

**NATIONAL EXAMINATIONS**

**May 2014**

**07-MEC-B3 ENERGY CONVERSION AND POWER GENERATION**

**Three hours duration**

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**Notes to Candidates**

1. This is a **Closed Book** examination.
2. Examination paper consists of two Sections. **Section A is Calculative** with four (4) questions and **Section B is Descriptive** with two (2) questions.
3. Note that Question 4 and Question 5 are each on two pages.
3. **Do three (3) questions (including all parts of each question) from Section A (Calculative) and one (1) question from Section B (Descriptive).**
4. **Four questions constitute a complete paper.** (Total 60 marks).
5. **All questions are of equal value.** (Each 15 marks).
6. If doubt exists as to the interpretation of any question or in the event of missing data, the candidate is urged to submit, with the answer paper, a clear statement of any assumptions made.
7. Candidates may use one of the approved **Casio** or **Sharp** calculators.
8. **Reference data** for particular questions are given on pages 10 to 17. **All pages used are to be returned with the answer booklet showing where data has been obtained.**
9. **Reference formulae and constants** are given on pages 18 to 21.
10. **Steam Tables** from "Thermodynamics and Heat Power" are provided.

**SECTION A CALCULATIVE SECTION****QUESTION 1 STEAM PLANT DESIGN**

Consider the proposed construction of a new coal fired power plant where an estimate of the required resources (fuel and water) and costs are required. The basic parameters are as follows:

Capacity of power plant	500 MW
Capacity factor of plant*	0.80
Life expectancy of plant	40 years
Heat rate of whole plant**	10 550 kJ/kWh
Efficiency of boiler	90%
Capital cost of plant	2 500 \$/kW
Cost of capital repayments	10% of capital cost each year
Cost of administration and maintenance	8% of capital cost each year
Cost of coal	100 \$/Mg
Heating value of coal	24 000 kJ/kg
Capacity of one train car	50 Mg
Number of coal cars per train	60

Note: \*Capacity factor = actual electrical output / maximum possible electrical output  
 \*\*Heat rate is inverse of thermal efficiency

Determine the following for a cooling water temperature rise of 10°C:

- Annual actual electrical production (kWh) and maximum possible electrical production (kWh).
- Annual amount of coal required (Mg) and number of trains required per day.
- Annual cost of coal (\$) and cost of coal per unit generated (cent/kWh).
- Annual capital cost repayment (\$) and cost per unit generated (cent/kWh).
- Annual administration and maintenance cost (\$) and cost per unit generated (cent/kWh).
- Total power production cost per unit generated (cent/kWh).
- Rate of heat rejection in cooling water from steam cycle at full load (kJ/s).
- Quantity of cooling water required at full load (m<sup>3</sup>/s).

[ 15 marks ]

**QUESTION 2 STEAM INJECTED GAS TURBINE**

Refer to the Examination Paper Attachments Page 10 **Steam Injected Gas Turbine**

A steam injected gas turbine system, as shown in the attachment, consists of an air compressor, a combustion chamber, a gas turbine, a once through heat recovery steam generator and a feedwater pump. Both the gas and steam systems are open cycles. The gas turbine can operate with or without steam injection. The operational parameters with steam injection are as follows:

Gas cycle pressure ratio	= 12
Air compressor air inlet temperature	= 30°C
Gas turbine gas inlet temperature	= 1000°C (without steam)
Steam generator steam outlet pressure	= 1.2 MPa
Steam generator steam outlet temperature	= 300°C
Steam generator water inlet temperature	= 30°C
Steam generator gas outlet temperature	= 160°C
Steam turbine exhaust pressure	= 0.1 MPa
Air compressor efficiency	= 0.80
Gas turbine efficiency	= 0.90 (with gas)
Gas turbine efficiency	= 0.90 (with steam)
Feedwater pump efficiency	= 1.00
Electrical generator efficiency	= 1.00
Fuel calorific value	= 42 000 kJ/kg

Assume cold air standard cycle (constant specific heats with  $k = 1.4$ ). For a gas mass flow of 100 kg/s calculate the following but see note below for acceptable assumptions:

- Mass flow rate of fuel (kg/s).
- Mass flow rate of steam (kg/s) during injection.
- Power output with steam injection (MW).
- Cycle efficiency with steam injection.

Note: Consider the gas and steam flows through the gas turbine and heat exchanger as separate streams with different properties and temperatures neglecting the transfer of heat between the two streams. It is not necessary to iterate to obtain more accurate answers. Use the point identifying numbers as shown on the accompanying diagram. For the thermodynamic calculations assume that the steam is injected at the place indicated.

[ 15 marks ]

### QUESTION 3 STEAM TURBINE OPERATIONAL CONDITIONS

Refer to the Examination Paper Attachments Page 11 **Mollier Chart**.

Steam is supplied to a turbine with an internal efficiency of 80% at 4 MPa (40 bar) and 400°C and exhausts at 0.005 MPa (0.05 bar). At full load the steam flow is 24 kg/s.

Note that the Mollier Chart is in bar (1 bar = 0.1 MPa).

Note that the steam flow under part load conditions is proportional to the inlet turbine pressure. Assume that for parts (a) to (c) the exhaust pressure remains constant.

- (a) Calculate the power developed by the turbine at full load.
- (b) Calculate the power developed by the turbine when the inlet steam is throttled to 1 MPa. Assume that the internal efficiency is unchanged.
- (c) Calculate the power developed by the turbine when the generator output is zero. Under these conditions the turbine power output is dissipated in friction in the bearings and windage in the generator. An inlet steam pressure of 0.1 MPa is required to maintain this condition. Assume that the internal efficiency has decreased to 70%.

Plot the processes on the Mollier Diagram on Page 11 but use Steam Tables to obtain improved accuracy in the calculations if necessary.

Return this page with the examination answer booklet.

Refer to the Examination Paper Attachments Page 12 **Condenser Conditions**. This shows the temperature profile in the condenser at full load. Assume now that the exhaust temperature does change with load and that the inlet cooling water temperature remains constant.

- (d) Using average temperature differences (not log mean) determine the temperature profiles for steam and water at part load conditions as defined in (b) above and plot these on the diagram.
- (e) Determine the condenser pressure at the temperature determined in (b) above.
- (f) Estimate (without further calculation) the condenser pressure for zero load conditions as defined in (c) above.

Return this page with the examination answer booklet.

[ 15 marks ]

## QUESTION 4 WIND AND WATER POWER

### PART I WIND TURBINE

Refer to the Examination Paper Attachments Page 13 **Vestas Wind Turbine** and Page 14 **Wind Power Efficiencies**.

The tables and graphs give information for the Vestas V80 1.8 MW Wind Turbine, as well as efficiencies, for ideal and actual wind turbines. Determine the following for a wind speed of 10 m/s and compare with the specified output.

- (a) Kinetic energy and potential power available in the wind passing through a flow area equivalent to the area swept out by the rotor at the wind speed given above.
- (b) Maximum theoretical power and efficiency that can be obtained based on energy and momentum theoretical equations for any wind speed.
- (c) Ideal efficiency and power based on ratio of blade tip speed to wind speed as given (from graph of efficiency on page 14).
- (d) Actual efficiency and power based on ratio of blade tip speed to wind speed as given (from graph of efficiency on Page 14).
- (e) Actual power output at the given wind speed as specified by the manufacturer (from graph on page 13).

(5 marks)

***Question 4 continued on next page . . . . .***

**QUESTION 4 (Continued)****PART II. VAN DER KLOOF HYDRO POWER STATION**

Refer to the Examination Paper Attachments Page 15 **Van der Kloof Hydro Power Station**. This shows a cross-sectional drawing of the plant close to the main wall of the dam. It has the following design parameters:

Reservoir water level	1170.5 m	(point 1)
Turbine inlet elevation	1091.5 m	(point 2)
Turbine outlet elevation	1086.5 m	(point 3)
Tailrace water level	1094.7 m	(point 4)
Penstock (inlet) diameter	7.0 m	(point 2)
Draft Tube (outlet) diameter	5.0 m	(point 3)
Turbine inlet pressure	700 kPa gauge	(point 2)
Turbine outlet pressure	65 kPa gauge	(point 3)
Water volume flow rate	200 m <sup>3</sup> /s	

Calculate the following:

- (a) (i) The water velocity at the turbine inlet (point 2) and at the turbine outlet (point 3).
- (ii) The head loss in the intake pipe (penstock) (between point 1 and point 2) and in the outlet pipe (draft tube) and tailrace (between point 3 and point 4).
- (b) (i) The potential power output of the whole plant based on elevation difference (between point 1 and point 4) and flow.
- (ii) The hydraulic power developed in the turbine based on inlet and outlet conditions (between point 2 and point 3) assuming no losses within the turbine.

(5)

(5)

( 10 marks )

[ 15 marks ]

## SECTION B DESCRIPTIVE SECTION

***Descriptive questions [ parts of Question 5 and all of Question 6 ] should be answered in essay form with sketches, if appropriate, and taking approximately one full page for every 5 marks. A full page means approximately 250 words unless diagrams take the place of some words.***

***While each part of each question specifies several aspects, more emphasis may be put on one or more aspects and less on others provided an overall comprehensive answer is given as required by the above.***

### QUESTION 5 GRAPHICAL REPRESENTATION

#### PART I T-s DIAGRAMS

Refer to the Examination Paper Attachments Page 16 T-s and p-V Diagrams.

- (a) On the diagrams given draw T-s and p-V Diagrams for the following thermodynamic power cycles:
- (i) Rankine cycle (saturated conditions)
  - (ii) Rankine cycle with superheating
  - (iii) Rankine cycle with superheating and reheating
  - (iv) Brayton cycle
  - (v) Otto cycle
  - (vi) Diesel cycle

*Return this page with the examination answer booklet.*

- (c) Explain why T-s diagrams are traditionally used to show certain cycles and p-V diagrams used to show other cycles. Clarify what parameter is the same for both types of diagrams.
- (d) Explain the advantages of superheating and reheating in the Rankine cycle.

( 10 marks )

***Question 5 continued on next page . . . . .***

**QUESTION 5 (Continued)**

**PART II LOAD SCHEDULING**

Refer to the Examination Paper Attachments Page 17 **Daily Load Curve**. This curve shows the daily power demand on a typical power system with the maximum demand being somewhat less than the total installed capacity of the system.

Consider a power utility having the following types of power generating equipment with their respective capacities given as a percentage of the total installed capacity:

- Fossil fuel plant                      30%
- Nuclear plant                            30%
- Gas turbines                              10%
- Solar energy                              5%
- Wind turbines                            10%
- Hydro turbines                          5%
- Pumped storage hydro                10%

- (a) Show by blocking in under the curve on the diagram when and to what degree these generating units should be operated assuming a normal sunny day with no wind.
- (b) Considering operating costs clarify which generating equipment would be reduced in load if wind power was available.
- (c) Considering operating costs clarify which generating equipment would be increased in load if the peak demand reached 90% of installed capacity.

