

National Exams May 2016

98-Pet-B5, Well Testing

3 hours duration

NOTES:

1. If doubt exists as to the interpretation of any question, the candidate is urged to submit with the answer paper, a clear statement of any assumptions made.
2. This is a CLOSED BOOK exam.
3. Any non-communicating calculator is permitted.
4. FIVE (5) questions constitute a complete exam paper.
5. The first five questions as they appear in the answer book will be marked.
6. All questions are of equal value unless otherwise stated and all parts in a multipart question have equal weight.
7. Clarity and organization of your answers are important, clearly explain your logic.
8. Pay close attention to units, some questions involve oilfield units, and these should be answered in the field units. Questions that are set in other units should be answered in the corresponding units.
9. A formula sheet is provided at the end of questions.

Question 1 (20 Marks)

Explain (briefly in one or two sentences or a simple equation) the following concepts.

- a) Wellbore storage
- b) Pulse test
- c) Diffusivity equation
- d) Back pressure test
- e) Non-Darcy flow
- f) Fall off test
- g) Line source approximation
- h) Superposition principle
- i) Pseudo radial flow
- j) Formation damage

Question 2 (20 Marks)

A downhole pressure gauge has been installed in an observation well located 330 ft away from an oil production well. Use the following reservoir data to calculate the production rate required to create 1 psi pressure drop at the observation well after 5 hours of production. Note: the production rate for the observation well is zero.

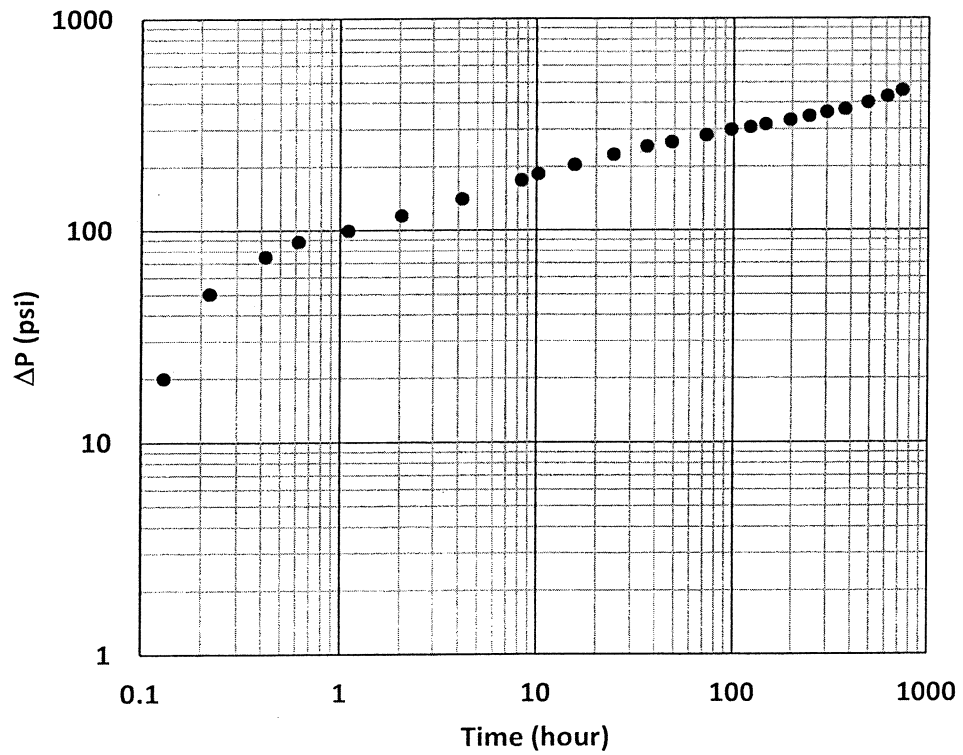
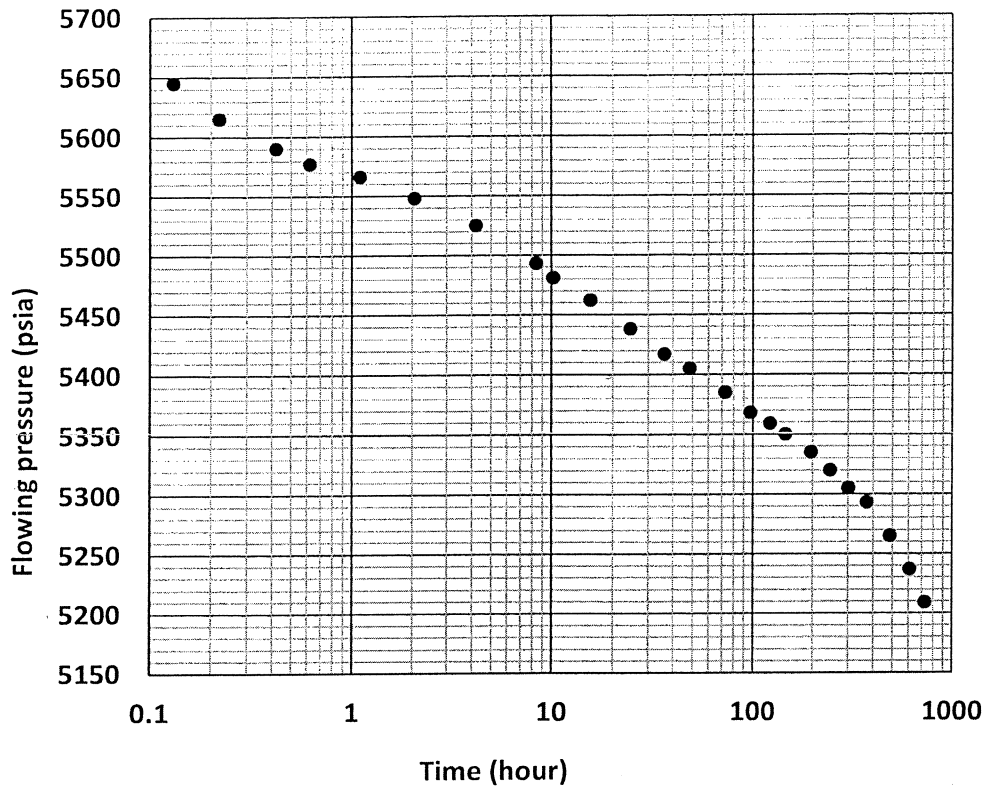
External radius, $r_e = 1452$ ft,
Wellbore radius, $r_w = 0.25$ ft,
Total compressibility, $c_t = 5 \times 10^{-5}$ psi⁻¹,
Oil viscosity, $\mu_o = 2$ cP,
Porosity, $\phi = 0.3$,
Permeability, $k = 2500$ mD,
Formation thickness, $h = 20$ ft,
Oil formation volume factor, $B_o = 1.2$ bbl/STB,
Initial pressure, $p_i = 3000$ psia.

