

NATIONAL EXAMINATIONS MAY 2016

07-Mec-A1 Applied Thermodynamics and Heat Transfer

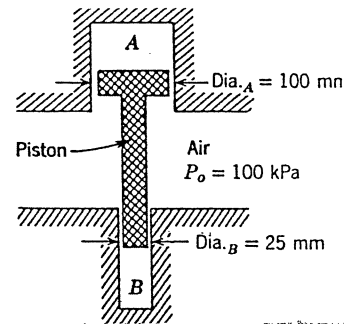
3 Hours Duration

Notes :

1. If doubt exists concerning the interpretation of any question, the candidate is urged to make assumptions and clearly explain what has been assumed along with the answer to the question.
2. The examination is open book. As a consequence, candidates are permitted to make use of any textbooks, references or notes.
3. Any non-communicating calculator is permitted. However, candidates must indicate the type of calculator(s) that they have used by writing the name and model designation of the calculator(s) on the inside of the cover of the first examination book.
4. It is expected that each candidate will have copies of both a thermodynamics text and a heat transfer text in order to make use of the information presented in the tables and graphs contained.
5. The answers to five questions, either three questions from Part A and two questions from Part B or two questions from Part A and three questions from Part B, comprise a complete examination.
6. Candidates must indicate the answers that they wish to have graded on the cover of the first examination book. Otherwise the answers will be graded in the order in which they appear in the examination book(s) up to a maximum of three answers per section.
7. The answer to any question carries the same value in the grading.

PART A - THERMODYNAMICS

1.(a) Gas is contained in two cylinders A and B connected by a piston having two different diameters as depicted in the illustration. The mass of the piston is 10 kg and the gas pressure inside cylinder A is 200 kPa. Determine the gas pressure inside cylinder B.



(b) Saturated water vapour at 200°C is contained in a cylinder fitted with a piston. The initial volume of the steam is 0.01 m^3 . The steam expands in a quasiequilibrium isothermal process until the final pressure is 200 kPa and in so doing does work against the piston. How much work is done during the process? How much error would be made by assuming the steam to behave as an ideal gas?

2. A combined reheat / regeneration cycle utilizes steam as the working fluid. The steam enters the high pressure turbine at 3.5 MPa and 350°C from which some is extracted at 0.8 MPa for the purposes of feedwater heating. The remainder of the steam is reheated to 350°C after which it enters the low pressure turbine from which some is extracted at 0.2 MPa for feedwater heating. The condenser pressure is 10 kPa and both feedwater heaters are open. Depict the cycle on a T-s diagram and determine the thermal efficiency and the net work output per kilogram of flowing steam.

3. Air enters the compressor of a Brayton cycle at 20°C and 100 kPa and leaves at a pressure of 475 kPa. The maximum temperature of the cycle is limited to 870°C by metallurgical considerations. Assuming a compressor efficiency of 82%, a turbine efficiency of 85% and a pressure drop of 13.7 kPa between the compressor and the turbine, determine (a) the pressure and temperature at each point in the cycle (b) the net work of the cycle (c) the thermal efficiency of the cycle and the percentage of the turbine work required to drive the compressor. Sketch the cycle on a temperature entropy diagram.

4. The following test data were obtained with a Freon-12 vapour compression refrigeration system operating at steady state.

| | |
|---------------------------------|---------------------|
| Condenser pressure | 700 kPa |
| Evaporator pressure | 150 kPa |
| Temperature at compressor inlet | 0°C |
| compressor outlet | 70°C |
| condenser inlet | 60°C |
| condenser outlet | 15°C |
| expansion valve inlet | 20°C |
| evaporator outlet | -10°C |

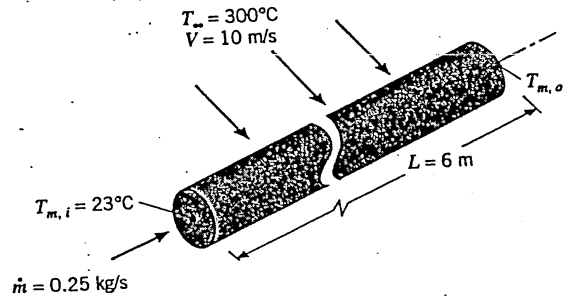
The heat transferred from the refrigerant during compression is 3.35 kJ/kg. Depict the refrigeration cycle on a T-s diagram and determine the coefficient of performance of the cycle and the thermal efficiency of the compression process.