Return this page with the examination answer booklet.

( 5 marks )

[ 15 marks ]



## QUESTION 6 ENERGY CONSIDERATIONS

### PART I FOSSIL FUEL CHARACTERISTICS

- (a) Explain the difference between the higher heating value (HHV or HCV) and the lower heating value (LHV or LCV) of a fossil fuel.
- (b) With regard to coal state what constitutes a Proximate Analysis and what constitutes an Ultimate Analysis. Clarify the usefulness of each.
- (c) Compare a high grade coal such as anthracite which is nearly pure carbon with natural gas which is primarily methane. State which one will give lower carbon dioxide emissions for the same energy release. Explain in detail what parameters need to be known to quantify this and how it would be proven that one or the other would give reduced emissions.

( 10 marks )

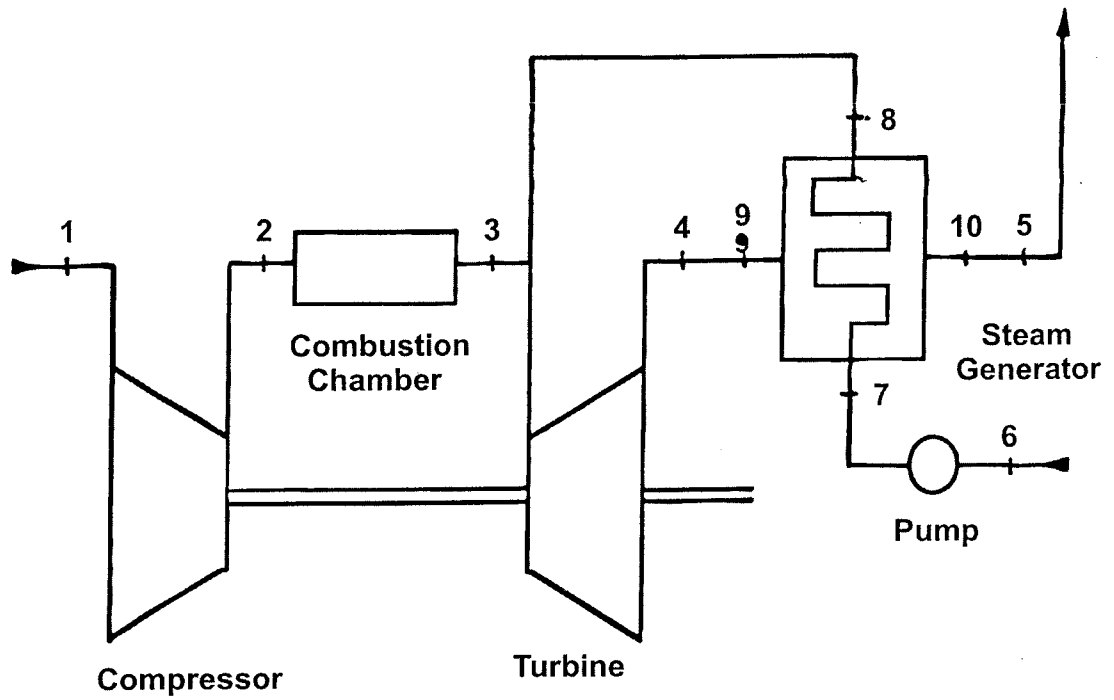
### PART II RENEWABLE ENERGY EFFICIENCIES

- (a) Hydro turbines can theoretically convert all (100%) the potential energy in the water into electrical energy but wind turbines can only theoretically convert a little more than half (59%) of the kinetic energy of the wind into electrical energy. Explain why this is the case.
- (b) Solar power plants can only convert part (approximately 20%) of the incoming solar radiation into electrical energy. Compare solar voltaic (solar photovoltaic panels) and solar thermal (reflecting collectors and steam cycle) systems and explain where and why the losses which limit efficiency occur.

( 5 marks )

[ 15 marks ]

QUESTION 2 STEAM INJECTED GAS TURBINE

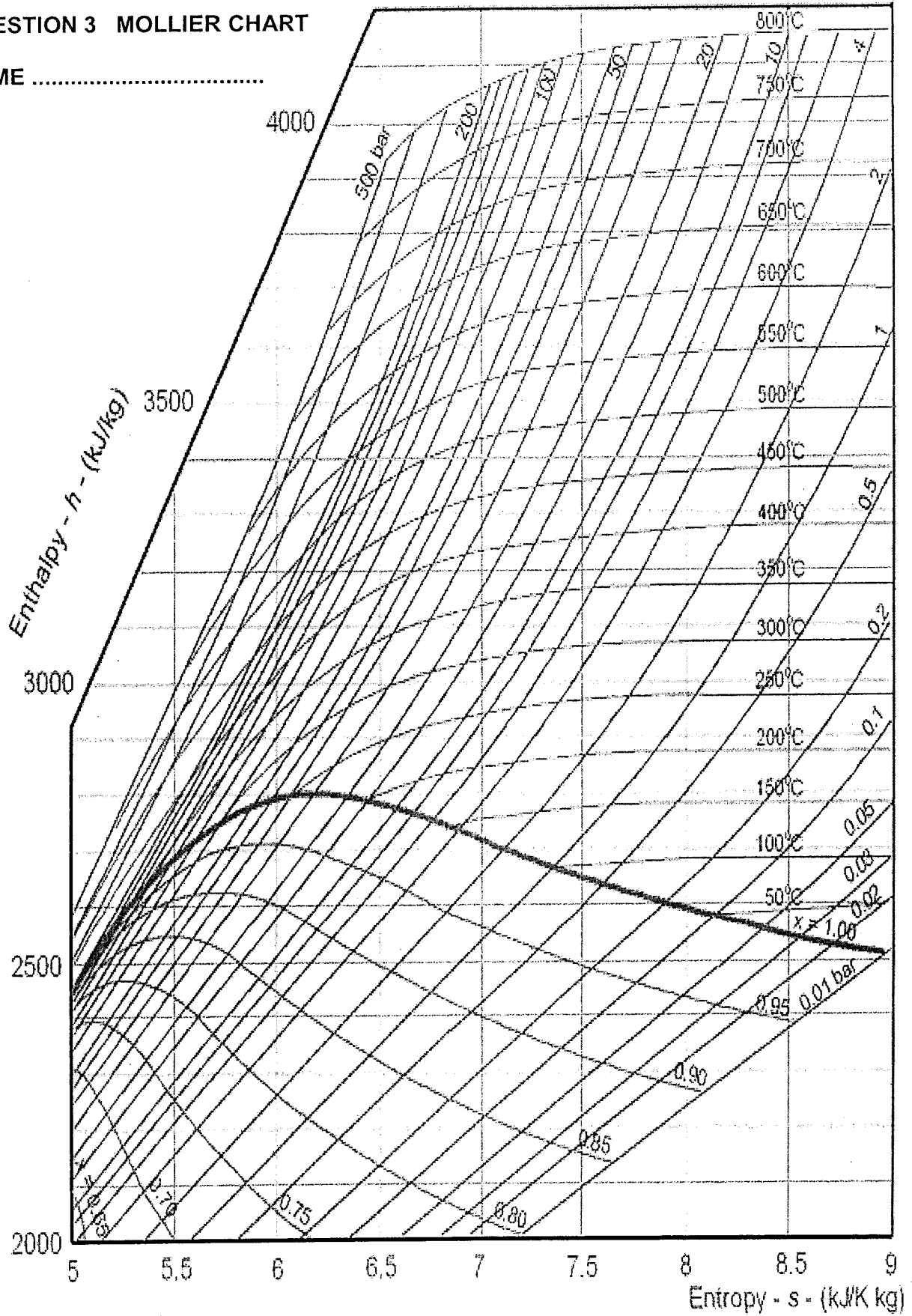


Gas Cycle 1 - 2 - 3 - 4 - 5

Steam Cycle 5 - 7 - 8 - 9 - 10

QUESTION 3 MOLLIER CHART

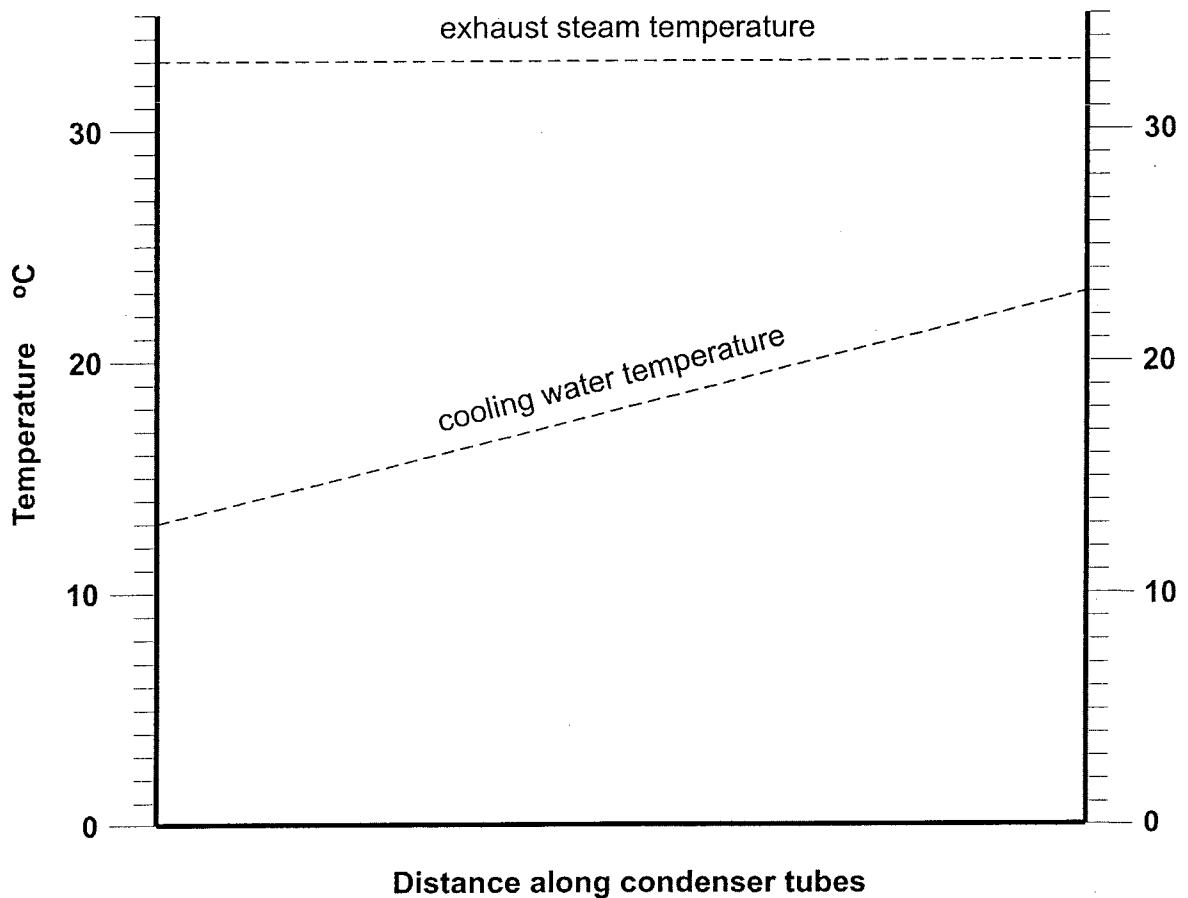
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**QUESTION 3 CONDENSER CONDITIONS**