Question 3 (20 Marks)

The drawdown test data of a discovery well in an oil reservoir are shown in the following. The well was produced at a single, constant rate of 550 STBD for a total time of 725 hours. Other reservoir and fluid properties data are as follows:

Formation thickness, $h = 20$ ft,
Initial reservoir pressure, $p_i = 5665$ psia,
Formation volume factor, $B_o = 1.45$ bbl/STB,
Porosity, $\phi = 0.23$,
Total compressibility, $c_t = 6 \times 10^{-5}$ psi⁻¹,
Oil viscosity, $\mu_o = 0.42$ cP,
Wellbore radius, $r_w = 0.5$ ft.

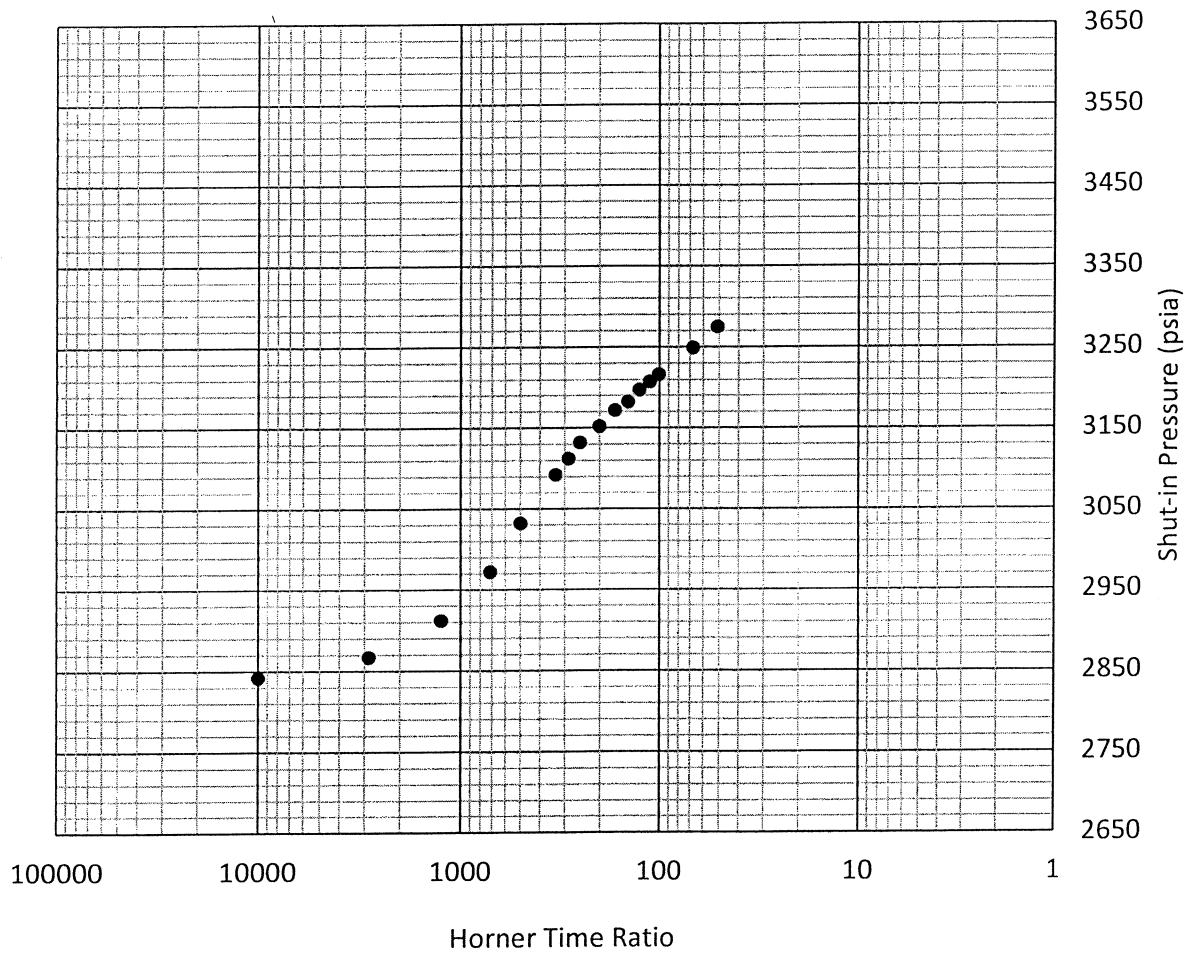
- a) Estimate reservoir permeability,
- b) Estimate the well skin factor,
- c) Estimate the end of wellbore storage,
- d) Do you suggest acidizing this well? Yes or No, and Why?



Question 4 (20 Marks)

A well in an oil reservoir was shut-in for a buildup test after producing 20,000 STB at a constant rate of 480 STBD. The shut-in pressures measured versus time are shown in the following. Calculate the effective permeability of the formation, the initial reservoir pressure, and skin factor.

- Flowing wellbore pressure prior to shut-in = 2832 psia,
- Formation thickness = 20 ft,
- Porosity = 18 %,
- Wellbore radius = 0.5 ft,
- Formation volume factor = 1.2 bbl/STB,
- Total compressibility = $2.6 \times 10^{-5} \text{ psi}^{-1}$,
- Oil viscosity = 1.5 cp.

