

17-Phys-B6, Applied Thermodynamics and Heat Transfer

3 Hours Duration

Notes :

1. If doubt exists concerning the interpretation of any question, the candidate is urged to make assumptions and clearly explain what has been assumed along with the answer to the question.
2. The examination is open book. As a consequence, candidates are permitted to make use of any textbooks, references or notes.
3. Any non-communicating calculator is permitted. However, candidates must indicate the type of calculator(s) that they have used by writing the name and model designation of the calculator(s) on the inside of the cover of the first examination book.
4. It is expected that each candidate will have copies of both a thermodynamics text and a heat transfer text in order to make use of the information presented in the tables and graphs contained.
5. The answers to five questions, either three questions from Part A and two questions from Part B or two questions from Part A and three questions from Part B, comprise a complete examination.
6. Candidates must indicate the answers that they wish to have graded on the cover of the first examination book. Otherwise the answers will be graded in the order in which they appear in the examination book(s) up to a maximum of three answers per section.
7. The answer to any question carries the same value in the grading.

PART A - THERMODYNAMICS

1. (a) A closed vessel containing 0.06 m³ of air at 40 atmospheres and 40°C is connected with another closed vessel containing 1.35 kg of argon at 7 atmospheres. When the valve separating these vessels is opened, the pressure of the mixture is 18 atmospheres and its temperature is 30°C. Determine the volume of the vessel containing the argon and the temperature of the argon prior to mixing.

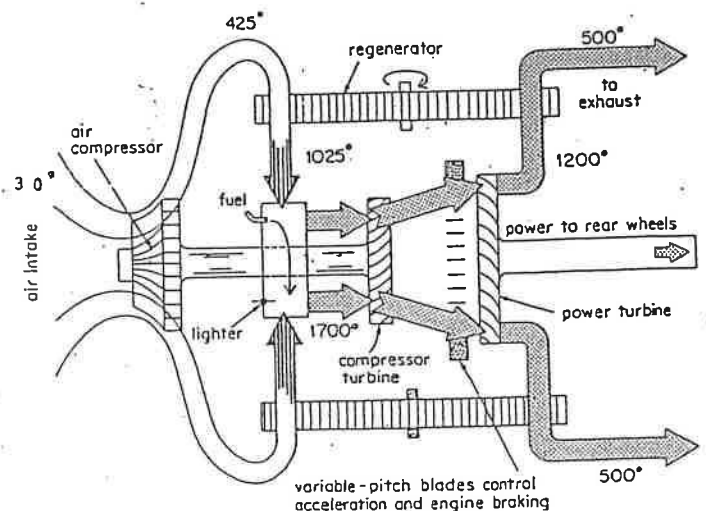
(b) A machine operates on an ideal cycle comprised of isentropic compression of the working substance, isometric heat addition to the working substance, isentropic expansion of the working substance and isometric heat rejection from the working substance. The working substance is assumed to be air with $\gamma = 1.4$ and $R = 0.287$ kJ/kgK. At the beginning of the compression process, the pressure is 138 kPa and the temperature is 37°C. The compression ratio is 8:1 and the maximum temperature in the cycle is 1772 K. Compute the other temperatures and pressures and indicate these values on a P-v and a T-s diagram for the cycle. What is the thermal efficiency of the cycle? Determine the power output corresponding to a heat addition of 370 W.

