.00	1328.4	2581.4	1262.31	1511.0	2773.3	3.1130	2.7070	5.8199	
290	7.436	0.001 366	0.025 57	1278.92	1297.1	2576.0	1289.07	1477.1	2766.2	3.1594	2.6227	5.7821	
295	7.993	0.001 384	0.023 54	1305.2	1264.7	2569.9	1316.3	1441.8	2758.1	3.2062	2.5375	5.7437	
300	8.581	0.001 404	0.021 67	1332.0	1231.0	2563.0	1344.0	1404.9	2749.0	3.2534	2.4511	5.7045	
305	9.202	0.001 425	0.019 948	1359.3	1195.9	2555.2	1372.4	1366.4	2738.7	3.3010	2.3633	5.6643	
310	9.856	0.001 447	0.018 350	1387.1	1159.4	2546.4	1401.3	1326.0	2727.3	3.3493	2.2737	5.6230	
315	10.547	0.001 472	0.016 867	1415.5	1121.1	2536.6	1431.0	1283.5	2714.5	3.3982	2.1821	5.5804	
320	11.274	0.001 499	0.015 488	1444.6	1080.9	2525.5	1461.5	1238.6	2700.1	3.4480	2.0882	5.5362	
330	12.845	0.001 561	0.012 996	1505.3	993.7	2498.9	1525.3	1140.6	2665.9	3.5507	1.8909	5.4417	
340	14.586	0.001 638	0.010 797	1570.3	894.3	2464.6	1594.2	1027.9	2622.0	3.6594	1.6763	5.3357	
350	16.513	0.001 740	0.008 813	1641.9	776.6	2418.4	1670.6	893.4	2563.9	3.7777	1.4335	5.2112	
360	18.651	0.001 893	0.006 945	1725.2	626.3	2351.5	1760.5	720.5	2481.0	3.9147	1.1379	5.0526	
370	21.03	0.002 213	0.004 925	1844.0	384.5	2228.5	1890.5	441.6	2332.1	4.1106	.6865	4.7971	
374.14	22.09	0.003 155	0.003 155	2029.6	0	2029.6	2099.3	0	2099.3	4.4298	0	4.4298	

TABLE A.2 (SI)  
Saturation Pressures (Steam)

Press. kPa <i>P</i>	Temp. °C <i>T</i>	Specific Volume (m <sup>3</sup> /kg)				Internal Energy (kJ/kg)				Enthalpy (kJ/kg)				Entropy (kJ/kg · °K)			
		Sat. Liquid	Sat. Vapor	Sat. Liquid	Sat. Vapor	Sat. Liquid	Sat. Vapor	Sat. Liquid	Sat. Vapor	Sat. Liquid	Sat. Vapor	Sat. Liquid	Sat. Vapor	Sat. Liquid	Sat. Vapor		
		<i>v<sub>f</sub></i>	<i>v<sub>g</sub></i>	<i>u<sub>f</sub></i>	<i>u<sub>g</sub></i>	<i>u<sub>fg</sub></i>	<i>u<sub>g</sub></i>	<i>h<sub>f</sub></i>	<i>h<sub>g</sub></i>	<i>h<sub>fg</sub></i>	<i>h<sub>g</sub></i>	<i>s<sub>f</sub></i>	<i>s<sub>g</sub></i>	<i>s<sub>f</sub></i>	<i>s<sub>g</sub></i>		
0.6113	0.01	0.001 000	206.14	.00	2375.3	2375.3	.01	2501.3	2501.3	.0000	9.1562	9.1562	0.0000	9.1562			
1.0	6.98	0.001 000	129.21	29.30	2355.7	2385.0	29.30	2484.9	2514.2	.1059	8.8697	8.9756	.1059	8.8697			
1.5	13.03	0.001 001	87.98	54.71	2338.6	2393.3	54.71	2470.6	2525.3	.1957	8.6322	8.8279	.1957	8.6322			
2.0	17.50	0.001 001	67.00	73.48	2326.0	2399.5	73.48	2460.0	2533.5	.2607	8.4629	8.7237	.2607	8.4629			
2.5	21.08	0.001 002	54.25	88.48	2315.9	2404.4	88.49	2451.6	2540.0	.3120	8.3311	8.6432	.3120	8.3311			
3.0	24.08	0.001 003	45.67	101.04	2307.5	2408.5	101.05	2444.5	2545.5	.3545	8.2231	8.5776	.3545	8.2231			
4.0	28.96	0.001 004	34.80	121.45	2293.7	2415.2	121.46	2432.9	2554.4	.4226	8.0520	8.4746	.4226	8.0520			
5.0	32.88	0.001 005	28.19	137.81	2282.7	2420.5	137.82	2423.7	2561.5	.4764	7.9187	8.3951	.4764	7.9187			
7.5	40.29	0.001 008	19.24	168.78	2261.7	2430.5	168.79	2406.0	2574.8	.5764	7.6750	8.2515	.5764	7.6750			
10	45.81	0.001 010	14.67	191.82	2246.1	2437.9	191.83	2392.8	2584.7	.6493	7.5009	8.1502	.6493	7.5009			
15	53.97	0.001 014	10.02	225.92	2222.8	2448.7	225.94	2373.1	2599.1	.7549	7.2536	8.0085	.7549	7.2536			
20	60.06	0.001 017	7.649	251.38	2205.4	2456.7	251.40	2358.3	2609.7	.8320	7.0766	7.9085	.8320	7.0766			
25	64.97	0.001 020	6.204	271.90	2191.2	2463.1	271.93	2346.3	2618.2	.8931	6.9383	7.8314	.8931	6.9383			
30	69.10	0.001 022	5.229	289.20	2179.2	2468.4	289.23	2336.1	2625.3	.9439	6.8247	7.7686	.9439	6.8247			
40	75.87	0.001 027	3.993	317.53	2159.5	2477.0	317.58	2319.2	2636.8	1.0259	6.6441	7.6700	1.0259	6.6441			
50	81.33	0.001 030	3.240	340.44	2143.4	2483.9	340.49	2305.4	2645.9	1.0910	6.5029	7.5939	1.0910	6.5029			
75	91.78	0.001 037	2.217	384.31	2112.4	2496.7	384.39	2278.6	2663.0	1.2130	6.2434	7.4564	1.2130	6.2434			
MPa																	
0.100	99.63	0.001 043	1.6940	417.36	2088.7	2506.1	417.46	2258.0	2675.5	1.3026	6.0568	7.3594	1.3026	6.0568			
0.125	105.99	0.001 048	1.3749	444.19	2069.3	2513.5	444.32	2241.0	2685.4	1.3740	5.9104	7.2844	1.3740	5.9104			
0.150	111.37	0.001 053	1.1593	466.94	2052.7	2519.7	467.11	2226.5	2693.6	1.4336	5.7897	7.2233	1.4336	5.7897			
0.175	116.06	0.001 057	1.0036	486.80	2038.1	2524.9	486.99	2213.6	2700.6	1.4849	5.6868	7.1717	1.4849	5.6868			
0.200	120.23	0.001 061	0.8857	504.49	2025.0	2529.5	504.70	2201.9	2706.7	1.5301	5.5970	7.1271	1.5301	5.5970			
0.225	124.00	0.001 064	0.7933	520.47	2013.1	2533.6	520.72	2191.3	2712.1	1.5706	5.5173	7.0878	1.5706	5.5173			