- (d) Show temperature profiles (exhaust steam and cooling water) for part load conditions (when throttled to 4 MPa. Assume that the cooling water inlet temperature remains constant



- (e) Determine the condenser pressure at part load conditions (4 MPa steam inlet)

- (f) Estimate the exhaust steam temperature and condenser pressure at zero load conditions (0.1 MPa steam inlet)

QUESTION 4 PART I VESTAS WIND TURBINE



# V80 – 1.8 MW

Pitch regulated wind turbine with OptiSlip® and OptiTip®

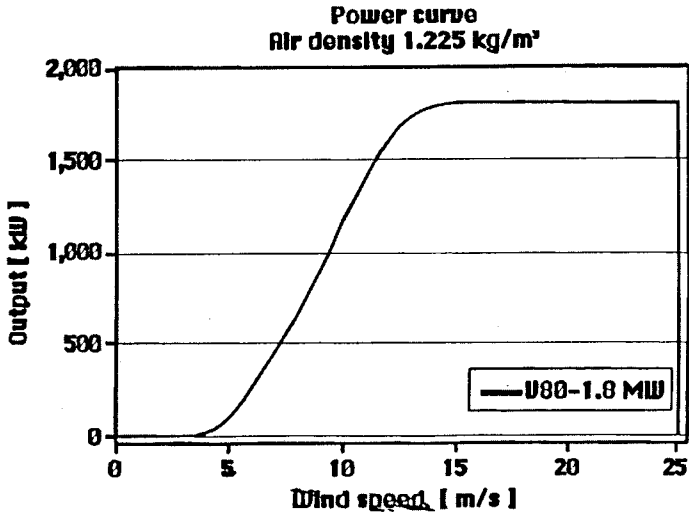
ROTOR			
Diameter:	80 m		
Swept area:	5,027 m <sup>2</sup>		
Speed of revolution:	15.7 RPM		
Number of blades:	3		
Power regulation:	Pitch + OptiSlip®		
Air brake:	3 separate pitch settings		
TOWER:			
Hub height (approx.):	60 - 67 - 78 m		
OPERATIONAL DATA:			
Cut-in wind speed:	4 m/s		
Nominal wind speed:	16 m/s		
Stop wind speed:	25 m/s		
GENERATOR:			
Type:	Asynchronous with OptiSlip®		
Nominal output:	1.8 MW		
Operational data:	60 Hz 690V 1,800 - 1,900 RPM		
GEARBOX:			
Type:	Planet/parallel gear		
CONTROL:			
Type:	Microprocessor-based control of all turbine functions with the option of remote monitoring. OptiSlip® output regulation and OptiTip® pitch regulation of the blades.		
WEIGHT: (APPROX.)			
	(60 m)	(67 m)	(78 m)
Nacelle:	63 t	63 t	63 t
Rotor:	30 t	30 t	30 t

## Ideal for moderate wind conditions

The V80-1.8 MW is particularly well suited for installation in areas with moderate to high wind conditions, and thanks to OptiSlip®, the turbine can adapt to wind conditions in almost any location. In this way, Vestas continues to strive for excellence by taking firm steps towards the full exploitation of wind energy.

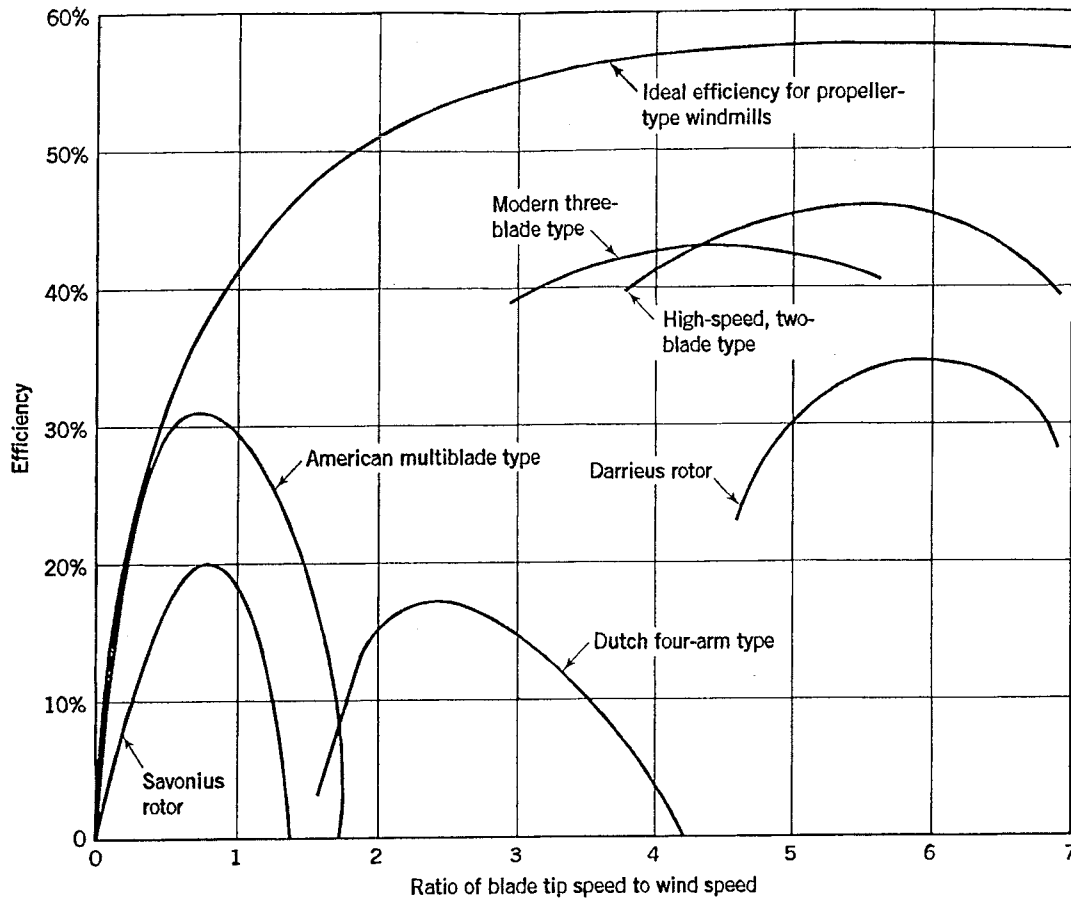
## Advanced Vestas technology

The Vestas V80-1.8 MW is based on the well-known technology from the V66-1.65 MW turbine. The turbine is a three blade 60 Hz pitch-regulated wind turbine with OptiSlip® and OptiTip®. The turbine's rotor diameter is 80 meters – and the turbine can be delivered with tower heights of up to 78 meters.



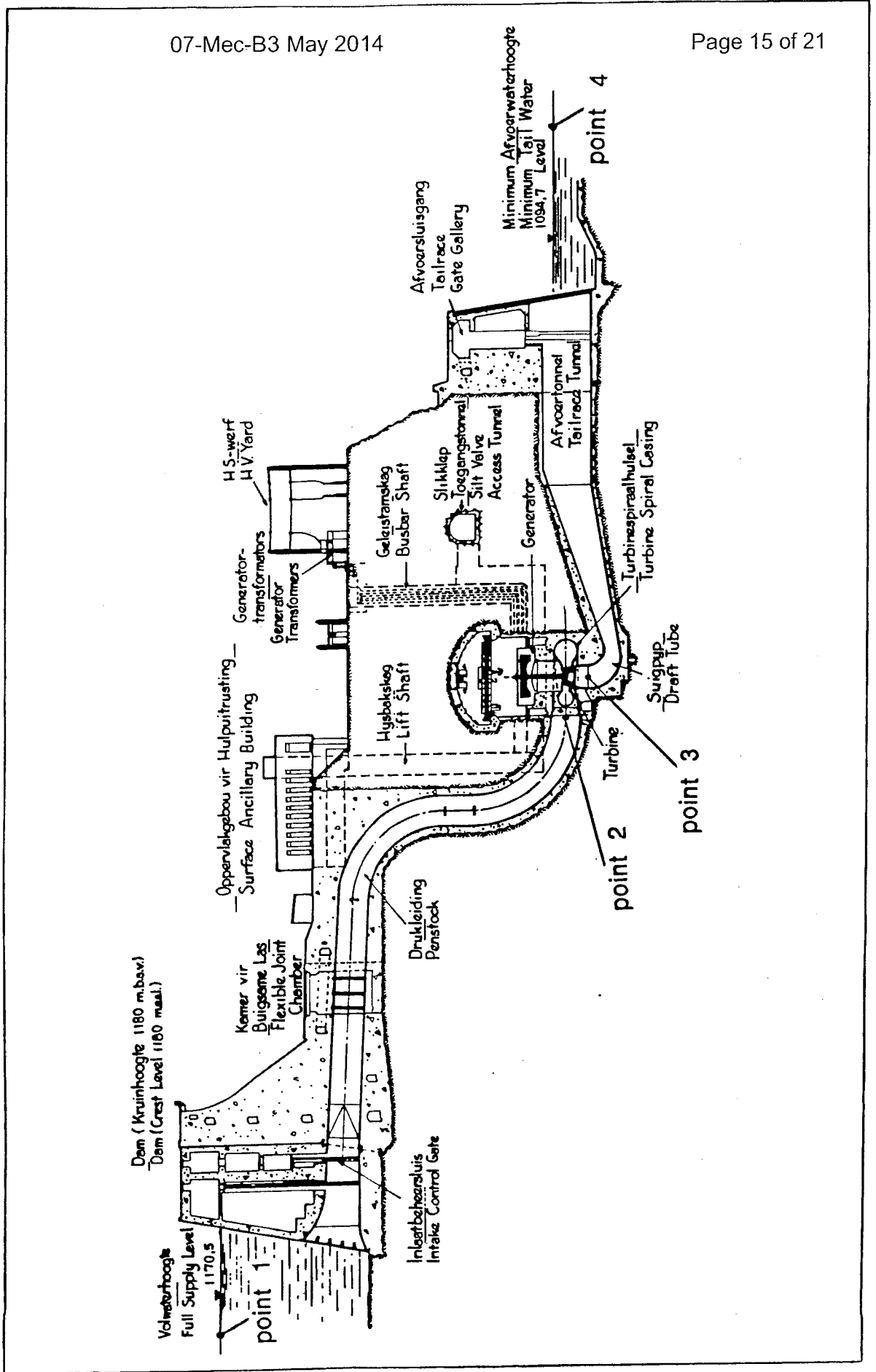
## QUESTION 4 PART I WIND POWER EFFICIENCIES

Wind Power 135



**Figure 5.6** Typical efficiencies of several types of windmills plotted against their tip-speed ratio. The maximum efficiencies are seen to vary from about 16 to 46%. The ideal efficiency shown is a mathematical ideal, never to be achieved in practice. (Source: Basic data from R. Wilson and P. Lissaman, *Applied Aerodynamics of Wind Power Machines*, Oregon State University.)