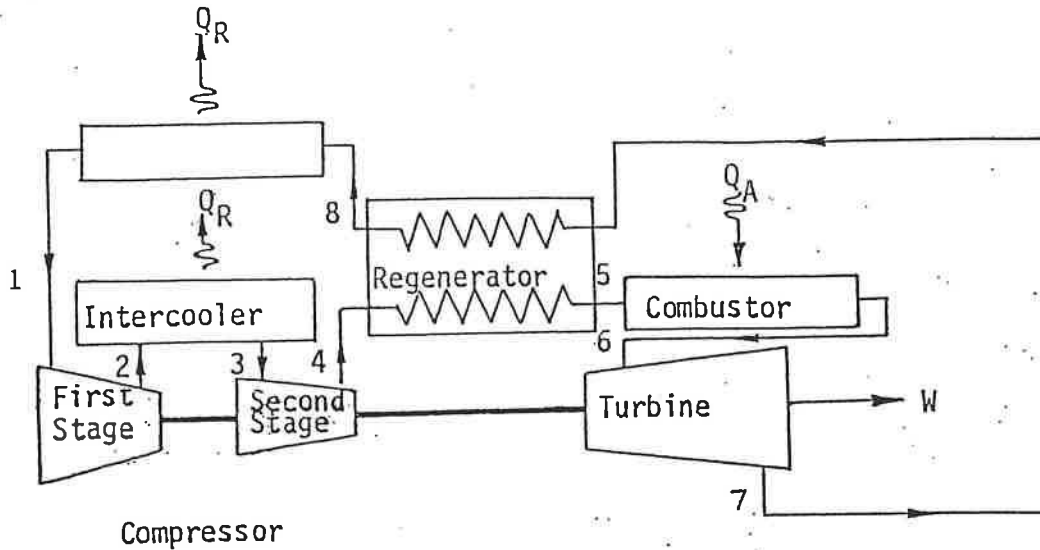
2. (a) Steam under a pressure of 1 MPa enters a throttling calorimeter and emerges as superheated steam at atmospheric pressure with a temperature of 150°C. What is the quality of the wet steam?

(b) The steam enters a turbine with a velocity of 1.5 m/s and leaves at 7.5 kPa and 78.3% quality with a velocity of 90 m/s while the heat loss is 527 W and the flowrate is 0.45 kg/s. What power will be developed?

(c) It can easily be seen by consulting the steam tables that the process is isentropic, despite the fact that heat was lost by the turbine. Explain how this is possible.

3. The diagram at the right is illustrative of a gas turbine power plant being developed for use in an automobile. Assuming that the temperatures indicated have been expressed in degrees Celsius (a) draw a schematic diagram for the gas turbine power plant (b) indicate each of the processes on a T-s diagram (c) calculate the thermal efficiency for the operating conditions given and (d) determine the air flowrate required to develop 50 kW at the rear axle of the car.



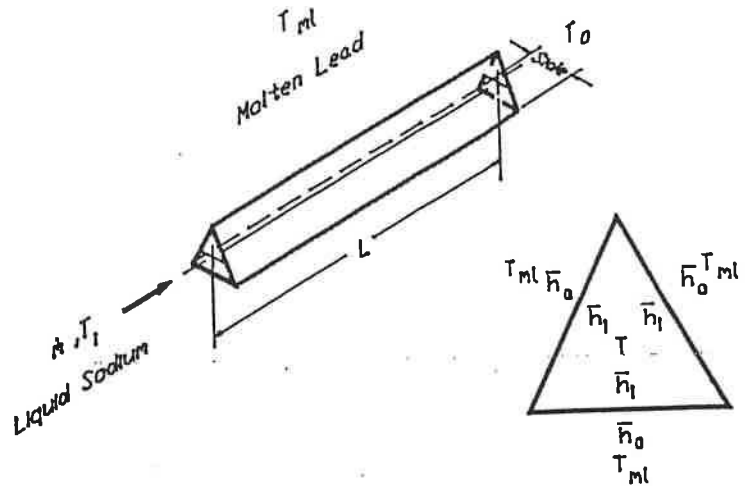


4. An ice-making refrigeration plant having a capacity of 70 kW of refrigeration operates with ammonia as the refrigerant. The evaporator operates at -15°C and the ammonia condenses at 31°C . Assuming that the compressor has an efficiency of 95% and neglecting piping losses, determine the power required per kW of refrigeration and the coefficient of performance. If cooling water enters the condenser at 20°C and leaves the condenser at 27°C , what cooling water flowrate is required ?