TABLE A.2 (SI) (cont'd.)

Press. MPa <i>P</i>	Temp. °C <i>T</i>	Specific Volume				Internal Energy				Enthalpy				Entropy			
		Liquid		Vapor		Liquid		Vapor		Liquid		Vapor		Liquid		Vapor	
		<i>v<sub>f</sub></i>	<i>v<sub>g</sub></i>	<i>u<sub>f</sub></i>	<i>u<sub>g</sub></i>	<i>u<sub>f</sub></i>	<i>u<sub>g</sub></i>	<i>h<sub>f</sub></i>	<i>h<sub>g</sub></i>	<i>h<sub>f</sub></i>	<i>h<sub>g</sub></i>	<i>s<sub>f</sub></i>	<i>s<sub>g</sub></i>	<i>s<sub>f</sub></i>	<i>s<sub>g</sub></i>		
0.250	127.44	0.001 067	0.7187	535.10	2002.1	2537.2	535.37	2181.5	2716.9	1.6072	5.4455	7.0527					
0.275	130.60	0.001 070	0.6573	548.59	1991.9	2540.5	548.89	2172.4	2721.3	1.6408	5.3801	7.0209					
0.300	133.55	0.001 073	0.6058	561.15	1982.4	2543.6	561.47	2163.8	2725.3	1.6718	5.3201	6.9919					
0.325	136.30	0.001 076	0.5620	572.90	1973.5	2546.4	573.25	2155.8	2729.0	1.7006	5.2646	6.9652					
0.350	138.88	0.001 079	0.5243	583.95	1965.0	2548.9	584.33	2148.1	2732.4	1.7275	5.2130	6.9405					
0.375	141.32	0.001 081	0.4914	594.40	1956.9	2551.3	594.81	2140.8	2735.6	1.7528	5.1647	6.9175					
0.40	143.63	0.001 084	0.4625	604.31	1949.3	2553.6	604.74	2133.8	2738.6	1.7766	5.1193	6.8959					
0.45	147.93	0.001 088	0.4140	622.77	1934.9	2557.6	623.25	2120.7	2743.9	1.8207	5.0359	6.8565					
0.50	151.86	0.001 093	0.3749	639.68	1921.6	2561.2	640.23	2108.5	2748.7	1.8607	4.9606	6.8213					
0.55	155.48	0.001 097	0.3427	655.32	1909.2	2564.5	655.93	2097.0	2753.0	1.8973	4.8920	6.7893					
0.60	158.85	0.001 101	0.3157	669.90	1897.5	2567.4	670.56	2086.3	2756.8	1.9312	4.8288	6.7600					
0.65	162.01	0.001 104	0.2927	683.56	1886.5	2570.1	684.28	2076.0	2760.3	1.9627	4.7703	6.7331					
0.70	164.97	0.001 108	0.2729	696.44	1876.1	2572.5	697.22	2066.3	2763.5	1.9922	4.7158	6.7080					
0.75	167.78	0.001 112	0.2556	708.64	1866.1	2574.7	709.47	2057.0	2766.4	2.0200	4.6647	6.6847					
0.80	170.43	0.001 115	0.2404	720.22	1856.6	2576.8	721.11	2048.0	2769.1	2.0462	4.6166	6.6628					
0.85	172.96	0.001 118	0.2270	731.27	1847.4	2578.7	732.22	2039.4	2771.6	2.0710	4.5711	6.6421					
0.90	175.38	0.001 121	0.2150	741.83	1838.6	2580.5	742.83	2031.1	2773.9	2.0946	4.5280	6.6226					
0.95	177.69	0.001 124	0.2042	751.95	1830.2	2582.1	753.02	2023.1	2776.1	2.1172	4.4869	6.6041					
1.00	179.91	0.001 127	0.194 44	761.68	1822.0	2583.6	762.81	2015.3	2778.1	2.1387	4.4478	6.5865					
1.10	184.09	0.001 133	0.177 53	780.09	1806.3	2586.4	781.34	2000.4	2781.7	2.1792	4.3744	6.5536					
1.20	187.99	0.001 139	0.163 33	797.29	1791.5	2588.8	798.65	1986.2	2784.8	2.2166	4.3067	6.5233					
1.30	191.64	0.001 144	0.151 25	813.44	1777.5	2591.0	814.93	1972.7	2787.6	2.2515	4.2438	6.4953					
1.40	195.07	0.001 149	0.140 84	828.70	1764.1	2592.8	830.30	1959.7	2790.0	2.2842	4.1850	6.4693					