Continued on Page 3

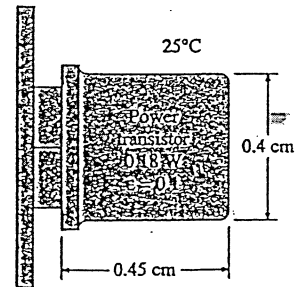
PART B - HEAT TRANSFER

5. Steam flows through a copper tube having an outside diameter $D = 2.54$ cm and a wall thickness $\delta = 0.54$ cm. The inside surface temperature $T_i = 100^\circ\text{C}$ and the temperature of the room in which the tube is located $T_\infty = 27^\circ\text{C}$. Determine the thickness of insulation having thermal conductivity $k = 0.0875$ W/m $^\circ\text{C}$ required to reduce the heat loss to the surrounding air by 95% when the tube is cooled by forced convection heat transfer where $\bar{h} = 55$ W/m 2 $^\circ\text{C}$. What would the outside surface temperature T_o be under these conditions ?

6. Oil flowing at $\dot{m} = 0.25$ kg/s enters a thin-walled tube 50 mm diameter by 6 m long at $T_{m,i} = 23^\circ\text{C}$ where it is heated by a hot gas at $T_\infty = 300^\circ\text{C}$ moving in crossflow over the tube at $V = 10$ m/s. The gas may be assumed to have the same thermophysical properties as those of air. In order to prevent the oil overheating and decomposing, the temperature of the wall must not exceed $T_t = 100^\circ\text{C}$ anywhere along the tube. Will there be any problem associated with heating the oil under these conditions ?



7. The illustration depicts a power transistor that dissipates 0.18 W when the temperature of the enclosure in which it is located is 35°C and the temperature of the air surrounding it is 25°C . The emissivity of its surface is 0.1. Disregarding any heat transfer from the base, determine the surface temperature of the power transistor.



8. A crossflow heat exchanger is comprised of 40 thin-walled tubes 1 cm in diameter located in a duct 1 m x 1 m in cross section. Cold water ($C_p = 4180$ J/kg $^\circ\text{C}$) enters the tubes at 18°C with an average velocity of 3 m/s while hot air ($C_p = 1010$ J/kg $^\circ\text{C}$) enters the channel at 130°C and 105 kPa with an average velocity of 12 m/s. If the overall heat transfer coefficient is 80 W/m 2 $^\circ\text{C}$, determine the temperatures at which the water and the air leave the heat exchanger and the rate of heat transfer.