QUESTION 4 PART II VANDERKLOOF HYDRO POWER STATION  
Cross-section through Power Station Waterways/Dwarsdeursnit van Kragstasie-Afvoerkanale

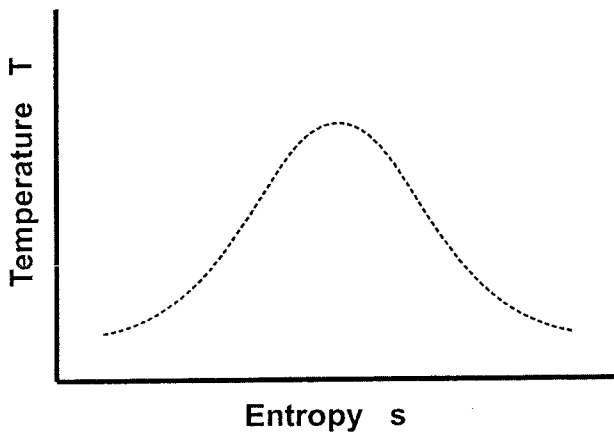


QUESTION 5 PART I T-s DIAGRAMS

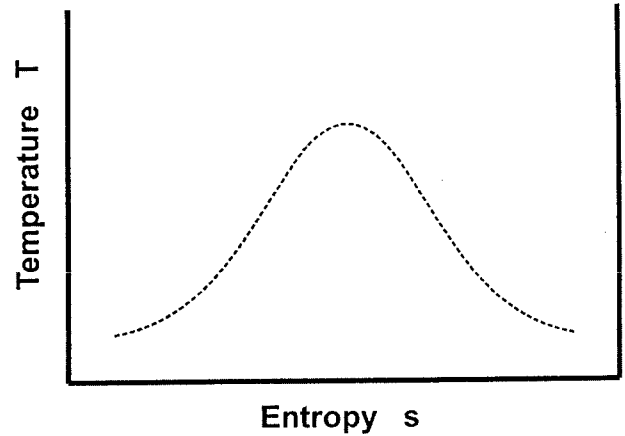
NAME .....

Draw T-s and p-V diagrams for the cycles specified on the given axes

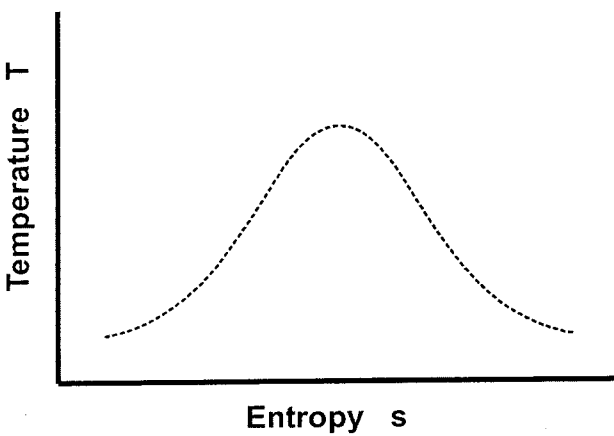
(i) Rankine cycle (saturated conditions)



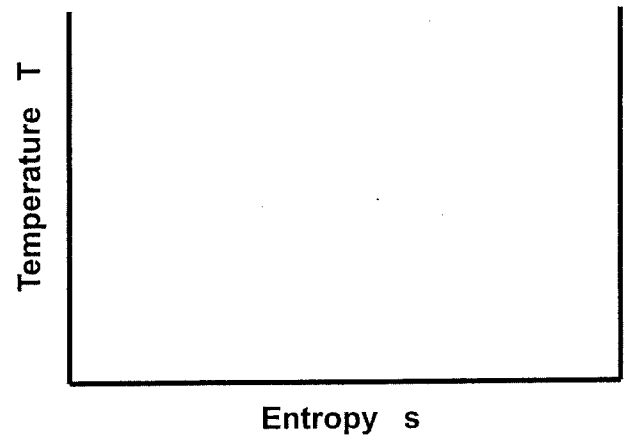
(ii) Rankine cycle with superheat



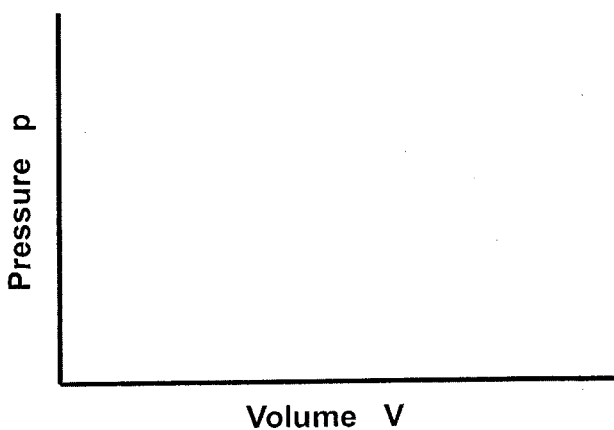
(iii) Rankine cycle with superheat and reheat



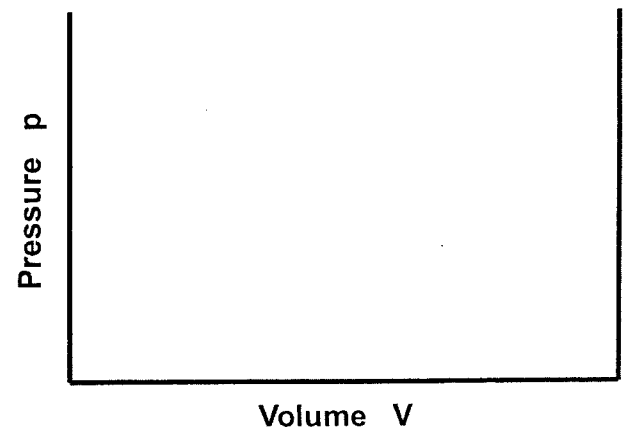
(iv) Brayton cycle



(v) Otto cycle



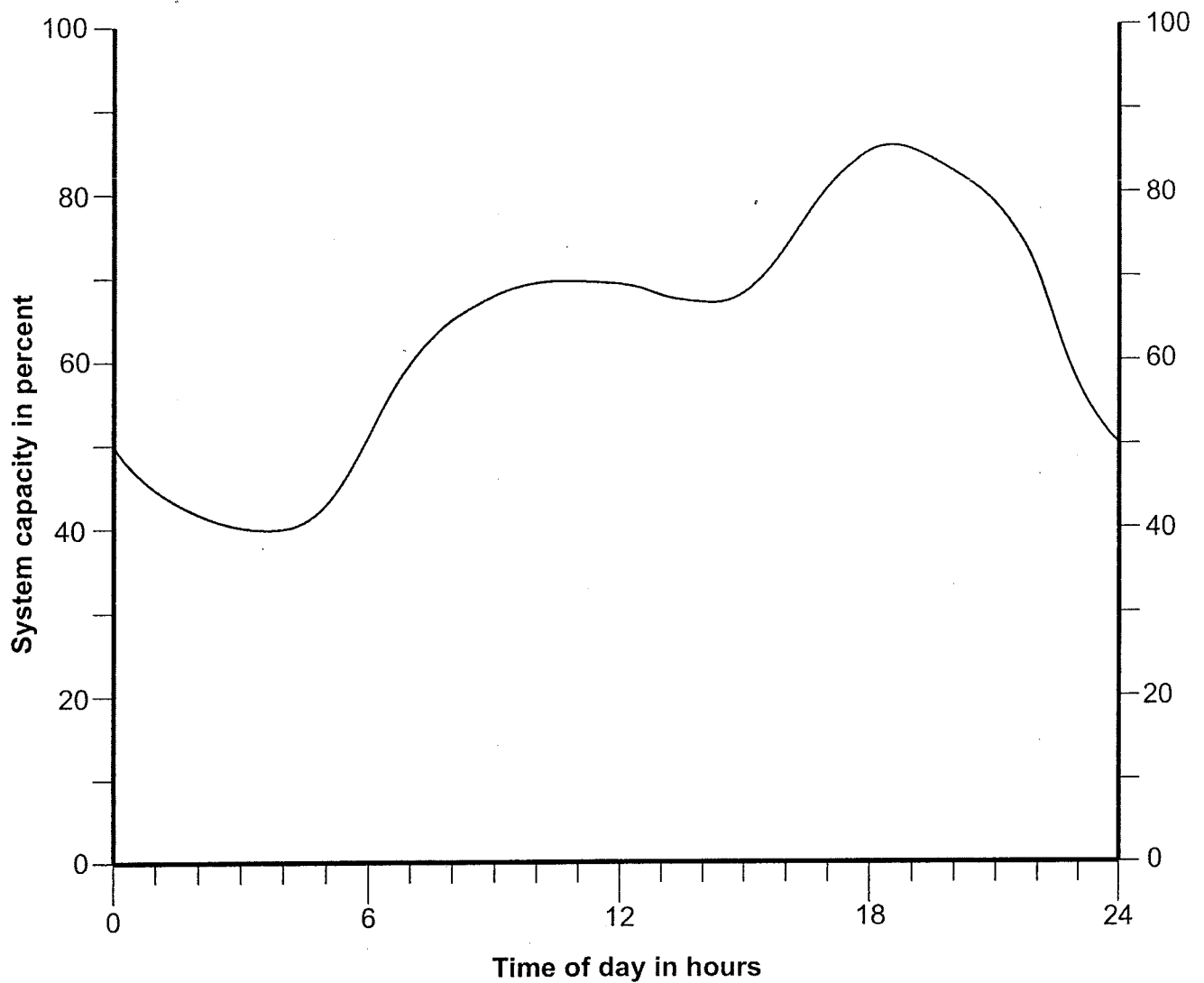
(vi) Diesel cycle



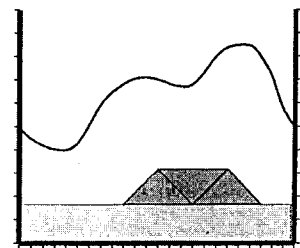


### QUESTION 5 PART II DAILY LOAD CURVE

- (a) Show how the given plants would be utilized to meet the daily demand as defined by the curve below