TABLE A.2 (SI) (cont'd.)

Press. MPa <i>P</i>	Temp. °C <i>T</i>	Specific Volume (m <sup>3</sup> /kg)				Internal Energy (kJ/kg)				Enthalpy (kJ/kg)				Entropy (kJ/kg·°K)			
		Sat. Liquid		Sat. Vapor		Sat. Liquid		Sat. Vapor		Sat. Liquid		Sat. Vapor		Sat. Liquid		Sat. Vapor	
		<i>v<sub>f</sub></i>	<i>v<sub>g</sub></i>	<i>u<sub>f</sub></i>	<i>u<sub>g</sub></i>	<i>h<sub>f</sub></i>	<i>h<sub>g</sub></i>	<i>u<sub>f</sub></i>	<i>u<sub>g</sub></i>	<i>h<sub>f</sub></i>	<i>h<sub>g</sub></i>	<i>s<sub>f</sub></i>	<i>s<sub>g</sub></i>	<i>s<sub>f</sub></i>	<i>s<sub>g</sub></i>	<i>s<sub>f</sub></i>	<i>s<sub>g</sub></i>
1.50	198.32	0.001 154	0.131 77	843.16	1751.3	2594.5	844.89	1947.3	2792.2	2.3150	4.1298	6.4448					
1.75	205.76	0.001 166	0.113 49	876.46	1721.4	2597.8	878.50	1917.9	2796.4	2.3851	4.0044	6.3896					
2.00	212.42	0.001 177	0.099 63	906.44	1693.8	2600.3	908.79	1890.7	2799.5	2.4474	3.8935	6.3409					
2.25	218.45	0.001 187	0.088 75	933.83	1668.2	2602.0	936.49	1865.2	2801.7	2.5035	3.7937	6.2972					
2.5	223.99	0.001 197	0.079 98	959.11	1644.0	2603.1	962.11	1841.0	2803.1	2.5547	3.7028	6.2575					
3.0	233.90	0.001 217	0.066 68	1004.78	1599.3	2604.1	1008.42	1795.7	2804.2	2.6457	3.5412	6.1869					
3.5	242.60	0.001 235	0.057 07	1045.43	1558.3	2603.7	1049.75	1753.7	2803.4	2.7253	3.4000	6.1253					
4	250.40	0.001 252	0.049 78	1082.31	1520.0	2602.3	1087.31	1714.1	2801.4	2.7964	3.2737	6.0701					
5	263.99	0.001 286	0.039 44	1147.81	1449.3	2597.1	1154.23	1640.1	2794.3	2.9202	3.0532	5.9734					
6	275.64	0.001 319	0.032 44	1205.44	1384.3	2589.7	1213.35	1571.0	2784.3	3.0267	2.8625	5.8892					
7	285.88	0.001 351	0.027 37	1257.55	1323.0	2580.5	1267.00	1505.1	2772.1	3.1211	2.6922	5.8133					
8	295.06	0.001 384	0.023 52	1305.57	1264.2	2569.8	1316.64	1441.3	2758.0	3.2068	2.5364	5.7432					
9	303.40	0.001 418	0.020 48	1350.51	1207.3	2557.8	1363.26	1378.9	2742.1	3.2858	2.3915	5.6772					
10	311.06	0.001 452	0.018 026	1393.04	1151.4	2544.4	1407.56	1317.1	2724.7	3.3596	2.2544	5.6141					
11	318.15	0.001 489	0.015 987	1433.7	1096.0	2529.8	1450.1	1255.5	2705.6	3.4295	2.1233	5.5527					
12	324.75	0.001 527	0.014 263	1473.0	1040.7	2513.7	1491.3	1193.6	2684.9	3.4962	1.9962	5.4924					
13	330.93	0.001 567	0.012 780	1511.1	985.0	2496.1	1531.5	1130.7	2662.2	3.5606	1.8718	5.4323					
14	336.75	0.001 611	0.011 485	1548.6	928.2	2476.8	1571.1	1066.5	2637.6	3.6232	1.7485	5.3717					
15	342.24	0.001 658	0.010 337	1585.6	869.8	2455.5	1610.5	1000.0	2610.5	3.6848	1.6249	5.3098					
16	347.44	0.001 711	0.009 306	1622.7	809.0	2431.7	1650.1	930.6	2580.6	3.7461	1.4994	5.2455					
17	352.37	0.001 770	0.008 364	1660.2	744.8	2405.0	1690.3	856.9	2547.2	3.8079	1.3698	5.1777					