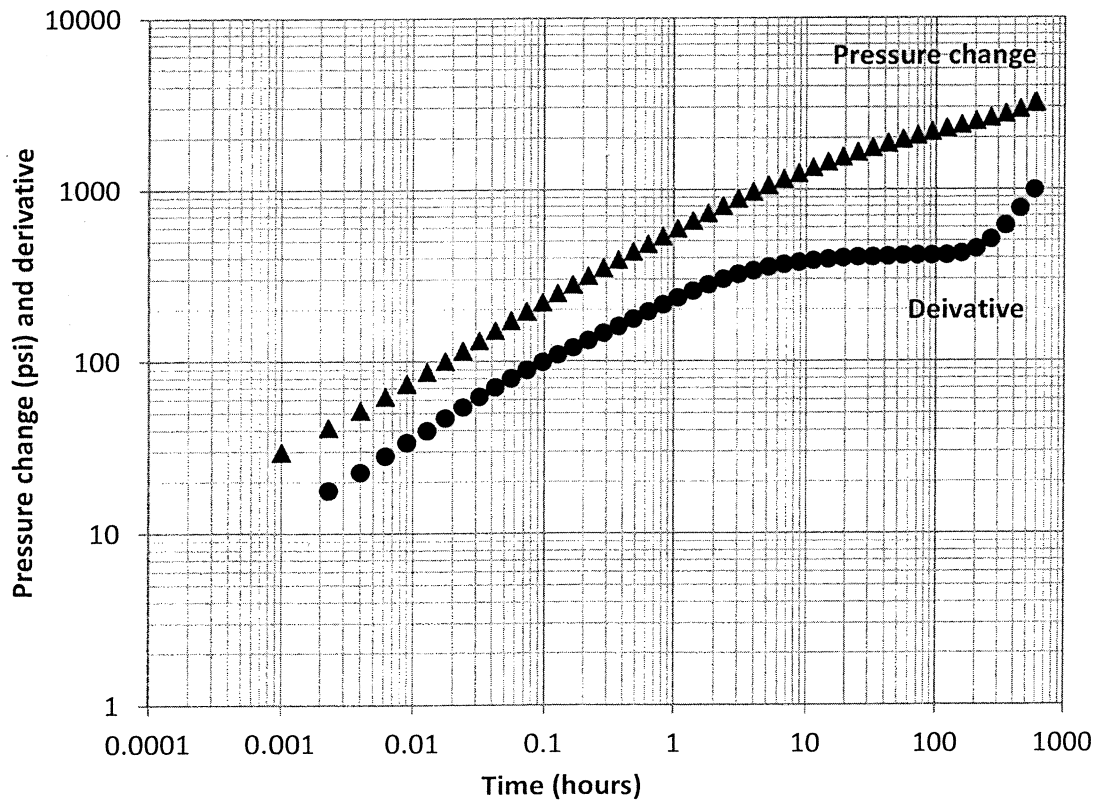


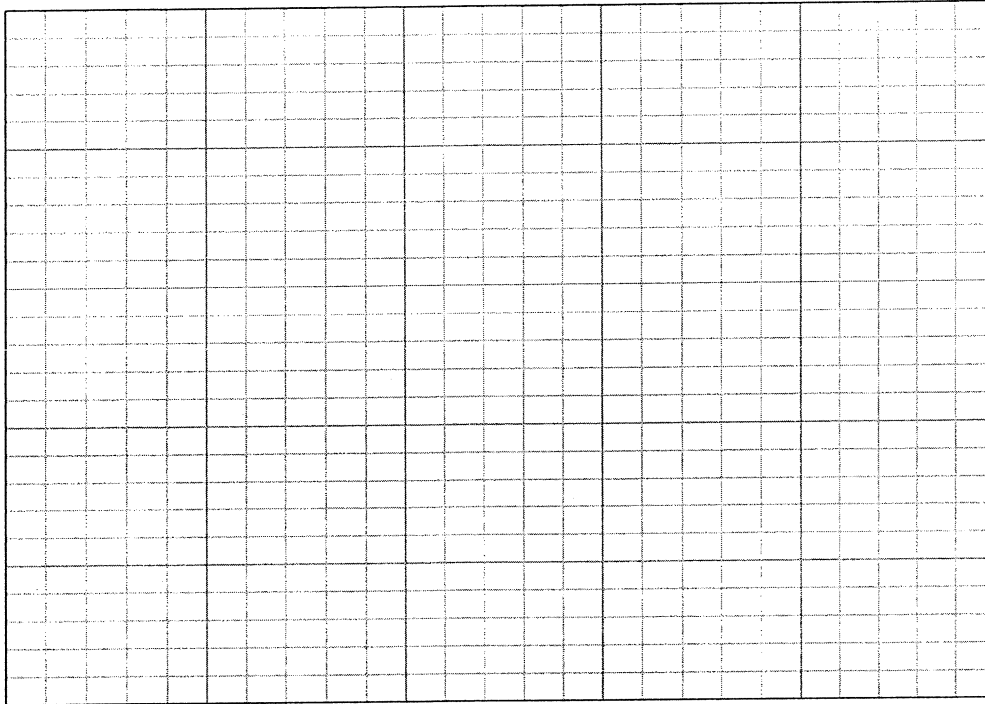
Question 6 (20 Marks)

Given the following formation and fluid properties, estimate fracture half-length from the drawdown test conducted in a fractured well interested with an infinite conductivity fracture. The pressure and pressure derivative data are also given in the following. Identify different flow regimes using the pressure change and pressure derivative plots given in the following.

$k=4$ mD; $q = 200$ STBD; $h = 12$ ft; $B_o = 1.325$ bbl/STB;
 $p_i = 3343.40$ psia; $\phi = 11.8\%$; $c_t = 14.7 \times 10^{-6}$ psi⁻¹; $r_w = 0.25$ ft;
 $\mu = 0.49$ cp.