PART B - HEAT TRANSFER

5. A steel tube 150 mm I.D. x 10 mm W.T. conveys wet steam at 200°C and is surrounded by air at 27°C . The loss of heat under these conditions is 2000 W per metre of length. Determine the loss of heat when the pipe is covered by a 50 mm thick layer of insulation, when the conductivities of the insulation and the pipe are respectively $0.35 \text{ W/m}^{\circ}\text{C}$ and $45 \text{ W/m}^{\circ}\text{C}$ and the heat transfer coefficient between metal and air is 40% greater than the heat transfer coefficient between insulation and air.
6. Heat is generated in a 75 mm diameter cylindrical electrical conductor made of a material having a thermal conductivity of $70 \text{ W/m}^{\circ}\text{C}$ which is located in a fluid having a temperature of 27°C . The surface heat transfer coefficient is $568 \text{ W/m}^2 \text{ }^{\circ}\text{C}$ and the temperature must not exceed 540°C anywhere in the cylinder.
- (a) Determine the maximum heat generation rate per unit length.
- (b) Determine the surface temperature under these conditions.

7. A device is to be built that will be capable of transferring heat from a pool of molten lead at 600 K to liquid sodium at 478 K entering an equilateral triangular duct immersed in the pool which is 4 m long by 3 cm on a side. The liquid sodium flows through the duct at 3.6 kg/s and the specific heat of liquid sodium is 1340 J/kg°C. Given that the heat transfer coefficient inside the duct $\bar{h}_i = 89,140 \text{ W/m}^2\text{°C}$ and that the heat transfer coefficient outside the duct $\bar{h}_o = 8687 \text{ W/m}^2\text{°C}$, determine



- (i) the temperature at which the liquid sodium leaves the duct
- (ii) the heat transfer between the molten lead and the liquid sodium
8. Water flowing at 10 kg/s through 50 brass tubes 2.3 cm ID by 2.6 cm OD heats air flowing at 1.6 kg/s through a shell within which the tubes are located in parallel. Each tube is 6.7 m long. The heat transfer coefficients inside and outside the tubes are $470 \text{ W/m}^2\text{°C}$ and $210 \text{ W/m}^2\text{°C}$ respectively. The water enters the tubes at 75°C and the air enters the shell at 15°C . Determine the heat exchanger effectiveness, the rate of heat transfer between the water and the air and the outlet temperatures of the water and the air.