18	357.06	0.001 840	0.007 489	1698.9	675.4	2374.3	1732.0	777.1	2509.1	3.8715	1.2329	5.1044					
19	361.54	0.001 924	0.006 657	1739.9	598.1	2338.1	1776.5	688.0	2464.5	3.9388	1.0839	5.0228					
20	365.81	0.002 036	0.005 834	1785.6	507.5	2293.0	1826.3	583.4	2409.7	4.0139	.9130	4.9269					
21	369.89	0.002 207	0.004 952	1842.1	388.5	2230.6	1888.4	446.2	2334.6	4.1075	.6938	4.8013					
22	373.80	0.002 742	0.003 568	1961.9	125.2	2087.1	2022.2	143.4	2165.6	4.3110	.2216	4.5327					
22.09	374.14	0.003 155	0.003 155	2029.6	0	2029.6	2099.3	0	2099.3	4.4298	0	4.4298					









TABLE A.3 (SI) (cont'd.)

T	P = 1.60 MPa (201.41)			P = 1.80 MPa (207.15)			P = 2.00 MPa (212.42)					
	v	u	h	s	v	u	h	s	v	u	h	s
800	.3086	3658.3	4152.1	8.2808	.2742	3657.6	4151.2	8.2258	.2467	3657.0	4150.3	8.1765
900	.3377	3850.5	4390.8	8.4935	.3001	3849.9	4390.1	8.4386	.2700	3849.3	4389.4	8.3895
1000	.3668	4049.0	4635.8	8.6938	.3260	4048.5	4635.2	8.6391	.2933	4048.0	4634.6	8.5901
1100	.3958	4253.7	4887.0	8.8837	.3518	4253.2	4886.4	8.8290	.3166	4252.7	4885.9	8.7800
1200	.4248	4464.2	5143.9	9.0643	.3776	4463.7	5143.4	9.0096	.3398	4463.3	5142.9	8.9607
1300	.4538	4679.9	5406.0	9.2364	.4034	4679.5	5405.6	9.1818	.3631	4679.0	5405.1	9.1329
P = 2.50 MPa (223.99)												
Sat.	.079 98	2603.1	2803.1	6.2575	.066 68	2604.1	2804.2	6.1869	.057 07	2603.7	2803.4	6.1253
225	.080 27	2605.6	2806.3	6.2639								
250	.087 00	2662.6	2880.1	6.4085	.070 58	2644.0	2855.8	6.2872	.058 72	2623.7	2829.2	6.1749
300	.098 90	2761.6	3008.8	6.6438	.081 14	2750.1	2993.5	6.5390	.068 42	2738.0	2977.5	6.4461
350	.109 76	2851.9	3126.3	6.8403	.090 53	2843.7	3115.3	6.7428	.076 78	2835.3	3104.0	6.6579
400	.120 10	2939.1	3239.3	7.0148	.099 36	2932.8	3230.9	6.9212	.084 53	2926.4	3222.3	6.8405
450	.130 14	3025.5	3350.8	7.1746	.107 87	3020.4	3344.0	7.0834	.091 96	3015.3	3337.2	7.0052
500	.139 98	3112.1	3462.1	7.3234	.116 19	3108.0	3456.5	7.2338	.099 18	3103.0	3450.9	7.1572
600	.159 30	3288.0	3686.3	7.5960	.132 43	3285.0	3682.3	7.5085	.113 24	3282.1	3678.4	7.4339
700	.178 32	3468.7	3914.5	7.8435	.148 38	3466.5	3911.7	7.7571	.126 99	3464.3	3908.8	7.6837
800	.197 16	3655.3	4148.2	8.0720	.164 14	3653.5	4145.9	7.9862	.140 56	3651.8	4143.7	7.9134
900	.215 90	3847.9	4387.6	8.2853	.179 80	3846.5	4385.9	8.1999	.154 02	3845.0	4384.1	8.1276
1000	.2346	4046.7	4633.1	8.4861	.195 41	4045.4	4631.6	8.4009	.167 43	4044.1	4630.1	8.3288
1100	.2532	4251.5	4884.6	8.6762	.210 98	4250.3	4883.3	8.5912	.180 80	4249.2	4881.9	8.5192
1200	.2718	4462.1	5141.7	8.8569	.226 52	4460.9	5140.5	8.7720	.194 15	4459.8	5139.3	8.7000
1300	.2905	4677.8	5404.0	9.0291	.242 06	4676.6	5402.8	8.9442	.207 49	4675.5	5401.7	8.8723
P = 3.00 MPa (233.90)												