The End

Thermodynamic Properties of Freon-12 (Dichlorodifluoromethane)^a

Saturated Freon-12

| Temp. °C | Abs. Press. MPa P | Specific Volume m ³ /kg | | | Enthalpy kJ/kg | | | Entropy kJ/kg K | | |
|-------------|----------------------------|---------------------------------------|-------------------|------------------------|-------------------------|-------------------|------------------------|-------------------------|-------------------|------------------------|
| | | Sat. Liquid v_f | Evap. v_{fg} | Sat. Vapor v_g | Sat. Liquid h_f | Evap. h_{fg} | Sat. Vapor h_g | Sat. Liquid s_f | Evap. s_{fg} | Sat. Vapor s_g |
| -90 | 0.0028 | 0.000 608 | 4.414 937 | 4.415 545 | -43.243 | 189.618 | 146.375 | -0.2084 | 1.0352 | 0.8268 |
| -85 | 0.0042 | 0.000 612 | 3.036 704 | 3.037 316 | -38.968 | 187.608 | 148.640 | -0.1854 | 0.9970 | 0.8116 |
| -80 | 0.0062 | 0.000 617 | 2.137 728 | 2.138 345 | -34.688 | 185.612 | 150.924 | -0.1630 | 0.9609 | 0.7979 |
| -75 | 0.0088 | 0.000 622 | 1.537 030 | 1.537 651 | -30.401 | 183.625 | 153.224 | -0.1411 | 0.9266 | 0.7855 |
| -70 | 0.0123 | 0.000 627 | 1.126 654 | 1.127 280 | -26.103 | 181.640 | 155.536 | -0.1197 | 0.8940 | 0.7744 |
| -65 | 0.0168 | 0.000 632 | 0.840 534 | 0.841 166 | -21.793 | 179.651 | 157.857 | -0.0987 | 0.8630 | 0.7643 |
| -60 | 0.0226 | 0.000 637 | 0.637 274 | 0.637 910 | -17.469 | 177.653 | 160.184 | -0.0782 | 0.8334 | 0.7552 |
| -55 | 0.0300 | 0.000 642 | 0.490 358 | 0.491 000 | -13.129 | 175.641 | 162.512 | -0.0581 | 0.8051 | 0.7470 |
| -50 | 0.0391 | 0.000 648 | 0.382 457 | 0.383 105 | -8.772 | 173.611 | 164.840 | -0.0384 | 0.7779 | 0.7396 |
| -45 | 0.0504 | 0.000 654 | 0.302 029 | 0.302 682 | -4.396 | 171.558 | 167.163 | -0.0190 | 0.7519 | 0.7329 |
| -40 | 0.0642 | 0.000 659 | 0.241 251 | 0.241 910 | -0.000 | 169.479 | 169.479 | -0.0000 | 0.7269 | 0.7269 |
| -35 | 0.0807 | 0.000 666 | 0.194 732 | 0.195 398 | 4.416 | 167.368 | 171.784 | 0.0187 | 0.7027 | 0.7214 |
| -30 | 0.1004 | 0.000 672 | 0.158 703 | 0.159 375 | 8.854 | 165.222 | 174.076 | 0.0371 | 0.6795 | 0.7165 |
| -25 | 0.1237 | 0.000 679 | 0.130 487 | 0.131 166 | 13.315 | 163.037 | 176.352 | 0.0552 | 0.6570 | 0.7121 |
| -20 | 0.1509 | 0.000 685 | 0.108 162 | 0.108 847 | 17.800 | 160.810 | 178.610 | 0.0730 | 0.6352 | 0.7082 |
| -15 | 0.1826 | 0.000 693 | 0.090 326 | 0.091 018 | 22.312 | 158.534 | 180.846 | 0.0906 | 0.6141 | 0.7046 |
| -10 | 0.2191 | 0.000 700 | 0.075 946 | 0.076 646 | 26.851 | 156.207 | 183.058 | 0.1079 | 0.5936 | 0.7014 |
| -5 | 0.2610 | 0.000 708 | 0.064 255 | 0.064 963 | 31.420 | 153.823 | 185.243 | 0.1250 | 0.5736 | 0.6986 |
