

16-CHEM-A2, UNIT OPERATIONS and SEPARATION PROCESSES

National Exams MAY 2019

3 hours duration

NOTES

1. If doubt exists as to the interpretation of any question, the candidate is urged to submit with the answer paper, a clear statement of any assumptions made.
2. The examination is an **open book exam**. One textbook of your choice with notations listed on the margins etc., but no loose notes are permitted into the exam.
3. Candidates may use any **non-communicating** calculator.
4. All problems are worth 25 points. **Two problems** from **each** of parts **A** and **B** must be attempted.
5. **Only the first two** questions from each section as they appear in the answer book will be marked.
6. State all assumptions clearly.

PART A: UNIT OPERATIONS

- A1. A batch centrifugal filter having a diameter of 750 mm and a height of 450 mm is used to filter a suspension (solids in water) at 25 °C having the following properties:

Concentration of solids in the feed = 60 g/L

Density of dry solid in the cake = 2000 kg/m³

Porosity of cake = 0.435

Final thickness of cake = 15 cm

Specific cake resistance = 9.5×10^{10} ft/lb

Filter medium resistance = 2.6×10^{10} ft⁻¹

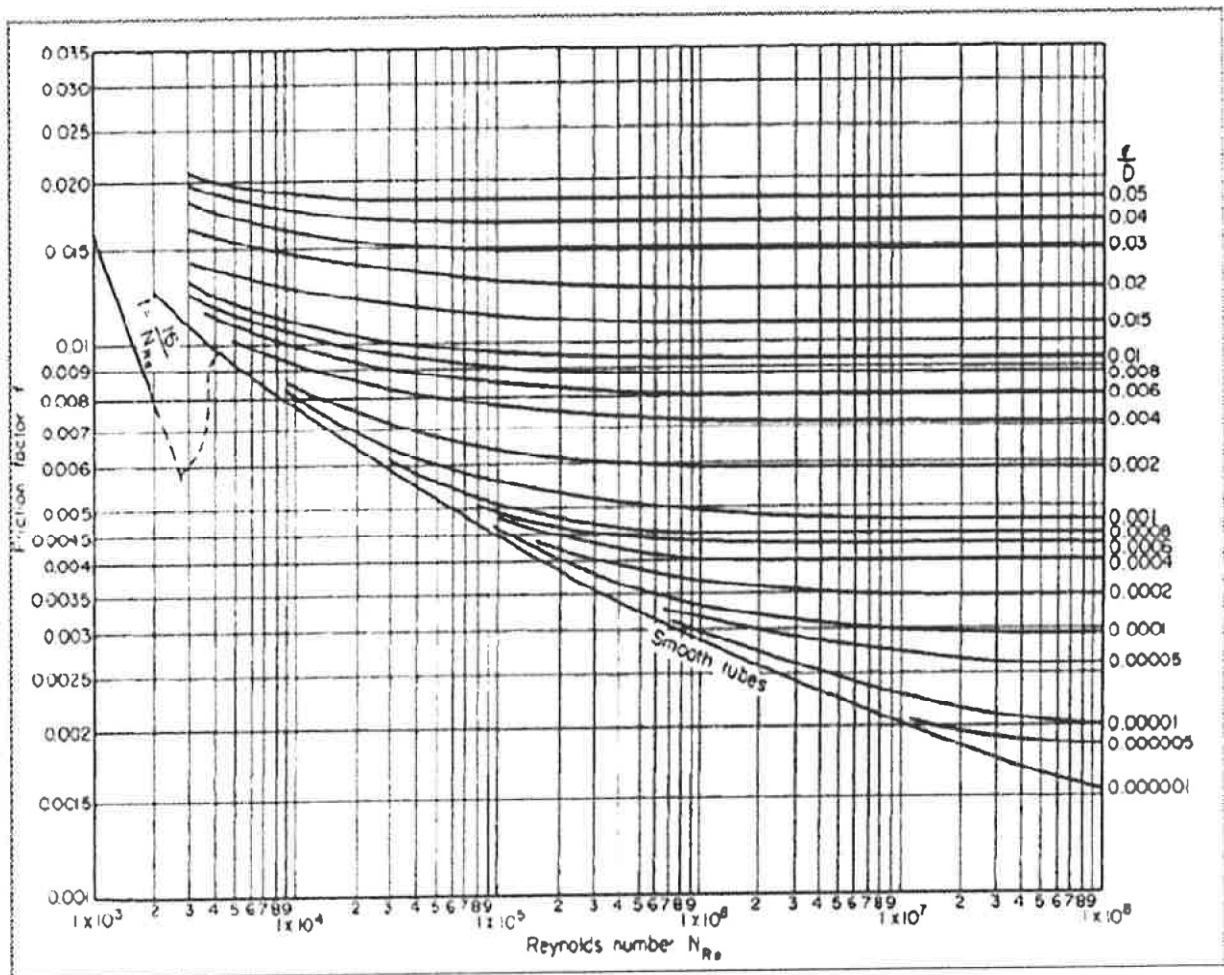
Speed of centrifuge filter = 2000 rpm

The cake is washed with water under such conditions that the radius of the inner surface of the liquid is 200 mm. Assuming that the rate of flow of wash water equals the final flow rate of filtrate, calculate the rate of washing in cubic meters per hour.

DATA: Viscosity of water = 0.9cP = 9×10^{-4} Pa.s

Density of water = 998 kg/m³

- A2. A liquid (specific gravity = 2.6, viscosity = 2×10^{-3} Pa.s) flows through a hydraulically smooth long pipe of unknown diameter, resulting in a pressure drop of $0.183 \text{ lb}_f/\text{in}^2$ over a distance of 2.784 kilometers. Calculate the diameter of the pipe in inches if the mass flow rate of the liquid is 3,175 kg/hr.



Fanning friction factor (f) vs. Reynolds number (Re) for pipes

Transactions of the American Society of Mechanical Engineers, vol. 66, p.672 (1944)

- A3. The pressure drop of water flowing through a bed of 20-mesh to 50-mesh resin (assume spherical particles) is said to be proportional to the flow rate and has a published value of 0.8 lb_f per square inch per foot at a flow rate of 10 gallons per minute per square foot.