Time (hours)	Flowing pressure (psia)
0.00	3343.4
0.0062	3280.78
0.0176	3243.17
0.0426	3192.27
0.0743	3148.39
0.1279	3095.23





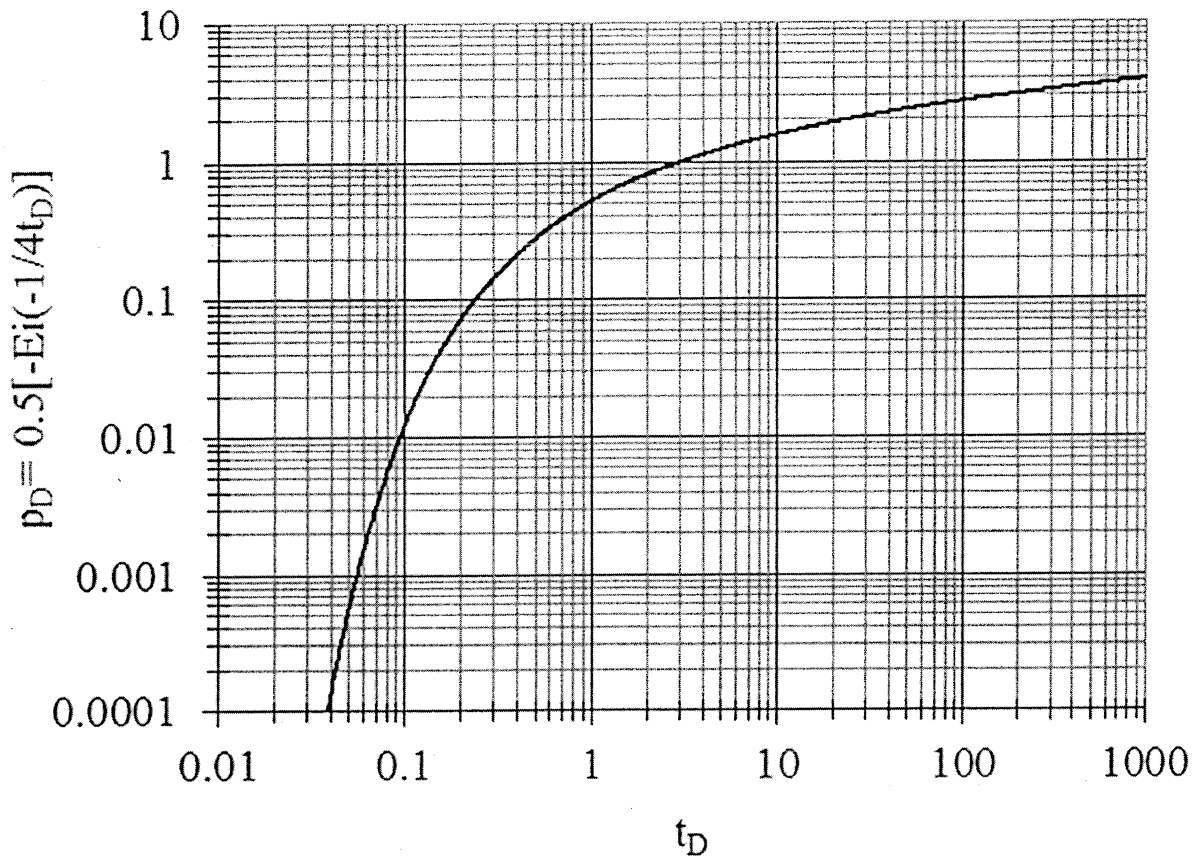
Question 7 (20 Marks)

A pressure build up test has been conducted on an oil well. The buildup pressure data versus time recorded during the test and other reservoir and fluid data are shown in the following. Use the given data to estimate the approximate end of wellbore storage and the dimensionless wellbore storage coefficient.

Flowing wellbore pressure prior to shut-in = 2832 psia,
 Formation thickness = 20 ft,
 Porosity = 18 %,
 Wellbore radius = 0.5 ft,
 Formation volume factor = 1.2 bbl/STB,
 Total compressibility = 2.6×10^{-5} psi⁻¹,
 Production rate = 50 STBD,
 Oil viscosity = 1.5 cp.

