16-CHEM-A2, UNIT OPERATIONS and SEPARATION PROCESSES

MAY 2017

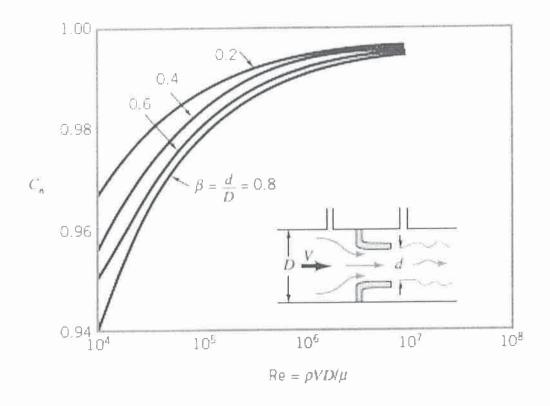
3 hours duration

NOTES

- 1. If doubt exists as to the interpretation of any question, the candidate is urged to submit with the answer paper, a clear statement of any assumptions made.
- 2. The examination is an **open book exam.** One textbook of your choice with notations listed on the margins etc., but no loose notes are permitted into the exam.
- 3. Candidates may use any non-communicating scientific calculator.
- 4. All problems are worth 25 points. At least **two problems** from **each** of parts **A** and **B** must be attempted.
- 5. Only the first two questions as they appear in the answer book from each section will be marked.

PART A: UNIT OPERATIONS

A1. Ethanol flows through a 60-mm diameter pipe in a refinery. The pressure drop across the nozzle meter used to measure the flowrate is to be 4 kPa when the flowrate is 3 x 10⁻³ m³/s. Determine the diameter of the nozzle.



Coefficient of Discharge (C_n) vs. Reynolds number (Re) for Nozzle Meters

"Measurement of Fluid Flow by Means of Orifice Plates, Nozzles, and Venturi Tubes Inserted in Circular Cross Section Conduits Running Full," Int. Organ. Stand. Rep. DIS-5167, Geneva, 1976.

<u>DATA</u>: Density of ethanol = 789 kg/m^3 Viscosity of ethanol = $1.19 \times 10^{-3} \text{ N.s/m}^2$

- A2. A Swenson-Walker crystallizer is to be used to produce 1 ton/hr of copperas (FeSO₄.7H₂O) crystals by cooling a saturated solution that enters the crystallizer at 120°F. The slurry leaving the crystallizer will be at 80°F. Cooling water enters the crystallizer jacket at 60°F and leaves at 70°F. At 120°F, the saturated solution contains 140 parts of copperas per 100 parts of excess water, and the saturated solution at 80°F contains 74 parts of copperas per 100 parts of excess water. It may be assumed that the overall heat transfer coefficient for the crystallizer is 35 BTU/hr.ft².°F. There are 3.5 ft² of cooling surface area per foot of crystallizer in length.
 - (a) [15 points] Estimate the cooling water required in gallons per minute.
 - (b) [10 points] Determine the number of crystallizer sections to be used.

Average specific heat capacity of initial solution = 0.70 BTU/lb °F Heat of solution of FeSO₄.7H₂O at 80°F = 28.5 BTU/lb

A3. A 6-inch plate-and-frame filter press using two frames, each 2 inches thick and having a total active filter area of 1 ft², is used to filter a slurry of calcium carbonate (CaCO₃) in water, and the following experimental data was obtained for constant-pressure filtration at a pressure difference of 30 lb_f/in² across the press:

Time of Filtration, in seconds	Weight of Filtrate, in pounds
0	0
26	5
98	10
211	15
361	20
555	25
788	30
1083	35

Determine the following based on the data obtained:

- (a) [15 points] The values of volume of filtrate and time required to form the cake.
- (b) [4 points] The value of the mean specific cake resistance.
- (c) [3 points] The value of the mean porosity of the cake.
- (d) [3 points] The value of the filter-medium resistance.

DATA:

Weight ratio of wet cake to dry cake = 1.473

Density of dry cake = $73.8 \text{ lb}_{\text{m}}/\text{ft}^3$

Weight fraction of $CaCO_3$ in slurry = 0.139

Viscosity of filtrate = 2.07 lb_m/ft.hr

Density of filtrate = $62.2 \text{ lb}_{\text{m}}/\text{ft}^3$

Density of filtrate = $164 \text{ lb}_{\text{m}}/\text{ft}^3$

PART B: SEPARATION PROCESSES

B1. In a batch reactor, 2.5 m³ of wastewater solution containing 0.25 kg of phenol/m³ is mixed with 3 kg of granular activated carbon until equilibrium is reached. The following experimental values were determined in a laboratory:

C _A , in g/cm ³	C _{A,S} , in grams solute per gram of activated carbon
0.004	0.026
0.0087	0.053
0.019	0.075
0.027	0.082
0.094	0.123
0.195	0.129

- (a) [5 points] Plot an adsorption isotherm.
- (b) [10 points] Determine the type of isotherm and calculate the isotherm parameters/constants.
- (c) [8 points] Calculate the steady-state values of C_A and $C_{A,S}$ in the batch reactor.
- (d) [2 points] Calculate the percentage of phenol that is recovered by the activated carbon adsorbent.

B2. A batch of sand was tray-dried with superheated steam and the following experimental data were obtained:

Drying Time, in hr	Total Moisture, in lb				
0.00	4.57				
0.25	4.29				
0.50	4.05				
0.75	3.84				
1.00	3.60				
1.25	3.37				
1.50	3.12				
1.75	2.91				
2.00	2.68				
2.25	2.47				
2.50	2.24				
2.75	2.02				
3.00	1.79				
3.25	1.56				
3.50	1.39				
3.75	1.18				
4.00	0.95				
4.25	0.78				
4.50	0.60				
4.75	0.48				
5.00	0.36				
5.50	0.26				
6.00	0.14				
6.50	0.07				
7.00	0.02				
7.50	0.00				

Obtain the drying-rate curve based on the experimental data.