TABLE A.3 (SI) (cont'd.)

<i>T</i>	<i>P</i> = 15.0 MPa (342.24)					<i>P</i> = 17.5 MPa (354.75)					<i>P</i> = 20.0 MPa (365.81)				
	<i>v</i>	<i>u</i>	<i>h</i>	<i>s</i>		<i>v</i>	<i>u</i>	<i>h</i>	<i>s</i>		<i>v</i>	<i>u</i>	<i>h</i>	<i>s</i>	
Sat.	.010 337	2455.5	2610.5	5.3098		.007 920	2390.2	2528.8	5.1419		.005 834	2293.0	2409.7	4.9269	
350	.011 470	2520.4	2692.4	5.4421											
400	.015 649	2740.7	2975.5	5.8811		.012 447	2685.0	2902.9	5.7213		.009 942	2619.3	2818.1	5.5540	
450	.018 445	2879.5	3156.2	6.1404		.015 174	2844.2	3109.7	6.0184		.012 695	2806.2	3060.1	5.9017	
500	.020 80	2996.6	3308.6	6.3443		.017 358	2970.3	3274.1	6.2383		.014 768	2942.9	3238.2	6.1401	
550	.022 93	3104.7	3448.6	6.5199		.019 288	3083.9	3421.4	6.4230		.016 555	3062.4	3393.5	6.3348	
600	.024 91	3208.6	3582.3	6.6776		.021 06	3191.5	3560.1	6.5866		.018 178	3174.0	3537.6	6.5048	
650	.026 80	3310.3	3712.3	6.8224		.022 74	3296.0	3693.9	6.7357		.019 693	3281.4	3675.3	6.6582	
700	.028 61	3410.9	3840.1	6.9572		.024 34	3398.7	3824.6	6.8736		.021 13	3386.4	3809.0	6.7993	
800	.032 10	3610.9	4092.4	7.2040		.027 38	3601.8	4081.1	7.1244		.023 85	3592.7	4069.7	7.0544	
900	.035 46	3811.9	4343.8	7.4279		.030 31	3804.7	4335.1	7.3507		.026 45	3797.5	4326.4	7.2830	
1000	.038 75	4015.4	4596.6	7.6348		.033 16	4009.3	4589.5	7.5589		.028 97	4003.1	4582.5	7.4925	
1100	.042 00	4222.6	4852.6	7.8283		.035 97	4216.9	4846.4	7.7531		.031 45	4211.3	4840.2	7.6874	
1200	.045 23	4433.8	5112.3	8.0108		.038 76	4428.3	5106.6	7.9360		.033 91	4422.8	5101.0	7.8707	
1300	.048 45	4649.1	5376.0	8.1840		.041 54	4643.5	5370.5	8.1093		.036 36	4638.0	5365.1	8.0442	