Show the utilization of the various plants by blocking in their output and operational time on the diagram above. The small illustration alongside indicates how this should be done with base load plants at the bottom and peak load plants to make up the remaining demand. Hint: Take account of the fuel price to minimize the overall operational cost



**NOMENCLATURE FOR REFERENCE EQUATIONS (SI UNITS)**

A	Flow area, Surface area	$m^2$
$c_p$	Specific heat at constant pressure	$J/kg^\circ C$
$c_v$	Specific heat at constant volume	$J/kg^\circ C$
D	Diameter	m
E	Energy	J
g	Gravitational acceleration	$m/s^2$
h	Specific enthalpy	$J/kg$
k	Ratio of specific heats	
L	Length	m
m	Fractional mass flow rate	
m	Mass	kg
M	Mass flow rate	kg/s
p	Pressure	Pa ( $N/m^2$ )
q	Heat transferred	$J/kg$
Q	Heat	J
Q	Volume flow rate	$m^3/s$
R	Specific gas constant	$J/kg K$
s	Entropy	$J/kg K$
T	Temperature	K
u	Specific internal energy	$J/kg$
U	Overall heat transfer coefficient	$W/m^2^\circ C$ ( $J/sm^2^\circ C$ )
v	Specific volume	$m^3/kg$
V	Velocity	m/s
w	Specific work	$J/kg$
W	Work	J
x	Length	m
z	Elevation	m
$\eta$	Efficiency	°
$\theta$	Nozzle angle	°
$\theta$	Temperature difference between fluids	$^\circ C$
$\mu$	Dynamic viscosity	$Ns/m^2$
$\nu$	Kinematic viscosity	$m^2/s$
$\rho$	Density	$kg/m^3$
$\tau$	Thrust	N
$\Omega$	Heat transfer rate	$J/s$

**GENERAL CONSTANTS**

Acceleration due to gravity: $g = 9.81 \text{ m/s}^2$	Specific heat of air: $c_p = 1.005 \text{ kJ/kg}^\circ\text{C}$
Atmospheric pressure: $p_{\text{atm}} = 100 \text{ kPa}$	Specific heat of air: $c_v = 0.718 \text{ kJ/kg}^\circ\text{C}$
Density of water: $\rho_{\text{water}} = 1000 \text{ kg/m}^3$	Specific heat of helium: $c_p = 5.193 \text{ kJ/kg}^\circ\text{C}$
Specific heat of water: $c_p = 4.190 \text{ kJ/kg}^\circ\text{C}$	Specific heat of helium: $c_v = 3.117 \text{ kJ/kg}^\circ\text{C}$

**THERMODYNAMICS REFERENCE EQUATIONS****Basic Thermodynamics**

First Law:	$dE = \delta Q - \delta W$
Enthalpy:	$h = u + pv$
Continuity:	$\rho VA = \text{constant}$
Flow Work:	$w = \Delta(pv)$
Energy Equation:	$zg + V^2/2 + u + pv + \Delta w + \Delta q = \text{constant}$
Entropy:	$\Delta s = \sum \delta q / T$ (reversible conditions)

**Ideal Gas Relationships**

Gas Law:	$pv = RT$
Specific Heat at Constant Pressure:	$c_p = \Delta h / \Delta T$
Specific Heat at Constant Volume:	$c_v = \Delta u / \Delta T$
Gas Constant:	$R = c_p - c_v$
Specific Heat Ratio:	$k = c_p / c_v$
Isentropic Relations:	$p_1 / p_2 = (v_2 / v_1)^k = (T_1 / T_2)^{k/(k-1)}$

## FLUID MECHANICS REFERENCE EQUATIONS

### Fluid Mechanics

Continuity Equation:  $\rho_1 V_1 A_1 = \rho_2 V_2 A_2 = M$

Bernoulli's Equation:  $p_1/\rho g + z_1 + V_1^2/2g = p_2/\rho g + z_2 + V_2^2/2g$

Momentum Equation:  $F = p_1 A_1 - p_2 A_2 - \rho V A (V_2 - V_1)$  (one dimensional)

### Steam Turbines

Nozzle Equation:  $h_1 - h_2 = (V_2^2 - V_1^2) / 2$

Work:  $w = [(V_1^2_{\text{absolute}} - V_2^2_{\text{absolute}}) + (V_2^2_{\text{relative}} - V_1^2_{\text{relative}})] / 2$

### Gas Turbines

State Equation:  $p v = R T$

Isentropic Equation:  $(T_2/T_1) = (p_2/p_1)^{(k-1)/k}$

Enthalpy Change:  $h_1 - h_2 = c_p (T_1 - T_2)$  (ideal gas)

Nozzle Equation:  $h_1 - h_2 = (V_2^2 - V_1^2) / 2$

### Jet Propulsion

Thrust:  $T = M(V_{\text{jet}} - V_{\text{aircraft}})$

Thrust Power:  $T V_{\text{aircraft}} = M(V_{\text{jet}} - V_{\text{aircraft}}) V_{\text{aircraft}}$

Jet Power:  $P = M(V_{\text{jet}}^2 - V_{\text{aircraft}}^2) / 2$

Propulsion Efficiency:  $\eta_p = 2V_{\text{aircraft}} / (V_{\text{jet}} + V_{\text{aircraft}})$

### Wind Turbine

Maximum Ideal Power:  $P_{\text{max}} = 8 \rho A V_1^3 / 27$

**HEAT EXCHANGER REFERENCE EQUATIONS**

Heat transferred between fluids

$$\Omega = U A \theta$$

Heat gained or lost by fluids

$$\Omega = M \Delta h$$

$$\Omega = M c_p \Delta T$$

$$\Omega = \rho Q \Delta T$$

**NUCLEAR REFERENCE EQUATIONS**

Number of nuclei per gram of material

$$N = N_A / M$$

Number of fissile nuclei per cm<sup>3</sup> of material

$$N_f = \gamma (N_A / M) \rho$$

Heat release rate in nuclear fuel

$$q^* = \phi N_f \sigma_f E_f$$

Nomenclature

N	=	number of nuclei (number/g)
N <sub>A</sub>	=	Avogadro's Number
M	=	molecular weight
γ	=	fuel enrichment
ρ	=	density (g/cm <sup>3</sup> )
q*	=	heat release rate (J/cm <sup>3</sup> )
φ	=	neutron flux (neutrons/cm <sup>2</sup> s)
N <sub>f</sub>	=	number of fissile nuclei (number/cm <sup>3</sup> )
σ <sub>f</sub>	=	cross section (barn) (1 barn = 10 <sup>-24</sup> cm <sup>2</sup> )
E <sub>f</sub>	=	energy release per fission of one atom

Avogadro's Number

$$N_A = 0.602 \times 10^{24} \text{ atoms/mole}$$

# Thermodynamics and Heat Power

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SIXTH EDITION

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**Irving Granet, P.E.**

*late, Queensborough Community College of City University of New York*

**Maurice Bluestein, Ph.D.**

*Indiana University—Purdue University, Indianapolis*

PRENTICE HALL

*Upper Saddle River, New Jersey Columbus, Ohio*

TABLE A.1 (SI)  
Saturation: Temperature (Steam)

Temp. °C <i>T</i>	Press. kPa <i>P</i>	Specific Volume (m <sup>3</sup> /kg)		Internal Energy (kJ/kg)				Enthalpy (kJ/kg)				Entropy (kJ/kg · K)			
		Sat. Liquid <i>v<sub>f</sub></i>	Sat. Vapor <i>v<sub>g</sub></i>	Sat. Liquid <i>u<sub>f</sub></i>	Evap. <i>u<sub>fg</sub></i>	Sat. Vapor <i>u<sub>g</sub></i>	Sat. Liquid <i>h<sub>f</sub></i>	Evap. <i>h<sub>fg</sub></i>	Sat. Vapor <i>h<sub>g</sub></i>	Sat. Liquid <i>s<sub>f</sub></i>	Evap. <i>s<sub>fg</sub></i>	Sat. Vapor <i>s<sub>g</sub></i>			
0.01	0.6113	0.001 000	206.14	.00	2375.3	2375.3	.01	2501.3	2501.4	.0000	9.1562	9.1562	9.1562		
5	0.8721	0.001 000	147.12	20.97	2361.3	2382.3	20.98	2489.6	2510.6	.0761	8.9496	9.0257	9.0257		
10	1.2276	0.001 000	106.38	42.00	2347.2	2389.2	42.01	2477.7	2519.8	.1510	8.7498	8.9008	8.9008		
15	1.7051	0.001 001	77.93	62.99	2333.1	2396.1	62.99	2465.9	2528.9	.2245	8.5569	8.7814	8.7814		
20	2.339	0.001 002	57.79	83.95	2319.0	2402.9	83.96	2454.1	2538.1	.2966	8.3706	8.6672	8.6672		
25	3.169	0.001 003	43.36	104.88	2304.9	2409.8	104.89	2442.3	2547.2	.3674	8.1905	8.5580	8.5580		
30	4.246	0.001 004	32.89	125.78	2290.8	2416.6	125.79	2430.5	2556.3	.4369	8.0164	8.4533	8.4533		
35	5.628	0.001 006	25.22	146.67	2276.7	2423.4	146.68	2418.6	2565.3	.5053	7.8478	8.3531	8.3531		
40	7.384	0.001 008	19.52	167.56	2262.6	2430.1	167.57	2406.7	2574.3	.5725	7.6845	8.2570	8.2570		
45	9.593	0.001 010	15.26	188.44	2248.4	2436.8	188.45	2394.8	2583.2	.6387	7.5261	8.1648	8.1648		
50	12.349	0.001 012	12.03	209.32	2234.2	2443.5	209.33	2382.7	2592.1	.7038	7.3725	8.0763	8.0763		
55	15.758	0.001 015	9.568	230.21	2219.9	2450.1	230.23	2370.7	2600.9	.7679	7.2234	7.9913	7.9913		
60	19.940	0.001 017	7.671	251.11	2205.5	2456.6	251.13	2358.5	2609.6	.8312	7.0784	7.9096	7.9096		
65	25.03	0.001 020	6.197	272.02	2191.1	2463.1	272.06	2346.2	2618.3	.8935	6.9375	7.8310	7.8310		
70	31.19	0.001 023	5.042	292.95	2176.6	2469.6	292.98	2333.8	2626.8	.9549	6.8004	7.7553	7.7553		
75	38.58	0.001 026	4.131	313.90	2162.0	2475.9	313.93	2321.4	2635.3	1.0155	6.6669	7.6824	7.6824		
80	47.39	0.001 029	3.407	334.86	2147.4	2482.2	334.91	2308.8	2643.7	1.0753	6.5369	7.6122	7.6122		
85	57.83	0.001 033	2.828	355.84	2132.6	2488.4	355.90	2296.0	2651.9	1.1343	6.4102	7.5445	7.5445		
90	70.14	0.001 036	2.361	376.85	2117.7	2494.5	376.92	2283.2	2660.1	1.1925	6.2866	7.4791	7.4791		
95	84.55	0.001 040	1.982	397.88	2102.7	2500.6	397.96	2270.2	2668.1	1.2500	6.1659	7.4159	7.4159		





TABLE A.1 (SI) (cont'd.)