Thermodynamic Properties of Ammonia

Saturated Ammonia

| Temp. °C | Abs. Press. kPa P | Specific Volume m ³ /kg | | | Enthalpy kJ/kg | | | Entropy kJ/kg K | | |
|-------------|----------------------------|--|--------------------------------|---------------------------------------|--|--------------------------------|---------------------------------------|--|--------------------------------|---------------------------------------|
| | | Sat. Liquid <i>v_f</i> | Evap. <i>v_{fg}</i> | Sat. Vapor <i>v_g</i> | Sat. Liquid <i>h_f</i> | Evap. <i>h_{fg}</i> | Sat. Vapor <i>h_g</i> | Sat. Liquid <i>s_f</i> | Evap. <i>s_{fg}</i> | Sat. Vapor <i>s_g</i> |
| -50 | 40.88 | 0.001 424 | 2.6239 | 2.6254 | -44.3 | 1416.7 | 1372.4 | -0.1942 | 6.3502 | 6.1561 |
| -48 | 45.96 | 0.001 429 | 2.3518 | 2.3533 | -35.5 | 1411.3 | 1375.8 | -0.1547 | 6.2696 | 6.1149 |
| -46 | 51.55 | 0.001 434 | 2.1126 | 2.1140 | -26.6 | 1405.8 | 1379.2 | -0.1156 | 6.1902 | 6.0746 |
| -44 | 57.69 | 0.001 439 | 1.9018 | 1.9032 | -17.8 | 1400.3 | 1382.5 | -0.0768 | 6.1120 | 6.0352 |
| -42 | 64.42 | 0.001 444 | 1.7155 | 1.7170 | -8.9 | 1394.7 | 1385.8 | -0.0382 | 6.0349 | 5.9967 |
| -40 | 71.77 | 0.001 449 | 1.5506 | 1.5521 | 0.0 | 1389.0 | 1389.0 | 0.0000 | 5.9589 | 5.9589 |
| -38 | 79.80 | 0.001 454 | 1.4043 | 1.4058 | 8.9 | 1383.3 | 1392.2 | 0.0380 | 5.8840 | 5.9220 |
| -36 | 88.54 | 0.001 460 | 1.2742 | 1.2757 | 17.8 | 1377.6 | 1395.4 | 0.0757 | 5.8101 | 5.8858 |
| -34 | 98.05 | 0.001 465 | 1.1582 | 1.1597 | 26.8 | 1371.8 | 1398.5 | 0.1132 | 5.7372 | 5.8504 |
| -32 | 108.37 | 0.001 470 | 1.0547 | 1.0562 | 35.7 | 1365.9 | 1401.6 | 0.1504 | 5.6652 | 5.8156 |
| -30 | 119.55 | 0.001 476 | 0.9621 | 0.9635 | 44.7 | 1360.0 | 1404.6 | 0.1873 | 5.5942 | 5.7815 |
| -28 | 131.64 | 0.001 481 | 0.8790 | 0.8805 | 53.6 | 1354.0 | 1407.6 | 0.2240 | 5.5241 | 5.7481 |
| -26 | 144.70 | 0.001 487 | 0.8044 | 0.8059 | 62.6 | 1347.9 | 1410.5 | 0.2605 | 5.4548 | 5.7153 |
| -24 | 158.78 | 0.001 492 | 0.7373 | 0.7388 | 71.6 | 1341.8 | 1413.4 | 0.2967 | 5.3864 | 5.6831 |
| -22 | 173.93 | 0.001 498 | 0.6768 | 0.6783 | 80.7 | 1335.6 | 1416.2 | 0.3327 | 5.3188 | 5.6515 |
| -20 | 190.22 | 0.001 504 | 0.6222 | 0.6237 | 89.7 | 1329.3 | 1419.0 | 0.3684 | 5.2520 | 5.6205 |
| -18 | 207.71 | 0.001 510 | 0.5728 | 0.5743 | 98.8 | 1322.9 | 1421.7 | 0.4040 | 5.1860 | 5.5900 |
| -16 | 226.45 | 0.001 515 | 0.5280 | 0.5296 | 107.8 | 1316.5 | 1424.4 | 0.4393 | 5.1207 | 5.5600 |
| -14 | 246.51 | 0.001 521 | 0.4874 | 0.4889 | 116.9 | 1310.0 | 1427.0 | 0.4744 | 5.0561 | 5.5305 |
| -12 | 267.95 | 0.001 528 | 0.4505 | 0.4520 | 126.0 | 1303.5 | 1429.5 | 0.5093 | 4.9922 | 5.5015 |
| -10 | 290.85 | 0.001 534 | 0.4169 | 0.4185 | 135.2 | 1296.8 | 1432.0 | 0.5440 | 4.9290 | 5.4730 |
| -8 | 315.25 | 0.001 540 | 0.3863 | 0.3878 | 144.3 | 1290.1 | 1434.4 | 0.5785 | 4.8664 | 5.4449 |