<i>P</i> = 25.0 MPa					<i>P</i> = 30.0 MPa					<i>P</i> = 35.0 MPa				
375	.001 973 1	1798.7	1848.0	4.0320		.001 789 2	1737.8	1791.5	3.9305		.001 700 3	1702.9	1762.4	3.8722
400	.006 004	2430.1	2580.2	5.1418		.002 790	2067.4	2151.1	4.4728		.002 100	1914.1	1987.6	4.2126
425	.007 881	2609.2	2806.3	5.4723		.005 303	2455.1	2614.2	5.1504		.003 428	2253.4	2373.4	4.7747
450	.009 162	2720.7	2949.7	5.6744		.006 735	2619.3	2821.4	5.4424		.004 961	2498.7	2672.4	5.1962
500	.011 123	2884.3	3162.4	5.9592		.008 678	2820.7	3081.1	5.7905		.006 927	2751.9	2994.4	5.6282
550	.012 724	3017.5	3335.6	6.1765		.010 168	2970.3	3275.4	6.0342		.008 345	2921.0	3213.0	5.9026
600	.014 137	3137.9	3491.4	6.3602		.011 446	3100.5	3443.9	6.2331		.009 527	3062.0	3395.5	6.1179
650	.015 433	3251.6	3637.4	6.5229		.012 596	3221.0	3598.9	6.4058		.010 575	3189.8	3559.9	6.3010

TABLE A.3 (SI) (cont'd.)

T	P = 25.0 MPa			P = 30.0 MPa			P = 35.0 MPa					
	v	u	s	v	u	s	v	u	s			
700	.016 646	3361.3	3777.5	6.6707	.013 661	3335.8	3745.6	6.5606	.011 533	3309.8	3713.5	6.4631
800	.018 912	3574.3	4047.1	6.9345	.015 623	3555.5	4024.2	6.8332	.013 278	3536.7	4001.5	6.7450
900	.021 045	3783.0	4309.1	7.1680	.017 448	3768.5	4291.9	7.0718	.014 883	3754.0	4274.9	6.9886
1000	.023 10	3990.9	4568.5	7.3802	.019 196	3978.8	4554.7	7.2867	.016 410	3966.7	4541.1	7.2064
1100	.025 12	4200.2	4828.2	7.5765	.020 903	4189.2	4816.3	7.4845	.017 895	4178.3	4804.6	7.4057
1200	.027 11	4412.0	5089.9	7.7605	.022 589	4401.3	5079.0	7.6692	.019 360	4390.7	5068.3	7.5910
1300	.029 10	4626.9	5354.4	7.9342	.024 266	4616.0	5344.0	7.8432	.020 815	4605.1	5333.6	7.7653

T	P = 40.0 MPa			P = 50.0 MPa			P = 60.0 MPa					
	v	u	s	v	u	s	v	u	s			
375	.001 640 7	1677.1	1742.8	3.8290	.001 559 4	1638.6	1716.6	3.7639	.001 502 8	1609.4	1699.5	3.7141
400	.001 907 7	1854.6	1930.9	4.1135	.001 730 9	1788.1	1874.6	4.0031	.001 633 5	1745.4	1843.4	3.9318
425	.002 532	2096.9	2198.1	4.5029	.002 007	1959.7	2060.0	4.2734	.001 816 5	1892.7	2001.7	4.1626
450	.003 693	2365.1	2512.8	4.9459	.002 486	2159.6	2284.0	4.5884	.002 085	2053.9	2179.0	4.4121
500	.005 622	2678.4	2903.3	5.4700	.003 892	2525.5	2720.1	5.1726	.002 956	2390.6	2567.9	4.9321
550	.006 984	2869.7	3149.1	5.7785	.005 118	2763.6	3019.5	5.5485	.003 956	2658.8	2896.2	5.3441
600	.008 094	3022.6	3346.4	6.0114	.006 112	2942.0	3247.6	5.8178	.004 834	2861.1	3151.2	5.6452
650	.009 063	3158.0	3520.6	6.2054	.006 966	3093.5	3441.8	6.0342	.005 595	3028.8	3364.5	5.8829
700	.009 941	3283.6	3681.2	6.3750	.007 727	3230.5	3616.8	6.2189	.006 272	3177.2	3553.5	6.0824
800	.011 523	3517.8	3978.7	6.6662	.009 076	3479.8	3933.6	6.5290	.007 459	3441.5	3889.1	6.4109
900	.012 962	3739.4	4257.9	6.9150	.010 283	3710.3	4224.4	6.7882	.008 508	3681.0	4191.5	6.6805
1000	.014 324	3954.6	4527.6	7.1356	.011 411	3930.5	4501.1	7.0146	.009 480	3906.4	4475.2	6.9127
1100	.015 642	4167.4	4793.1	7.3364	.012 496	4145.7	4770.5	7.2184	.010 409	4124.1	4748.6	7.1195
1200	.016 940	4380.1	5057.7	7.5224	.013 561	4359.1	5037.2	7.4058	.011 317	4338.2	5017.2	7.3083
1300	.018 229	4594.3	5323.5	7.6969	.014 616	4572.8	5303.6	7.5808	.012 215	4551.4	5284.3	7.4837