Time (hours)	Pressure (psia)
0.10	2842
0.35	2867
0.80	2912
1.40	2972
2.00	3032
5.00	3152
9.00	3207
20.00	3275

A large grid of empty cells, likely a table or spreadsheet, occupying the central portion of the page. The grid is composed of approximately 20 columns and 20 rows of small, uniform cells. The lines are thin and black, creating a clear structure for data entry.



Plot of dimensionless pressure versus dimensionless time

Formula Sheet

Pressure solution for infinite acting reservoirs:

$$p(r,t) = p_i - \frac{q\mu B_o}{0.00708kh} p_D, \quad \eta = \frac{0.0002637k}{\phi\mu c_i}, \quad t_D = \frac{\eta t}{r^2}$$

$$p_D = \frac{1}{2}(\ln t_D + 0.809) \text{ only if } t_D > 100, \text{ for } t_D < 100 \text{ use the provided } p_D \text{ graph.}$$

Pseudo steady state equations: $\frac{dp_w}{dt} = -\frac{0.234qB_o}{c_i V_p}$, (psi/hr)

$$p(r_w,t) = p_i - \frac{0.0744qB_o t}{\phi c_i h r_e^2} - \frac{q\mu B_o}{0.00708kh} \left[\ln\left(\frac{r_e}{r_w}\right) - \frac{3}{4} + S \right]$$

Slope of semi-log straight line, psi/cycle: $m = \frac{162.6q\mu B_o}{kh}$

Radius of investigation, ft: $r \approx \sqrt{\frac{kt}{948\phi\mu c_i}}$

Permeability-thickness product for double porosity reservoirs, mD-ft: $(kh)_f = \hat{k}_f h = \frac{162.6q\mu B}{m}$

Average fracture permeability, mD: $\hat{k}_f = \hat{k}_f h / h$

Skin factor for buildup test: $S = 1.151 \left(\frac{p(1hr) - p_{wf}(\Delta t = 0)}{|m|} - \log\left(\frac{k}{\phi\mu c_i r_w^2}\right) + 3.23 \right)$

Skin factor for drawdown test: $S = 1.151 \left(\frac{p_i - p(1hr)}{|m|} - \log\left(\frac{k}{\phi\mu c_i r_w^2}\right) + 3.23 \right)$

Horner time ratio: $\frac{t_p + \Delta t}{\Delta t}$

Distance to fault, ft: $L = \sqrt{\frac{0.000148k\Delta t}{\phi\mu c_i}}$

The approximate time required for the slope to double, hr: $\Delta t = \frac{3.8 \times 10^5 \phi\mu c_i L^2}{k}$

Gas wells build up:

$$m = \frac{1637q_g T}{kh}$$

$$S' = 1.151 \left(\left(\frac{p_{p1hr} - p_{pwf}(@\Delta t = 0)}{m} \right) - \log\left(\frac{k}{\phi\mu c_i r_w^2}\right) + 3.23 \right)$$

Fracture half length:

$$L_f = \frac{4.064qB_o}{mh\sqrt{k}} \left(\frac{\mu_o}{\phi c_t} \right)^{0.5}, L_f = 2r_w e^{-S}$$

Wellbore storage coefficient:

$$C = \frac{qB}{24} \left(\frac{\Delta t_e}{\Delta p} \right)_{USL} \text{ in } bbl / psi$$

Dimensionless wellbore storage coefficient:

$$C_D = \frac{0.8939C}{\phi c_t hr_w^2}$$

Nomenclature

B_o	Oil formation volume factor	bbbl/STB
c_t	Total compressibility	1/psi
h	Formation thickness	ft
k	Permeability	mD
L	Distance	ft
P	Pressure	psia
p_p	Pseudo pressure	psia ² /cP
q	Oil flow rate	STBD
q_g	Gas flow rate	MSCFD
r	Radius	ft
S	Skin factor	dimensionless
T	Temperature	Rankin
t	Time	hr
V_p	Pore volume	ft ³

Greek letters

ϕ	Porosity	fraction
μ	Oil viscosity	cP
η	Hydraulic diffusivity	ft ² /hr

Subscripts

D	dimensionless
e	external
f	fracture
i	initial
o	oil
p	production
t	total
w	wellbore

Conversion Factors

1 m ³	= 6.28981 bbl = 35.3147 ft ³
1 acre	= 43560 ft ²
1 ac-ft	= 7758 bbl
1 Darcy	= 9.869233 × 10 ⁻¹³ m ²
1 atm	= 14.6959488 psi = 101.32500 kPa = 1.01325 bar
1 cP	= 0.001 Pa-sec
1 m	= 3.28084 ft = 39.3701 inch