- (a) [7.5 points] Predict the pressure drop using an arithmetic average particle size and a bed void fraction of 0.35.
- (b) [10 points] What average particle size would be needed for agreement with the published value of pressure drop?
- (c) [7.5 points] What void fraction would be needed for agreement with the published value of pressure drop?

DATA: Viscosity of water = 1 cP = 1×10^{-3} Pa.s
 Density of water = 1000 kg/m^3

PART B: SEPARATION PROCESSES

- B1.** 100 moles of a saturated liquid feed containing 40 mol% acetone and 60 mol% ethanol is to be separated in a packed tower into an overhead product containing 85% acetone and a bottom product containing 5% acetone. The distillation is to be carried out at 1 atm using the following acetone-ethanol vapor-liquid equilibrium data:

| Temperature (K) | Liquid Mole Fraction of Acetone | Vapor Mole Fraction of Acetone |
|-----------------|------------------------------------|-----------------------------------|
| 351.45 | 0.000 | 0.000 |
| 349.55 | 0.033 | 0.111 |
| 347.15 | 0.078 | 0.216 |
| 343.95 | 0.149 | 0.345 |
| 342.25 | 0.195 | 0.410 |
| 338.75 | 0.316 | 0.534 |
| 336.55 | 0.414 | 0.614 |
| 334.45 | 0.532 | 0.697 |
| 332.15 | 0.691 | 0.796 |
| 330.45 | 0.852 | 0.896 |
| 329.25 | 1.000 | 1.000 |

The local mass transfer coefficients for this process are

$$k'_y a = 0.2 \text{ kmol/m}^3 \cdot \text{s (mole fraction)}$$

$$k'_x a = 1.6 \text{ kmol/m}^3 \cdot \text{s (mole fraction)}$$

Assuming equal molar overflow, using a total condenser and reflux ratio of $L/D = 2.5$, determine the number of transfer units to perform the separation.

- B2.** Solute A is to be recovered from an inert carrier gas B by absorption into a non-volatile solvent. The gas mixture enters the absorber at a rate of 500 kmol/hr containing 30% by mole of A, and leaves the absorber with 1% by mole of A. Solvent enters the absorber at a rate of 1500 kmol/hr containing 0.1% by mole of A. The equilibrium relationship is the vapor phase mole fraction of A is 2.8 times the liquid phase mole fraction of A. The carrier gas is insoluble in the solvent. Compute and then construct x-y plot of equilibrium line and operating line on one graph using solute-free coordinates.