B3. An air stream with an absolute humidity of 0.011 kg of water per kg of dry air is dried to a humidity of 0.002 kg of water per kg of dry air in an absorption tower packed with 2-inch Raschig rings. A 50% by weight sodium hydroxide (NaOH) solution is used. The equilibrium data for this system are presented in the following table:

X	Y			
(mole of H ₂ O/mole of NaOH)	(mole of H2O/mole of dry air)			
0	0			
1	4			
2	11			
3	28			
4	67			
5	100			
6	126			
7	142			
8	157			
9	170			
10	177			
12	190			
16	202			

If the flow of the absorbent solution is 25% larger than the minimum and the height of one transfer unit is 60 cm, calculate the height of the tower in order to carry out this operation.

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Table
Periodic
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18	Helium 2 2 He	10 10 Neon 20.18	Argon 18 Ar 39.95		Krypton 36	83.80	Xenon 54	Xe 131.29	Radon 86 Rn (222)	118 Uuo (294)
	11	Fluorine 9 F 19.00	Chiorine 17 C C 35.45		Bromine 35	Br 79.90	lodine 53	126.90	85 At (210)	Ununseptium 117 Uns (294?)
	16	0 0 16.00	Settur 16 S 32.07		Selenium 34	Se 78.96	Tellunum 52	Te 127.60	Polonium 84 PO (209)	Ununhexium 116 Uuh (293)
	15	Nitrogen 7 N 14.01	Phosphorus 15 P		Arsenic 33	AS 74.92	Antimony 51	Sb 121.76	Bismuth 83 83 208.98	Ununpentium 115 Uup (288)
	4	C C 12.01	Silicon 74 8i 8i 28.09		Germanium 32	Ge 72.61	in	Sn 118.71	R2 82 Pb 207.20	Und (289)
nI.	13	B 5 6 7 1 0 .81	Aluminum 13 AI 26.98		Gallium 31	Ga 69.72	Indium 49	In	### Thallium ### ################################	Ununtrium 113 Uut (284)
	*	Mass		12	Zinc 30	Zn 65.39	Cadmium 48	Cd 112.41	80 80 Hg 200.59	Copernicium 112 Cn (285)
	Atomic #	– Avg. Mass		7	Copper 29	Cu 63.55	Silver 47	Ag 107.87	Au 196.97	Roengenium 111 Rg (280)
	Sury	2 00.		10	Nicket 28	N 58.69	Palladium 46	Pd	Platinum 78 Pt 195.08	Damstadtium 110 DS (281)
	→ Mercury 80 ←	200.59		6	Сорап 27	Co 58.93	Rhodium 45	Rh 102.91	192.22	Metherium 109 Mt (276)
			r	œ	1ron 26	Fe 55.85	Ruthenium 44	Ru 101.07	Osmium 76 OS 190.23	Hassium 108 Hs (270)
	Element name.	`		7	Manganese 25	Mn 54.94	Technetium	Tc (98)	Rhenium 75 Re 186.21	Bonnum 107 Bh (272)
	Ele			9	Chromium 24	5 2.00	Molybdenum 42	Mo 95.94	Tungsten 74 W 183.84	Seaborgium 106 Sg (271)
	netals ils ii-metal)			r.	Vanadium 23	> 50.94	Niobium 41	Nb 92.91	Tantalum 73	105 105 Db (268)
	Alkali metals Alkaline earth metals Transition metals Other metals Metalloids (semi-metal)	Nonmetals Halogens Noble gases		4	Teanlum 22	Ti 47.88	Zirconium 40	Zr 91.22	Hatnium 72 Hf 178.49	Rutherfordium 104 Rf (267)
	Alka Alka Trar Oth	Non Nob		က	Scandium 21	Sc 44,96	Yttrium 39	88.91	71	Lawrencium 103 Lr (262)
			y						\$*	89-102
	6	Beryllium 4 Be 9.01	Magnesium 12 Mg)	Calcium 20	Ca 40.08	Strontium 38	ST 87.62	Barium 56 Ba 137.33	Radium 88 Ra (226)
-	Hydrogen 1.01	Li Li 6.94	11 11 Na 22 99		Potassium 19	39.10	Rubidium 37	Rb 85.47	Cesium 55 CS 132.91	Francium 87 Fr (223)
			100							

E 4	E ^
70 70 Yb 173.04	102 102 No (259)
Thullum 69 Tm 168.93	Mendelevium 101 Md (258)
Erbum 68 Er 167.26	Fermium 100 Fm (257)
Hoimium 67 HO 164.93	Einsteinium 99 ES (252)
Dysprosium 66 Dy 162.50	Californium 98 Cf (251)
Terbium 65 Tb 158.93	97 97 BK (247)
Gadolinium 64 Gd 157.25	Currum 96 CM (247)
Europium 63 Eu 151.97	Americium 95 Am (243)
Samarium 62 Sm 150.36	Prutonium 94 Pu (244)
Promethium 61 Pm (145)	93 Np (237)
Neodymium 60 Nd 144.24	Uranium 92 U 238.03
Praseodymium 59 Pr 140.91	91 91 Pa 231,04
Cenum 58 Ce 140.12	Thorium 90 Th 232,04
57 57 La 138.91	Actinium 89 AC (227)
*lanthanides	**actinides