Temp. °C T	Press. MPa P	Specific Volume (m <sup>3</sup> /kg)				Internal Energy (kJ/kg)				Enthalpy (kJ/kg)				Entropy (kJ/kg · °K)			
		Sat. Liquid $v_f$	Sat. Vapor $v_g$	Sat. Liquid $u_f$	Sat. Vapor $u_g$	Sat. Liquid $u_f$	Sat. Vapor $u_g$	Sat. Liquid $h_f$	Sat. Vapor $h_g$	Sat. Liquid $h_f$	Sat. Vapor $h_g$	Sat. Liquid $s_f$	Sat. Vapor $s_g$	Sat. Liquid $s_f$	Sat. Vapor $s_g$		
250	3.973	0.001 251	0.050 13	1080.39	1522.0	2602.4	1085.36	1716.2	2801.5	2.7927	3.2802	6.0730					
255	4.319	0.001 263	0.045 98	1104.28	1496.7	2600.9	1109.73	1689.8	2799.5	2.8383	3.1992	6.0375					
260	4.688	0.001 276	0.042 21	1128.39	1470.6	2599.0	1134.37	1662.5	2796.9	2.8838	3.1181	6.0019					
265	5.081	0.001 289	0.038 77	1152.74	1443.9	2596.6	1159.28	1634.4	2793.6	2.9294	3.0368	5.9662					
270	5.499	0.001 302	0.035 64	1177.36	1416.3	2593.7	1184.51	1605.2	2789.7	2.9751	2.9551	5.9301					
275	5.942	0.001 317	0.032 79	1202.25	1387.9	2590.2	1210.07	1574.9	2785.0	3.0208	2.8730	5.8938					
280	6.412	0.001 332	0.030 17	1227.46	1358.7	2586.1	1235.99	1543.6	2779.6	3.0668	2.7903	5.8571					
285	6.909	0.001 348	0.027 77	1253.00	1328.4	2581.4	1262.31	1511.0	2773.3	3.1130	2.7070	5.8199					
290	7.436	0.001 366	0.025 57	1278.92	1297.1	2576.0	1289.07	1477.1	2766.2	3.1594	2.6227	5.7821					
295	7.993	0.001 384	0.023 54	1305.2	1264.7	2569.9	1316.3	1441.8	2758.1	3.2062	2.5375	5.7437					
300	8.581	0.001 404	0.021 67	1332.0	1231.0	2563.0	1344.0	1404.9	2749.0	3.2534	2.4511	5.7045					
305	9.202	0.001 425	0.019 948	1359.3	1195.9	2555.2	1372.4	1366.4	2738.7	3.3010	2.3633	5.6643					
310	9.856	0.001 447	0.018 350	1387.1	1159.4	2546.4	1401.3	1326.0	2727.3	3.3493	2.2737	5.6230					
315	10.547	0.001 472	0.016 867	1415.5	1121.1	2536.6	1431.0	1283.5	2714.5	3.3982	2.1821	5.5804					
320	11.274	0.001 499	0.015 488	1444.6	1080.9	2525.5	1461.5	1238.6	2700.1	3.4480	2.0882	5.5362					
330	12.845	0.001 561	0.012 996	1505.3	993.7	2498.9	1525.3	1140.6	2665.9	3.5507	1.8909	5.4417					
340	14.586	0.001 638	0.010 797	1570.3	894.3	2464.6	1594.2	1027.9	2622.0	3.6594	1.6763	5.3357					
350	16.513	0.001 740	0.008 813	1641.9	776.6	2418.4	1670.6	893.4	2563.9	3.7777	1.4335	5.2112					
360	18.651	0.001 893	0.006 945	1725.2	626.3	2351.5	1760.5	720.5	2481.0	3.9147	1.1379	5.0526					
370	21.03	0.002 213	0.004 925	1844.0	384.5	2228.5	1890.5	441.6	2332.1	4.1106	.6865	4.7971					
374.14	22.09	0.003 155	0.003 155	2029.6	0	2029.6	2099.3	0	2099.3	4.4298	0	4.4298					

TABLE A.2 (SI)  
Saturation Pressures (Steam)

Press. kPa <i>P</i>	Temp. °C <i>T</i>	Specific Volume (m <sup>3</sup> /kg)				Internal Energy (kJ/kg)				Enthalpy (kJ/kg)				Entropy (kJ/kg · °K)			
		Sat. Liquid <i>v<sub>f</sub></i>	Sat. Vapor <i>v<sub>g</sub></i>	Sat. Liquid <i>u<sub>f</sub></i>	Sat. Vapor <i>u<sub>g</sub></i>	Sat. Liquid <i>u<sub>f</sub></i>	Evap. <i>u<sub>fg</sub></i>	Sat. Vapor <i>u<sub>g</sub></i>	Sat. Liquid <i>h<sub>f</sub></i>	Evap. <i>h<sub>fg</sub></i>	Sat. Vapor <i>h<sub>g</sub></i>	Sat. Liquid <i>s<sub>f</sub></i>	Evap. <i>s<sub>fg</sub></i>	Sat. Vapor <i>s<sub>g</sub></i>			
0.6113	0.01	0.001 000	206.14	.00	2375.3	2375.3	2375.3	.01	2501.3	2501.4	.0000	9.1562	9.1562				
1.0	6.98	0.001 000	129.21	29.30	2355.7	2385.0	2385.0	29.30	2484.9	2514.2	.1059	8.8697	8.9756				
1.5	13.03	0.001 001	87.98	54.71	2338.6	2393.3	2393.3	54.71	2470.6	2525.3	.1957	8.6322	8.8279				
2.0	17.50	0.001 001	67.00	73.48	2326.0	2399.5	2399.5	73.48	2460.0	2533.5	.2607	8.4629	8.7237				
2.5	21.08	0.001 002	54.25	88.48	2315.9	2404.4	2404.4	88.48	2451.6	2540.0	.3120	8.3311	8.6432				
3.0	24.08	0.001 003	45.67	101.04	2307.5	2408.5	2408.5	101.05	2444.5	2545.5	.3545	8.2231	8.5776				
4.0	28.96	0.001 004	34.80	121.45	2293.7	2415.2	2415.2	121.46	2432.9	2554.4	.4226	8.0520	8.4746				
5.0	32.88	0.001 005	28.19	137.81	2282.7	2420.5	2420.5	137.82	2423.7	2561.5	.4764	7.9187	8.3951				
7.5	40.29	0.001 008	19.24	168.78	2261.7	2430.5	2430.5	168.79	2406.0	2574.8	.5764	7.6750	8.2515				
10	45.81	0.001 010	14.67	191.82	2246.1	2437.9	2437.9	191.83	2392.8	2584.7	.6493	7.5009	8.1502				
15	53.97	0.001 014	10.02	225.92	2222.8	2448.7	2448.7	225.94	2373.1	2599.1	.7549	7.2536	8.0085				
20	60.06	0.001 017	7.649	251.38	2205.4	2456.7	2456.7	251.40	2358.3	2609.7	.8320	7.0766	7.9085				
25	64.97	0.001 020	6.204	271.90	2191.2	2463.1	2463.1	271.93	2346.3	2618.2	.8931	6.9383	7.8314				
30	69.10	0.001 022	5.229	289.20	2179.2	2468.4	2468.4	289.23	2336.1	2625.3	.9439	6.8247	7.7686				
40	75.87	0.001 027	3.993	317.53	2159.5	2477.0	2477.0	317.58	2319.2	2636.8	1.0259	6.6441	7.6700				
50	81.33	0.001 030	3.240	340.44	2143.4	2483.9	2483.9	340.49	2305.4	2645.9	1.0910	6.5029	7.5939				
75	91.78	0.001 037	2.217	384.31	2112.4	2496.7	2496.7	384.39	2278.6	2663.0	1.2130	6.2434	7.4564				
MPa																	
0.100	99.63	0.001 043	1.6940	417.36	2088.7	2506.1	2506.1	417.46	2258.0	2675.5	1.3026	6.0568	7.3594				
0.125	105.99	0.001 048	1.3749	444.19	2069.3	2513.5	2513.5	444.32	2241.0	2685.4	1.3740	5.9104	7.2844				
0.150	111.37	0.001 053	1.1593	466.94	2052.7	2519.7	2519.7	467.11	2226.5	2693.6	1.4336	5.7897	7.2233				
0.175	116.06	0.001 057	1.0036	486.80	2038.1	2524.9	2524.9	486.99	2213.6	2700.6	1.4849	5.6868	7.1717				
0.200	120.23	0.001 061	0.8857	504.49	2025.0	2529.5	2529.5	504.70	2201.9	2706.7	1.5301	5.5970	7.1271				
0.225	124.00	0.001 064	0.7933	520.47	2013.1	2533.6	2533.6	520.72	2191.3	2712.1	1.5706	5.5173	7.0878				

TABLE A.2 (SI) (cont'd.)