- B3. The adsorption of sulfur dioxide (SO₂) on mordenite zeolite was studied at 0 °C and the following data was obtained:

| Pressure of SO ₂ , in mm Hg | SO ₂ Uptake, in mmol/g |
|--|-----------------------------------|
| 5 | 1.75 |
| 10 | 2.20 |
| 15 | 2.40 |
| 20 | 2.62 |
| 30 | 2.75 |
| 40 | 2.85 |
| 50 | 3.00 |
| 60 | 3.05 |
| 70 | 3.12 |

- (a) [20 points] Determine which isotherm fits the data and then evaluate the isotherm constants.
- (b) [5 points] Calculate the total surface area of the solid.

DATA: Avagadro's number = 6.023×10^{23} molecules/mole
Density of liquid SO₂ at 0 °C in the adsorbed phase = 1430 kg/m³

APPENDIX D

PARTICLE SIZE—U.S. SIEVE SIZE AND TYLER SCREEN MESH EQUIVALENTS

In the multiphase combustion area, we often encounter unburned and partially burned particles of different sizes. In the United States, these sizes are often expressed in a standard measured quantity in terms of either U.S. Sieve Size or Tyler Screen Mesh. Sieving or screening is a method of separating a mixture of particles (or grains) into two or more size fractions (see Tables E.1 and E.2). The over size particles are trapped above the screen while undersize particles can pass through the screen. Sieves can be used in stacks, to divide samples up into various size fractions and hence determine particle size distributions. Sieves and screen usually are used for larger particle sizes, $d_p \geq 37 \mu\text{m}$ (0.037mm).

TABLE D.1. Standard U.S. Sieve Sizes and Tyler Mesh Sizes

| U.S. Sieve Size | Tyler Mesh Size | Opening (mm) | Opening (in) |
|-----------------|-----------------|--------------|--------------|
| — | 2½ mesh | 8.00 | 0.312 |
| — | 3 mesh | 6.73 | 0.265 |
| No. 3½ | 3½ mesh | 5.66 | 0.233 |
| No. 4 | 4 mesh | 4.76 | 0.187 |
| No. 5 | 5 mesh | 4.00 | 0.157 |
| No. 6 | 6 mesh | 3.36 | 0.132 |
| No. 7 | 7 mesh | 2.83 | 0.111 |
| No. 8 | 8 mesh | 2.38 | 0.0937 |
| No. 10 | 9 mesh | 2.00 | 0.0787 |
| No. 12 | 10 mesh | 1.68 | 0.0661 |
| No. 14 | 12 mesh | 1.41 | 0.0555 |
| No. 16 | 14 mesh | 1.19 | 0.0469 |
| No. 18 | 16 mesh | 1.00 | 0.0394 |
| No. 20 | 20 mesh | 0.841 | 0.0331 |
| No. 25 | 24 mesh | 0.707 | 0.0278 |
| No. 30 | 28 mesh | 0.595 | 0.0234 |
| No. 35 | 32 mesh | 0.500 | 0.0197 |
| No. 40 | 35 mesh | 0.420 | 0.0165 |
| No. 45 | 42 mesh | 0.354 | 0.0139 |
| No. 50 | 48 mesh | 0.297 | 0.0117 |
| No. 60 | 60 mesh | 0.250 | 0.0098 |
| No. 70 | 65 mesh | 0.210 | 0.0083 |
| No. 80 | 80 mesh | 0.177 | 0.0070 |
| No. 100 | 100 mesh | 0.149 | 0.0059 |
| No. 120 | 115 mesh | 0.125 | 0.0049 |
| No. 140 | 150 mesh | 0.105 | 0.0041 |
| No. 170 | 170 mesh | 0.088 | 0.0035 |
| No. 200 | 200 mesh | 0.074 | 0.0029 |
| No. 230 | 250 mesh | 0.063 | 0.0025 |
| No. 270 | 270 mesh | 0.053 | 0.0021 |
| No. 325 | 325 mesh | 0.044 | 0.0017 |
| No. 400 | 400 mesh | 0.037 | 0.0015 |