| -6 | 341.25 | 0.001 546 | 0.3583 | 0.3599 | 153.5 | 1283.3 | 1436.8 | 0.6128 | 4.8045 | 5.4173 |
| -4 | 368.90 | 0.001 553 | 0.3328 | 0.3343 | 162.7 | 1276.4 | 1439.1 | 0.6469 | 4.7432 | 5.3901 |
| -2 | 398.27 | 0.001 559 | 0.3094 | 0.3109 | 171.9 | 1269.4 | 1441.3 | 0.6808 | 4.6825 | 5.3633 |
| 0 | 429.44 | 0.001 566 | 0.2879 | 0.2895 | 181.1 | 1262.4 | 1443.5 | 0.7145 | 4.6223 | 5.3369 |
| 2 | 462.49 | 0.001 573 | 0.2683 | 0.2698 | 190.4 | 1255.2 | 1445.6 | 0.7481 | 4.5627 | 5.3108 |
| 4 | 497.49 | 0.001 580 | 0.2502 | 0.2517 | 199.6 | 1248.0 | 1447.6 | 0.7815 | 4.5037 | 5.2852 |
| 6 | 534.51 | 0.001 587 | 0.2335 | 0.2351 | 208.9 | 1240.6 | 1449.6 | 0.8148 | 4.4451 | 5.2599 |
| 8 | 573.64 | 0.001 594 | 0.2182 | 0.2198 | 218.3 | 1233.2 | 1451.5 | 0.8479 | 4.3871 | 5.2350 |
| 10 | 614.95 | 0.001 601 | 0.2040 | 0.2056 | 227.6 | 1225.7 | 1453.3 | 0.8808 | 4.3295 | 5.2104 |
| 12 | 658.52 | 0.001 608 | 0.1910 | 0.1926 | 237.0 | 1218.1 | 1455.1 | 0.9136 | 4.2725 | 5.1861 |
| 14 | 704.44 | 0.001 616 | 0.1789 | 0.1805 | 246.4 | 1210.4 | 1456.8 | 0.9463 | 4.2159 | 5.1621 |
| 16 | 752.79 | 0.001 623 | 0.1677 | 0.1693 | 255.9 | 1202.6 | 1458.5 | 0.9788 | 4.1597 | 5.1385 |
| 18 | 803.66 | 0.001 631 | 0.1574 | 0.1590 | 265.4 | 1194.7 | 1460.0 | 1.0112 | 4.1039 | 5.1151 |
| 20 | 857.12 | 0.001 639 | 0.1477 | 0.1494 | 274.9 | 1186.7 | 1461.5 | 1.0434 | 4.0486 | 5.0920 |
| 22 | 913.27 | 0.001 647 | 0.1388 | 0.1405 | 284.4 | 1178.5 | 1462.9 | 1.0755 | 3.9937 | 5.0692 |
| 24 | 972.19 | 0.001 655 | 0.1305 | 0.1322 | 294.0 | 1170.3 | 1464.3 | 1.1075 | 3.9392 | 5.0467 |
| 26 | 1033.97 | 0.001 663 | 0.1228 | 0.1245 | 303.6 | 1162.0 | 1465.6 | 1.1394 | 3.8850 | 5.0244 |
| 28 | 1098.71 | 0.001 671 | 0.1156 | 0.1173 | 313.2 | 1153.6 | 1466.8 | 1.1711 | 3.8312 | 5.0023 |
| 30 | 1166.49 | 0.001 680 | 0.1089 | 0.1106 | 322.9 | 1145.0 | 1467.9 | 1.2028 | 3.7777 | 4.9805 |
| 32 | 1237.41 | 0.001 689 | 0.1027 | 0.1044 | 332.6 | 1136.4 | 1469.0 | 1.2343 | 3.7246 | 4.9589 |
| 34 | 1311.55 | 0.001 698 | 0.0969 | 0.0986 | 342.3 | 1127.6 | 1469.9 | 1.2656 | 3.6718 | 4.9374 |
| 36 | 1389.03 | 0.001 707 | 0.0914 | 0.0931 | 352.1 | 1118.7 | 1470.8 | 1.2969 | 3.6192 | 4.9161 |
| 38 | 1469.92 | 0.001 716 | 0.0863 | 0.0880 | 361.9 | 1109.7 | 1471.5 | 1.3281 | 3.5669 | 4.8950 |
| 40 | 1554.33 | 0.001 726 | 0.0815 | 0.0833 | 371.7 | 1100.5 | 1472.2 | 1.3591 | 3.5148 | 4.8740 |
| 42 | 1642.35 | 0.001 735 | 0.0771 | 0.0788 | 381.6 | 1091.2 | 1472.8 | 1.3901 | 3.4630 | 4.8530 |
| 44 | 1734.09 | 0.001 745 | 0.0728 | 0.0746 | 391.5 | 1081.7 | 1473.2 | 1.4209 | 3.4112 | 4.8322 |
| 46 | 1829.65 | 0.001 756 | 0.0689 | 0.0707 | 401.5 | 1072.0 | 1473.5 | 1.4518 | 3.3595 | 4.8113 |
| 48 | 1929.13 | 0.001 766 | 0.0652 | 0.0669 | 411.5 | 1062.2 | 1473.7 | 1.4826 | 3.3079 | 4.7905 |
| 50 | 2032.62 | 0.001 777 | 0.0617 | 0.0635 | 421.7 | 1052.0 | 1473.7 | 1.5135 | 3.2561 | 4.7696 |