Press. MPa <i>P</i>	Temp. °C <i>T</i>	Specific Volume		Internal Energy				Enthalpy				Entropy	
		Sat. Liquid <i>v<sub>f</sub></i>	Sat. Vapor <i>v<sub>g</sub></i>	Sat. Liquid <i>u<sub>f</sub></i>	Evap. <i>u<sub>fg</sub></i>	Sat. Vapor <i>u<sub>g</sub></i>	Sat. Liquid <i>h<sub>f</sub></i>	Evap. <i>h<sub>fg</sub></i>	Sat. Vapor <i>h<sub>g</sub></i>	Sat. Liquid <i>s<sub>f</sub></i>	Evap. <i>s<sub>fg</sub></i>	Sat. Vapor <i>s<sub>g</sub></i>	
0.250	127.44	0.001 067	0.7187	535.10	2002.1	2537.2	535.37	2181.5	2716.9	1.6072	5.4455	7.0527	
0.275	130.60	0.001 070	0.6573	548.59	1991.9	2540.5	548.89	2172.4	2721.3	1.6408	5.3801	7.0209	
0.300	133.55	0.001 073	0.6058	561.15	1982.4	2543.6	561.47	2163.8	2725.3	1.6718	5.3201	6.9919	
0.325	136.30	0.001 076	0.5620	572.90	1973.5	2546.4	573.25	2155.8	2729.0	1.7006	5.2646	6.9652	
0.350	138.88	0.001 079	0.5243	583.95	1965.0	2548.9	584.33	2148.1	2732.4	1.7275	5.2130	6.9405	
0.375	141.32	0.001 081	0.4914	594.40	1956.9	2551.3	594.81	2140.8	2735.6	1.7528	5.1647	6.9175	
0.40	143.63	0.001 084	0.4625	604.31	1949.3	2553.6	604.74	2133.8	2738.6	1.7766	5.1193	6.8959	
0.45	147.93	0.001 088	0.4140	622.77	1934.9	2557.6	623.25	2120.7	2743.9	1.8207	5.0359	6.8565	
0.50	151.86	0.001 093	0.3749	639.68	1921.6	2561.2	640.23	2108.5	2748.7	1.8607	4.9606	6.8213	
0.55	155.48	0.001 097	0.3427	655.32	1909.2	2564.5	655.93	2097.0	2753.0	1.8973	4.8920	6.7893	
0.60	158.85	0.001 101	0.3157	669.90	1897.5	2567.4	670.56	2086.3	2756.8	1.9312	4.8288	6.7600	
0.65	162.01	0.001 104	0.2927	683.56	1886.5	2570.1	684.28	2076.0	2760.3	1.9627	4.7703	6.7331	
0.70	164.97	0.001 108	0.2729	696.44	1876.1	2572.5	697.22	2066.3	2763.5	1.9922	4.7158	6.7080	
0.75	167.78	0.001 112	0.2556	708.64	1866.1	2574.7	709.47	2057.0	2766.4	2.0200	4.6647	6.6847	
0.80	170.43	0.001 115	0.2404	720.22	1856.6	2576.8	721.11	2048.0	2769.1	2.0462	4.6166	6.6628	
0.85	172.96	0.001 118	0.2270	731.27	1847.4	2578.7	732.22	2039.4	2771.6	2.0710	4.5711	6.6421	
0.90	175.38	0.001 121	0.2150	741.83	1838.6	2580.5	742.83	2031.1	2773.9	2.0946	4.5280	6.6226	
0.95	177.69	0.001 124	0.2042	751.95	1830.2	2582.1	753.02	2023.1	2776.1	2.1172	4.4869	6.6041	
1.00	179.91	0.001 127	0.194 44	761.68	1822.0	2583.6	762.81	2015.3	2778.1	2.1387	4.4478	6.5865	
1.10	184.09	0.001 133	0.177 53	780.09	1806.3	2586.4	781.34	2000.4	2781.7	2.1792	4.3744	6.5536	
1.20	187.99	0.001 139	0.163 33	797.29	1791.5	2588.8	798.65	1986.2	2784.8	2.2166	4.3067	6.5233	
1.30	191.64	0.001 144	0.151 25	813.44	1777.5	2591.0	814.93	1972.7	2787.6	2.2515	4.2438	6.4953	
1.40	195.07	0.001 149	0.140 84	828.70	1764.1	2592.8	830.30	1959.7	2790.0	2.2842	4.1850	6.4693	

TABLE A.2 (SI) (cont'd.)

Press. MPa P	Temp. °C T	Specific Volume (m <sup>3</sup> /kg)			Internal Energy (kJ/kg)			Enthalpy (kJ/kg)			Entropy (kJ/kg · K)		
		Sat. Liquid $v_f$	Sat. Vapor $v_g$	Sat. Liquid $u_f$	Evap. $u_{fg}$	Sat. Vapor $u_g$	Sat. Liquid $h_f$	Evap. $h_{fg}$	Sat. Vapor $h_g$	Sat. Liquid $s_f$	Evap. $s_{fg}$	Sat. Vapor $s_g$	
1.50	198.32	0.001 154	0.131 77	843.16	1751.3	2594.5	844.89	1947.3	2792.2	2.3150	4.1298	6.4448	
1.75	205.76	0.001 166	0.113 49	876.46	1721.4	2597.8	878.50	1917.9	2796.4	2.3851	4.0044	6.3896	
2.00	212.42	0.001 177	0.099 63	906.44	1693.8	2600.3	908.79	1890.7	2799.5	2.4474	3.8935	6.3409	
2.25	218.45	0.001 187	0.088 75	933.83	1668.2	2602.0	936.49	1865.2	2801.7	2.5035	3.7937	6.2972	
2.5	223.99	0.001 197	0.079 98	959.11	1644.0	2603.1	962.11	1841.0	2803.1	2.5547	3.7028	6.2575	
3.0	233.90	0.001 217	0.066 68	1004.78	1599.3	2604.1	1008.42	1795.7	2804.2	2.6457	3.5412	6.1869	
3.5	242.60	0.001 235	0.057 07	1045.43	1558.3	2603.7	1049.75	1753.7	2803.4	2.7253	3.4000	6.1253	
4	250.40	0.001 252	0.049 78	1082.31	1520.0	2602.3	1087.31	1714.1	2801.4	2.7964	3.2737	6.0701	
5	263.99	0.001 286	0.039 44	1147.81	1449.3	2597.1	1154.23	1640.1	2794.3	2.9202	3.0532	5.9734	
6	275.64	0.001 319	0.032 44	1205.44	1384.3	2589.7	1213.35	1571.0	2784.3	3.0267	2.8625	5.8892	
7	285.88	0.001 351	0.027 37	1257.55	1323.0	2580.5	1267.00	1505.1	2772.1	3.1211	2.6922	5.8133	
8	295.06	0.001 384	0.023 52	1305.57	1264.2	2569.8	1316.64	1441.3	2758.0	3.2068	2.5364	5.7432	
9	303.40	0.001 418	0.020 48	1350.51	1207.3	2557.8	1363.26	1378.9	2742.1	3.2858	2.3915	5.6772	
10	311.06	0.001 452	0.018 026	1393.04	1151.4	2544.4	1407.56	1317.1	2724.7	3.3596	2.2544	5.6141	
11	318.15	0.001 489	0.015 987	1433.7	1096.0	2529.8	1450.1	1255.5	2705.6	3.4295	2.1233	5.5527	
12	324.75	0.001 527	0.014 263	1473.0	1040.7	2513.7	1491.3	1193.6	2684.9	3.4962	1.9962	5.4924	
13	330.93	0.001 567	0.012 780	1511.1	985.0	2496.1	1531.5	1130.7	2662.2	3.5606	1.8718	5.4323	
14	336.75	0.001 611	0.011 485	1548.6	928.2	2476.8	1571.1	1066.5	2637.6	3.6232	1.7485	5.3717	
15	342.24	0.001 658	0.010 337	1585.6	869.8	2455.5	1610.5	1000.0	2610.5	3.6848	1.6249	5.3098	
16	347.44	0.001 711	0.009 306	1622.7	809.0	2431.7	1650.1	930.6	2580.6	3.7461	1.4994	5.2455	
17	352.37	0.001 770	0.008 364	1660.2	744.8	2405.0	1690.3	856.9	2547.2	3.8079	1.3698	5.1777	
18	357.06	0.001 840	0.007 489	1698.9	675.4	2374.3	1732.0	777.1	2509.1	3.8715	1.2329	5.1044	
19	361.54	0.001 924	0.006 657	1739.9	598.1	2338.1	1776.5	688.0	2464.5	3.9388	1.0839	5.0228	
20	365.81	0.002 036	0.005 834	1785.6	507.5	2293.0	1826.3	583.4	2409.7	4.0139	.9130	4.9269	
21	369.89	0.002 207	0.004 952	1842.1	388.5	2230.6	1888.4	446.2	2334.6	4.1075	.6938	4.8013	
22	373.80	0.002 742	0.003 568	1961.9	125.2	2087.1	2022.2	143.4	2165.6	4.3110	.2216	4.5327	
22.09	374.14	0.003 155	0.003 155	2029.6	0	2029.6	2099.3	0	2099.3	4.4298	0	4.4298	

















TABLE A.3 (SI) (cont'd.)

T	P = 25.0 MPa					P = 30.0 MPa					P = 35.0 MPa					
	v	u	h	s	v	u	h	s	v	u	h	s	v	u	h	s
700	.016 646	3361.3	3777.5	6.6707	.013 661	3335.8	3745.6	6.5606	.011 533	3309.8	3713.5	6.4631				
800	.018 912	3574.3	4047.1	6.9345	.015 623	3555.5	4024.2	6.8332	.013 278	3536.7	4001.5	6.7450				
900	.021 045	3783.0	4309.1	7.1680	.017 448	3768.5	4291.9	7.0718	.014 883	3754.0	4274.9	6.9886				
1000	.023 10	3990.9	4568.5	7.3802	.019 196	3978.8	4554.7	7.2867	.016 410	3966.7	4541.1	7.2064				
1100	.025 12	4200.2	4828.2	7.5765	.020 903	4189.2	4816.3	7.4845	.017 895	4178.3	4804.6	7.4057				
1200	.027 11	4412.0	5089.9	7.7605	.022 589	4401.3	5079.0	7.6692	.019 360	4390.7	5068.3	7.5910				
1300	.029 10	4626.9	5354.4	7.9342	.024 266	4616.0	5344.0	7.8432	.020 815	4605.1	5333.6	7.7653				
P = 40.0 MPa																
375	.001 640 7	1677.1	1742.8	3.8290	.001 559 4	1638.6	1716.6	3.7639	.001 502 8	1609.4	1699.5	3.7141				
400	.001 907 7	1854.6	1930.9	4.1135	.001 730 9	1788.1	1874.6	4.0031	.001 633 5	1745.4	1843.4	3.9318				
425	.002 532	2096.9	2198.1	4.5029	.002 007	1959.7	2060.0	4.2734	.001 816 5	1892.7	2001.7	4.1626				
450	.003 693	2365.1	2512.8	4.9459	.002 486	2159.6	2284.0	4.5884	.002 085	2053.9	2179.0	4.4121				
500	.005 622	2678.4	2903.3	5.4700	.003 892	2525.5	2720.1	5.1726	.002 956	2390.6	2567.9	4.9321				
550	.006 984	2869.7	3149.1	5.7785	.005 118	2763.6	3019.5	5.5485	.003 956	2658.8	2896.2	5.3441				
600	.008 094	3022.6	3346.4	6.0114	.006 112	2942.0	3247.6	5.8178	.004 834	2861.1	3151.2	5.6452				
650	.009 063	3158.0	3520.6	6.2054	.006 966	3093.5	3441.8	6.0342	.005 595	3028.8	3364.5	5.8829				
700	.009 941	3283.6	3681.2	6.3750	.007 727	3230.5	3616.8	6.2189	.006 272	3177.2	3553.5	6.0824				
800	.011 523	3517.8	3978.7	6.6662	.009 076	3479.8	3933.6	6.5290	.007 459	3441.5	3889.1	6.4109				
900	.012 962	3739.4	4257.9	6.9150	.010 283	3710.3	4224.4	6.7882	.008 508	3681.0	4191.5	6.6805				
1000	.014 324	3954.6	4527.6	7.1356	.011 411	3930.5	4501.1	7.0146	.009 480	3906.4	4475.2	6.9127				
1100	.015 642	4167.4	4793.1	7.3364	.012 496	4145.7	4770.5	7.2184	.010 409	4124.1	4748.6	7.1195				
1200	.016 940	4380.1	5057.7	7.5224	.013 561	4359.1	5037.2	7.4058	.011 317	4338.2	5017.2	7.3083				
1300	.018 229	4594.3	5323.5	7.6969	.014 616	4572.8	5303.6	7.5808	.012 215	4551.4	5284.3	7.4837				