| 0 | 0.3086 | 0.000 716 | 0.054 673 | 0.055 389 | 36.022 | 151.376 | 187.397 | 0.1418 | 0.5542 | 0.6960 |
| 5 | 0.3626 | 0.000 724 | 0.046 761 | 0.047 485 | 40.659 | 148.859 | 189.518 | 0.1585 | 0.5351 | 0.6937 |
| 10 | 0.4233 | 0.000 733 | 0.040 180 | 0.040 914 | 45.337 | 146.265 | 191.602 | 0.1750 | 0.5165 | 0.6916 |
| 15 | 0.4914 | 0.000 743 | 0.034 671 | 0.035 413 | 50.058 | 143.586 | 193.644 | 0.1914 | 0.4983 | 0.6897 |
| 20 | 0.5673 | 0.000 752 | 0.030 028 | 0.030 780 | 54.828 | 140.812 | 195.641 | 0.2076 | 0.4803 | 0.6879 |
| 25 | 0.6516 | 0.000 763 | 0.026 091 | 0.026 854 | 59.653 | 137.933 | 197.586 | 0.2237 | 0.4626 | 0.6863 |
| 30 | 0.7449 | 0.000 774 | 0.022 734 | 0.023 508 | 64.539 | 134.936 | 199.475 | 0.2397 | 0.4451 | 0.6848 |
| 35 | 0.8477 | 0.000 786 | 0.019 855 | 0.020 641 | 69.494 | 131.805 | 201.299 | 0.2557 | 0.4277 | 0.6834 |
| 40 | 0.9607 | 0.000 798 | 0.017 373 | 0.018 171 | 74.527 | 128.525 | 203.051 | 0.2716 | 0.4104 | 0.6820 |
| 45 | 1.0843 | 0.000 811 | 0.015 220 | 0.016 032 | 79.647 | 125.074 | 204.722 | 0.2875 | 0.3931 | 0.6806 |
| 50 | 1.2193 | 0.000 826 | 0.013 344 | 0.014 170 | 84.868 | 121.430 | 206.298 | 0.3034 | 0.3758 | 0.6792 |
| 55 | 1.3663 | 0.000 841 | 0.011 701 | 0.012 542 | 90.201 | 117.565 | 207.766 | 0.3194 | 0.3582 | 0.6777 |
| 60 | 1.5259 | 0.000 858 | 0.010 253 | 0.011 111 | 95.665 | 113.443 | 209.109 | 0.3355 | 0.3405 | 0.6760 |
| 65 | 1.6988 | 0.000 877 | 0.008 971 | 0.009 847 | 101.279 | 109.024 | 210.303 | 0.3518 | 0.3224 | 0.6742 |
| 70 | 1.8858 | 0.000 897 | 0.007 828 | 0.008 725 | 107.067 | 104.255 | 211.321 | 0.3683 | 0.3038 | 0.6721 |
| 75 | 2.0874 | 0.000 920 | 0.006 802 | 0.007 723 | 113.058 | 99.068 | 212.126 | 0.3851 | 0.2845 | 0.6697 |
| 80 | 2.3046 | 0.000 946 | 0.005 875 | 0.006 821 | 119.291 | 93.373 | 212.665 | 0.4023 | 0.2644 | 0.6667 |
| 85 | 2.5380 | 0.000 976 | 0.005 029 | 0.006 005 | 125.818 | 87.047 | 212.865 | 0.4201 | 0.2430 | 0.6631 |
| 90 | 2.7885 | 0.001 012 | 0.004 246 | 0.005 258 | 132.708 | 79.907 | 212.614 | 0.4385 | 0.2200 | 0.6585 |
| 95 | 3.0569 | 0.001 056 | 0.003 508 | 0.004 563 | 140.068 | 71.658 | 211.726 | 0.4579 | 0.1946 | 0.6526 |
| 100 | 3.3440 | 0.001 113 | 0.002 790 | 0.003 903 | 148.076 | 61.768 | 209.843 | 0.4788 | 0.1655 | 0.6444 |
| 105 | 3.6509 | 0.001 197 | 0.002 045 | 0.003 242 | 157.085 | 49.014 | 206.099 | 0.5023 | 0.1296 | 0.6319 |
| 110 | 3.9784 | 0.001 364 | 0.001 098 | 0.002 462 | 168.059 | 28.425 | 196.484 | 0.5322 | 0.0742 | 0.6064 |
| 112 | 4.1155 | 0.001 792 | 0.000 005 | 0.001 797 | 174.920 | 0.151 | 175.071 | 0.5651 | 0.0004 | 0.5655 |