Superheated Ammonia

| T °C | v m ³ /kg | u kJ/kg | h kJ/kg | s kJ/kg · K | v m ³ /kg | u kJ/kg | h kJ/kg | s kJ/kg · K |
|--|---------------------------|--------------|--------------|--|---------------------------|--------------|--------------|------------------|
| $p = 12.0 \text{ bars} = 1.20 \text{ MPa}$ ($T_{\text{sat}} = 30.94^\circ\text{C}$) | | | | $p = 14.0 \text{ bars} = 1.40 \text{ MPa}$ ($T_{\text{sat}} = 36.26^\circ\text{C}$) | | | | |
| Sat. | 0.10751 | 1337.52 | 1466.53 | 4.9625 | 0.09231 | 1339.56 | 1468.79 | 4.9050 |
| 40 | 0.11287 | 1359.73 | 1495.18 | 5.0553 | 0.09432 | 1349.29 | 1481.33 | 4.9453 |
| 60 | 0.12378 | 1404.54 | 1553.07 | 5.2347 | 0.10423 | 1396.97 | 1542.89 | 5.1360 |
| 80 | 0.13387 | 1445.91 | 1606.56 | 5.3906 | 0.11324 | 1440.06 | 1598.59 | 5.2984 |
| 100 | 0.14347 | 1485.55 | 1657.71 | 5.5315 | 0.12172 | 1480.79 | 1651.20 | 5.4433 |
| 120 | 0.15275 | 1524.41 | 1707.71 | 5.6620 | 0.12986 | 1520.41 | 1702.21 | 5.5765 |
| 140 | 0.16181 | 1563.09 | 1757.26 | 5.7850 | 0.13777 | 1559.63 | 1752.52 | 5.7013 |
| 160 | 0.17072 | 1601.95 | 1806.81 | 5.9021 | 0.14552 | 1598.92 | 1802.65 | 5.8198 |
| 180 | 0.17950 | 1641.23 | 1856.63 | 6.0145 | 0.15315 | 1638.53 | 1852.94 | 5.9333 |
| 200 | 0.18819 | 1681.05 | 1906.87 | 6.1230 | 0.16068 | 1678.64 | 1903.59 | 6.0427 |
| 220 | 0.19680 | 1721.50 | 1957.66 | 6.2282 | 0.16813 | 1719.35 | 1954.73 | 6.1485 |
| 240 | 0.20534 | 1762.63 | 2009.04 | 6.3303 | 0.17551 | 1760.72 | 2006.43 | 6.2513 |
| 260 | 0.21382 | 1804.48 | 2061.06 | 6.4297 | 0.18283 | 1802.78 | 2058.75 | 6.3513 |
| 280 | 0.22225 | 1847.04 | 2113.74 | 6.5267 | 0.19010 | 1845.55 | 2111.69 | 6.4488 |