TABLE 4

<i>t</i> p (t Sat.) MPa	Liquid											
	0			2.5 (223.99)			5.0 (263.99)					
	<i>10<sup>3</sup>v</i>	<i>u</i>	<i>h</i>	<i>s</i>	<i>10<sup>3</sup>v</i>	<i>u</i>	<i>h</i>	<i>s</i>	<i>10<sup>3</sup>v</i>	<i>u</i>	<i>h</i>	<i>s</i>
Sat.												
0	1.0002	-0.03	-0.03	-0.0001	0.9990	-0.00	2.50	-0.0000	0.9977	0.04	5.04	0.0001
20	1.0018	83.95	83.95	0.2966	1.0006	83.80	86.30	0.2961	0.9995	83.65	88.65	0.2956
40	1.0078	167.56	167.56	0.5725	1.0067	167.25	169.77	0.5715	1.0056	166.95	171.97	0.5705
60	1.0172	251.12	251.12	0.8312	1.0160	250.67	253.21	0.8298	1.0149	250.23	255.30	0.8285
80	1.1291	334.87	334.87	1.0753	1.0280	334.29	336.86	1.0737	1.0268	333.72	338.85	1.0720
100	1.0436	418.96	418.96	1.3069	1.0423	418.24	420.85	1.3050	1.0410	417.52	422.72	1.3030
120	1.0604	503.57	503.57	1.5278	1.0590	502.68	505.33	1.5255	1.0576	501.80	507.09	1.5233
140	1.0800	588.89	588.89	1.7395	1.0784	587.82	590.52	1.7369	1.0768	586.76	592.15	1.7343
160	1.1024	675.19	675.19	1.9434	1.1006	673.90	676.65	1.9404	1.0988	672.62	678.12	1.9375
180	1.1283	762.72	762.72	2.1410	1.1261	761.16	763.97	2.1375	1.1240	759.63	765.25	2.1341
200	1.1581	851.8	851.8	2.3334	1.1555	849.9	852.8	2.3294	1.1530	848.1	853.9	2.3255
210	1.1749	897.1	897.1	2.4281	1.1720	895.0	898.0	2.4238	1.1691	893.0	898.8	2.4195
220	1.1930	943.0	943.0	2.5221	1.1898	940.7	943.7	2.5174	1.1866	938.4	944.4	2.5128
230	1.2129	989.6	989.6	2.6157	1.2092	987.0	990.1	2.6105	1.2056	984.5	990.6	2.6055
240	1.2347	1037.1	1037.1	2.7091	1.2305	1034.2	1037.2	2.7034	1.2264	1031.4	1037.5	2.6979
250	1.2590	1085.6	1085.6	2.8027	1.2540	1082.3	1085.4	2.7964	1.2493	1079.1	1085.3	2.7902
260	1.2862	1135.4	1135.4	2.8970	1.2804	1131.6	1134.8	2.8898	1.2749	1127.9	1134.3	2.8830
270	1.3173	1186.8	1186.8	2.9926	1.3102	1182.4	1185.7	2.9844	1.3036	1178.2	1184.3	2.9766
280	1.3535	1240.4	1240.4	3.0904	1.3447	1235.1	1238.5	3.0808	1.3365	1230.2	1236.8	3.0717
290	1.3971	1297.0	1297.0	3.1918	1.3855	1290.5	1294.0	3.1801	1.3750	1284.4	1291.3	3.1693
300	1.4520	1358.1	1358.1	3.2992	1.4357	1349.6	1353.2	3.2843	1.4214	1341.9	1349.0	3.2708
310									1.4803	1404.1	1411.5	3.3789

FIGURE 5.11a Extract from subcooled table (SI units).

TABLE A.4 (SI)  
Properties of Compressed Liquid (Steam)

T	P = 5 MPa (263.99)					P = 10 MPa (311.06)					P = 15 MPa (342.24)				
	v	u	h	s		v	u	h	s		v	u	h	s	
Sat.	.001 285 9	1147.8	1154.2	2.9202		.001 452 4	1393.0	1407.6	3.3596		.001 658 1	1585.6	1610.5	3.6848	
0	.000 997 7	.04	5.04	.0001		.000 995 2	.09	10.04	.0002		.000 992 8	.15	15.05	.0004	
20	.000 999 5	83.65	88.65	.2956		.000 997 2	83.36	93.33	.2945		.000 995 0	83.06	97.99	.2934	
40	.001 005 6	166.95	171.97	.5705		.001 003 4	166.35	176.38	.5686		.001 001 3	165.76	180.78	.5666	
60	.001 014 9	250.23	255.30	.8285		.001 012 7	249.36	259.49	.8258		.001 010 5	248.51	263.67	.8232	
80	.001 026 8	333.72	338.85	1.0720		.001 024 5	332.59	342.83	1.0688		.001 022 2	331.48	346.81	1.0656	
100	.001 041 0	417.52	422.72	1.3030		.001 038 5	416.12	426.50	1.2992		.001 036 1	414.74	430.28	1.2955	
120	.001 057 6	501.80	507.09	1.5233		.001 054 9	500.08	510.64	1.5189		.001 052 2	498.40	514.19	1.5145	
140	.001 076 8	586.76	592.15	1.7343		.001 073 7	584.68	595.42	1.7292		.001 070 7	582.66	598.72	1.7242	
160	.001 098 8	672.62	678.12	1.9375		.001 095 3	670.13	681.08	1.9317		.001 091 8	667.71	684.09	1.9260	
180	.001 124 0	759.63	765.25	2.1341		.001 119 9	756.65	767.84	2.1275		.001 115 9	753.76	770.50	2.1210	
200	.001 153 0	848.1	853.9	2.3255		.001 148 0	844.5	856.0	2.3178		.001 143 3	841.0	858.2	2.3104	
220	.001 186 6	938.4	944.4	2.5128		.001 180 5	934.1	945.9	2.5039		.001 174 8	929.9	947.5	2.4953	
240	.001 226 4	1031.4	1037.5	2.6979		.001 218 7	1026.0	1038.1	2.6872		.001 211 4	1020.8	1039.0	2.6771	
260	.001 274 9	1127.9	1134.3	2.8830		.001 264 5	1121.1	1133.7	2.8699		.001 255 0	1114.6	1133.4	2.8576	
280						.001 321 6	1220.9	1234.1	3.0548		.001 308 4	1212.5	1232.1	3.0393	
300						.001 397 2	1328.4	1342.3	3.2469		.001 377 0	1316.6	1337.3	3.2260	
320											.001 472 4	1431.1	1453.2	3.4247	
340											.001 631 1	1567.5	1591.9	3.6546	

TABLE A.4 (SI) (cont'd.)

T	P = 20 MPa (365.81)					P = 30 MPa					P = 50 MPa				
	v	u	h	s	s	v	u	h	s	s	v	u	h	s	s
Sat.	.002 036	1785.6	1826.3	4.0139		.000 985 6	.25	29.82	.0001		.000 976 6	.20	49.03	.0014	
0	.000 990 4	.19	20.01	.0004		.000 988 6	82.17	111.84	.2899		.000 980 4	81.00	130.02	.2848	
20	.000 992 8	82.77	102.62	.2923		.000 995 1	164.04	193.89	.5607		.000 987 2	161.86	211.21	.5527	
40	.000 999 2	165.17	185.16	.5646		.001 004 2	246.06	276.19	.8154		.000 996 2	242.98	292.79	.8052	
60	.001 008 4	247.68	267.85	.8206		.001 015 6	328.30	358.77	1.0561		.001 007 3	324.34	374.70	1.0440	
80	.001 019 9	330.40	350.80	1.0624		.001 029 0	410.78	441.66	1.2844		.001 020 1	405.88	456.89	1.2703	
100	.001 033 7	413.39	434.06	1.2917		.001 044 5	493.59	524.93	1.5018		.001 034 8	487.65	539.39	1.4857	
120	.001 049 6	496.76	517.76	1.5102		.001 062 1	576.88	608.75	1.7098		.001 051 5	569.77	622.35	1.6915	
140	.001 067 8	580.69	602.04	1.7193		.001 082 1	660.82	693.28	1.9096		.001 070 3	652.41	705.92	1.8891	
160	.001 088 5	665.35	687.12	1.9204		.001 104 7	745.59	778.73	2.1024		.001 091 2	735.69	790.25	2.0794	
180	.001 112 0	750.95	773.20	2.1147		.001 130 2	831.4	865.3	2.2893		.001 114 6	819.7	875.5	2.2634	
200	.001 138 8	837.7	860.5	2.3031		.001 159 0	918.3	953.1	2.4711		.001 140 8	904.7	961.7	2.4419	
220	.001 169 3	925.9	949.3	2.4870		.001 192 0	1006.9	1042.6	2.6490		.001 170 2	990.7	1049.2	2.6158	
240	.001 204 6	1016.0	1040.0	2.6674		.001 230 3	1097.4	1134.3	2.8243		.001 203 4	1078.1	1138.2	2.7860	
260	.001 246 2	1108.6	1133.5	2.8459		.001 275 5	1190.7	1229.0	2.9986		.001 241 5	1167.2	1229.3	2.9537	
280	.001 296 5	1204.7	1230.6	3.0248		.001 330 4	1287.9	1327.8	3.1741		.001 286 0	1258.7	1323.0	3.1200	
300	.001 359 6	1306.1	1333.3	3.2071		.001 399 7	1390.7	1432.7	3.3539		.001 338 8	1353.3	1420.2	3.2868	
320	.001 443 7	1415.7	1444.6	3.3979		.001 492 0	1501.7	1546.5	3.5426		.001 403 2	1452.0	1522.1	3.4557	
340	.001 568 4	1539.7	1571.0	3.6075		.001 626 5	1626.6	1675.4	3.7494		.001 483 8	1556.0	1630.2	3.6291	
360	.001 822 6	1702.8	1739.3	3.8772		.001 869 1	1781.4	1837.5	4.0012		.001 588 4	1667.2	1746.6	3.8101	
380															