TABLE 4

		Liquid											
		0				2.5 (223.99)				5.0 (263.99)			
<i>t</i>	<i>p</i> ( <i>t</i> Sat.) MPa	$10^3 v$	<i>u</i>	<i>h</i>	<i>s</i>	$10^3 v$	<i>u</i>	<i>h</i>	<i>s</i>	$10^3 v$	<i>u</i>	<i>h</i>	<i>s</i>
Sat.													
0		1.0002	-0.03	-0.03	-0.0001	0.9990	-0.00	2.50	-0.0000	0.9977	0.04	5.04	0.0001
20		1.0018	83.95	83.95	0.2966	1.0006	83.80	86.30	0.2961	0.9995	83.65	88.65	0.2956
40		1.0078	167.56	167.56	0.5725	1.0067	167.25	169.77	0.5715	1.0056	166.95	171.97	0.5705
60		1.0172	251.12	251.12	0.8312	1.0160	250.67	253.21	0.8298	1.0149	250.23	255.30	0.8285
80		1.1291	334.87	334.87	1.0753	1.0280	334.29	336.86	1.0737	1.0268	333.72	338.85	1.0720
100		1.0436	418.96	418.96	1.3069	1.0423	418.24	420.85	1.3050	1.0410	417.52	422.72	1.3030
120		1.0604	503.57	503.57	1.5278	1.0590	502.68	505.33	1.5255	1.0576	501.80	507.09	1.5233
140		1.0800	588.89	588.89	1.7395	1.0784	587.82	590.52	1.7369	1.0768	586.76	592.15	1.7343
160		1.1024	675.19	675.19	1.9434	1.1006	673.90	676.65	1.9404	1.0988	672.62	678.12	1.9375
180		1.1283	762.72	762.72	2.1410	1.1261	761.16	763.97	2.1375	1.1240	759.63	765.25	2.1341
200		1.1581	851.8	851.8	2.3334	1.1555	849.9	852.8	2.3294	1.1530	848.1	853.9	2.3255
210		1.1749	897.1	897.1	2.4281	1.1720	895.0	898.0	2.4238	1.1691	893.0	898.8	2.4195
220		1.1930	943.0	943.0	2.5221	1.1898	940.7	943.7	2.5174	1.1866	938.4	944.4	2.5128
230		1.2129	989.6	989.6	2.6157	1.2092	987.0	990.1	2.6105	1.2056	984.5	990.6	2.6055
240		1.2347	1037.1	1037.1	2.7091	1.2305	1034.2	1037.2	2.7034	1.2264	1031.4	1037.5	2.6979
250		1.2590	1085.6	1085.6	2.8027	1.2540	1082.3	1085.4	2.7964	1.2493	1079.1	1085.3	2.7902
260		1.2862	1135.4	1135.4	2.8970	1.2804	1131.6	1134.8	2.8898	1.2749	1127.9	1134.3	2.8830
270		1.3173	1186.8	1186.8	2.9926	1.3102	1182.4	1185.7	2.9844	1.3036	1178.2	1184.3	2.9766
280		1.3535	1240.4	1240.4	3.0904	1.3447	1235.1	1238.5	3.0808	1.3365	1230.2	1236.8	3.0717
290		1.3971	1297.0	1297.0	3.1918	1.3855	1290.5	1294.0	3.1801	1.3750	1284.4	1291.3	3.1693
300		1.4520	1358.1	1358.1	3.2992	1.4357	1349.6	1353.2	3.2843	1.4214	1341.9	1349.0	3.2708
310										1.4803	1404.1	1411.5	3.3789

FIGURE 5.11a Extract from subcooled table (SI units).



TABLE A.4 (SI)  
Properties of Compressed Liquid (Steam)

T	P = 5 MPa (263.99)					P = 10 MPa (311.06)					P = 15 MPa (342.24)				
	v	u	h	s		v	u	h	s		v	u	h	s	
Sat.	.001 285 9	1147.8	1154.2	2.9202		.001 452 4	1393.0	1407.6	3.3596		.001 658 1	1585.6	1610.5	3.6848	
0	.000 997 7	.04	5.04	.0001		.000 995 2	.09	10.04	.0002		.000 992 8	.15	15.05	.0004	
20	.000 999 5	83.65	88.65	.2956		.000 997 2	83.36	93.33	.2945		.000 995 0	83.06	97.99	.2934	
40	.001 005 6	166.95	171.97	.5705		.001 003 4	166.35	176.38	.5686		.001 001 3	165.76	180.78	.5666	
60	.001 014 9	250.23	255.30	.8285		.001 012 7	249.36	259.49	.8258		.001 010 5	248.51	263.67	.8232	
80	.001 026 8	333.72	338.85	1.0720		.001 024 5	332.59	342.83	1.0688		.001 022 2	331.48	346.81	1.0656	
100	.001 041 0	417.52	422.72	1.3030		.001 038 5	416.12	426.50	1.2992		.001 036 1	414.74	430.28	1.2955	
120	.001 057 6	501.80	507.09	1.5233		.001 054 9	500.08	510.64	1.5189		.001 052 2	498.40	514.19	1.5145	
140	.001 076 8	586.76	592.15	1.7343		.001 073 7	584.68	595.42	1.7292		.001 070 7	582.66	598.72	1.7242	
160	.001 098 8	672.62	678.12	1.9375		.001 095 3	670.13	681.08	1.9317		.001 091 8	667.71	684.09	1.9260	
180	.001 124 0	759.63	765.25	2.1341		.001 119 9	756.65	767.84	2.1275		.001 115 9	753.76	770.50	2.1210	
200	.001 153 0	848.1	853.9	2.3255		.001 148 0	844.5	856.0	2.3178		.001 143 3	841.0	858.2	2.3104	
220	.001 186 6	938.4	944.4	2.5128		.001 180 5	934.1	945.9	2.5039		.001 174 8	929.9	947.5	2.4953	
240	.001 226 4	1031.4	1037.5	2.6979		.001 218 7	1026.0	1038.1	2.6872		.001 211 4	1020.8	1039.0	2.6771	
260	.001 274 9	1127.9	1134.3	2.8830		.001 264 5	1121.1	1133.7	2.8699		.001 255 0	1114.6	1133.4	2.8576	
280						.001 321 6	1220.9	1234.1	3.0548		.001 308 4	1212.5	1232.1	3.0393	
300						.001 397 2	1328.4	1342.3	3.2469		.001 377 0	1316.6	1337.3	3.2260	
320											.001 472 4	1431.1	1453.2	3.4247	
340											.001 631 1	1567.5	1591.9	3.6546	