| | | | | | | | | |
|--|---------|---------|---------|--|---------|---------|---------|--------|
| $p = 16.0 \text{ bars} = 1.60 \text{ MPa}$ ($T_{\text{sat}} = 41.03^\circ\text{C}$) | | | | $p = 18.0 \text{ bars} = 1.80 \text{ MPa}$ ($T_{\text{sat}} = 45.38^\circ\text{C}$) | | | | |
| Sat. | 0.08079 | 1340.97 | 1470.23 | 4.8542 | 0.07174 | 1341.88 | 1471.01 | 4.8086 |
| 60 | 0.08951 | 1389.06 | 1532.28 | 5.0461 | 0.07801 | 1380.77 | 1521.19 | 4.9627 |
| 80 | 0.09774 | 1434.02 | 1590.40 | 5.2156 | 0.08565 | 1427.79 | 1581.97 | 5.1399 |
| 100 | 0.10539 | 1475.93 | 1644.56 | 5.3648 | 0.09267 | 1470.97 | 1637.78 | 5.2937 |
| 120 | 0.11268 | 1516.34 | 1696.64 | 5.5008 | 0.09931 | 1512.22 | 1690.98 | 5.4326 |
| 140 | 0.11974 | 1556.14 | 1747.72 | 5.6276 | 0.10570 | 1552.61 | 1742.88 | 5.5614 |
| 160 | 0.12663 | 1595.85 | 1798.45 | 5.7475 | 0.11192 | 1592.76 | 1794.23 | 5.6828 |
| 180 | 0.13339 | 1635.81 | 1849.23 | 5.8621 | 0.11801 | 1633.08 | 1845.50 | 5.7985 |
| 200 | 0.14005 | 1676.21 | 1900.29 | 5.9723 | 0.12400 | 1673.78 | 1896.98 | 5.9096 |
| 220 | 0.14663 | 1717.18 | 1951.79 | 6.0789 | 0.12991 | 1715.00 | 1948.83 | 6.0170 |
| 240 | 0.15314 | 1758.79 | 2003.81 | 6.1823 | 0.13574 | 1756.85 | 2001.18 | 6.1210 |
| 260 | 0.15959 | 1801.07 | 2056.42 | 6.2829 | 0.14152 | 1799.35 | 2054.08 | 6.2222 |
| 280 | 0.16599 | 1844.05 | 2109.64 | 6.3809 | 0.14724 | 1842.55 | 2107.58 | 6.3207 |

| | | | | |
|--|---------|---------|---------|--------|
| $p = 20.0 \text{ bars} = 2.00 \text{ MPa}$ ($T_{\text{sat}} = 49.37^\circ\text{C}$) | | | | |
| Sat. | 0.06445 | 1342.37 | 1471.26 | 4.7670 |
| 60 | 0.06875 | 1372.05 | 1509.54 | 4.8838 |
| 80 | 0.07596 | 1421.36 | 1573.27 | 5.0696 |
| 100 | 0.08248 | 1465.89 | 1630.86 | 5.2283 |
| 120 | 0.08861 | 1508.03 | 1685.24 | 5.3703 |
| 140 | 0.09447 | 1549.03 | 1737.98 | 5.5012 |
| 160 | 0.10016 | 1589.65 | 1789.97 | 5.6241 |
| 180 | 0.10571 | 1630.32 | 1841.74 | 5.7409 |
| 200 | 0.11116 | 1671.33 | 1893.64 | 5.8530 |
| 220 | 0.11652 | 1712.82 | 1945.87 | 5.9611 |
| 240 | 0.12182 | 1754.90 | 1998.54 | 6.0658 |
| 260 | 0.12706 | 1797.63 | 2051.74 | 6.1675 |
| 280 | 0.13224 | 1841.03 | 2105.50 | 6.2665 |