TABLE A.4 (SI) (cont'd.)

T	P = 20 MPa (365.81)					P = 30 MPa					P = 50 MPa				
	v	u	h	s		v	u	h	s		v	u	h	s	
Sat.	.002 036	1785.6	1826.3	4.0139		.000 985 6	.25	29.82	.0001		.000 976 6	.20	49.03	.0014	
0	.000 990 4	.19	20.01	.0004		.000 988 6	82.17	111.84	.2899		.000 980 4	81.00	130.02	.2848	
20	.000 992 8	82.77	102.62	.2923		.000 995 1	164.04	193.89	.5607		.000 987 2	161.86	211.21	.5527	
40	.000 999 2	165.17	185.16	.5646		.001 004 2	246.06	276.19	.8154		.000 996 2	242.98	292.79	.8052	
60	.001 008 4	247.68	267.85	.8206		.001 015 6	328.30	358.77	1.0561		.001 007 3	324.34	374.70	1.0440	
80	.001 019 9	330.40	350.80	1.0624		.001 029 0	410.78	441.66	1.2844		.001 020 1	405.88	456.89	1.2703	
100	.001 033 7	413.39	434.06	1.2917		.001 044 5	493.59	524.93	1.5018		.001 034 8	487.65	539.39	1.4857	
120	.001 049 6	496.76	517.76	1.5102		.001 062 1	576.88	608.75	1.7098		.001 051 5	569.77	622.35	1.6915	
140	.001 067 8	580.69	602.04	1.7193		.001 082 1	660.82	693.28	1.9096		.001 070 3	652.41	705.92	1.8891	
160	.001 088 5	665.35	687.12	1.9204		.001 104 7	745.59	778.73	2.1024		.001 091 2	735.69	790.25	2.0794	
180	.001 112 0	750.95	773.20	2.1147		.001 130 2	831.4	865.3	2.2893		.001 114 6	819.7	875.5	2.2634	
200	.001 138 8	837.7	860.5	2.3031		.001 159 0	918.3	953.1	2.4711		.001 140 8	904.7	961.7	2.4419	
220	.001 169 3	925.9	949.3	2.4870		.001 192 0	1006.9	1042.6	2.6490		.001 170 2	990.7	1049.2	2.6158	
240	.001 204 6	1016.0	1040.0	2.6674		.001 230 3	1097.4	1134.3	2.8243		.001 203 4	1078.1	1138.2	2.7860	
260	.001 246 2	1108.6	1133.5	2.8459		.001 275 5	1190.7	1229.0	2.9986		.001 241 5	1167.2	1229.3	2.9537	
280	.001 296 5	1204.7	1230.6	3.0248		.001 330 4	1287.9	1327.8	3.1741		.001 286 0	1258.7	1323.0	3.1200	
300	.001 359 6	1306.1	1333.3	3.2071		.001 399 7	1390.7	1432.7	3.3539		.001 338 8	1353.3	1420.2	3.2868	
320	.001 443 7	1415.7	1444.6	3.3979		.001 492 0	1501.7	1546.5	3.5426		.001 403 2	1452.0	1522.1	3.4557	
340	.001 568 4	1539.7	1571.0	3.6075		.001 626 5	1626.6	1675.4	3.7494		.001 483 8	1556.0	1630.2	3.6291	
360	.001 822 6	1702.8	1739.3	3.8772		.001 869 1	1781.4	1837.5	4.0012		.001 588 4	1667.2	1746.6	3.8101	
380															