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Superheated Freon-12

| Temp. °C | <i>v</i> m ³ /kg | <i>h</i> kJ/kg | <i>s</i> kJ/kg K | <i>v</i> m ³ /kg | <i>h</i> kJ/kg | <i>s</i> kJ/kg K | <i>v</i> m ³ /kg | <i>h</i> kJ/kg | <i>s</i> kJ/kg K |
|-------------|--------------------------------|-------------------|---------------------|--------------------------------|-------------------|---------------------|--------------------------------|-------------------|---------------------|
| 0.05 MPa | | | 0.10 MPa | | | 0.15 MPa | | | |
| -20.0 | 0.341 857 | 181.042 | 0.7912 | 0.167 701 | 179.861 | 0.7401 | | | |
| -10.0 | 0.356 227 | 186.757 | 0.8133 | 0.175 222 | 185.707 | 0.7628 | 0.114 716 | 184.619 | 0.7318 |
| 0.0 | 0.370 508 | 192.567 | 0.8350 | 0.182 647 | 191.628 | 0.7849 | 0.119 866 | 190.660 | 0.7543 |
| 10.0 | 0.384 716 | 198.471 | 0.8562 | 0.189 994 | 197.628 | 0.8064 | 0.124 932 | 196.762 | 0.7763 |
| 20.0 | 0.398 863 | 204.469 | 0.8770 | 0.197 277 | 203.707 | 0.8275 | 0.129 930 | 202.927 | 0.7977 |
| 30.0 | 0.412 959 | 210.557 | 0.8974 | 0.204 506 | 209.866 | 0.8482 | 0.134 873 | 209.160 | 0.8186 |
| 40.0 | 0.427 012 | 216.733 | 0.9175 | 0.211 691 | 216.104 | 0.8684 | 0.139 768 | 215.463 | 0.8390 |
| 50.0 | 0.441 030 | 222.997 | 0.9372 | 0.218 839 | 222.421 | 0.8883 | 0.144 625 | 221.835 | 0.8591 |
| 60.0 | 0.455 017 | 229.344 | 0.9565 | 0.225 955 | 228.815 | 0.9078 | 0.149 450 | 228.277 | 0.8787 |
| 70.0 | 0.468 978 | 235.774 | 0.9755 | 0.233 044 | 235.285 | 0.9269 | 0.154 247 | 234.789 | 0.8980 |
| 80.0 | 0.482 917 | 242.282 | 0.9942 | 0.240 111 | 241.829 | 0.9457 | 0.159 020 | 241.371 | 0.9169 |
| 90.0 | 0.496 838 | 248.868 | 1.0126 | 0.247 159 | 248.446 | 0.9642 | 0.163 774 | 248.020 | 0.9354 |
| 0.20 MPa | | | 0.25 MPa | | | 0.30 MPa | | | |
| 0.0 | 0.088 608 | 189.669 | 0.7320 | 0.069 752 | 188.644 | 0.7139 | 0.057 150 | 187.583 | 0.6984 |
| 10.0 | 0.092 550 | 195.878 | 0.7543 | 0.073 024 | 194.969 | 0.7366 | 0.059 984 | 194.034 | 0.7216 |
| 20.0 | 0.096 418 | 202.135 | 0.7760 | 0.076 218 | 201.322 | 0.7587 | 0.062 734 | 200.490 | 0.7440 |
| 30.0 | 0.100 228 | 208.446 | 0.7972 | 0.079 350 | 207.715 | 0.7801 | 0.065 418 | 206.969 | 0.7658 |
| 40.0 | 0.103 989 | 214.814 | 0.8178 | 0.082 431 | 214.155 | 0.8010 | 0.068 049 | 213.480 | 0.7869 |
| 50.0 | 0.107 710 | 221.243 | 0.8381 | 0.085 470 | 220.642 | 0.8214 | 0.070 635 | 220.030 | 0.8075 |
| 60.0 | 0.111 397 | 227.735 | 0.8578 | 0.088 474 | 227.185 | 0.8413 | 0.073 185 | 226.627 | 0.8276 |
| 70.0 | 0.115 055 | 234.291 | 0.8772 | 0.091 449 | 233.785 | 0.8608 | 0.075 705 | 233.273 | 0.8473 |
| 80.0 | 0.118 690 | 240.910 | 0.8962 | 0.094 398 | 240.443 | 0.8800 | 0.078 200 | 239.971 | 0.8665 |
| 90.0 | 0.122 304 | 247.593 | 0.9149 | 0.097 327 | 247.160 | 0.8987 | 0.080 673 | 246.723 | 0.8853 |
| 100.0 | 0.125 901 | 254.339 | 0.9332 | 0.100 238 | 253.936 | 0.9171 | 0.083 127 | 253.530 | 0.9038 |
| 110.0 | 0.129 483 | 261.147 | 0.9512 | 0.103 134 | 260.770 | 0.9352 | 0.085 566 | 260.391 | 0.9220 |
| 0.40 MPa | | | 0.50 MPa | | | 0.60 MPa | | | |
| 20.0 | 0.045 836 | 198.762 | 0.7199 | 0.035 646 | 196.935 | 0.6999 | | | |
| 30.0 | 0.047 971 | 205.428 | 0.7423 | 0.037 464 | 203.814 | 0.7230 | 0.030 422 | 202.116 | 0.7063 |
| 40.0 | 0.050 046 | 212.095 | 0.7639 | 0.039 214 | 210.656 | 0.7452 | 0.031 966 | 209.154 | 0.7291 |
| 50.0 | 0.052 072 | 218.779 | 0.7849 | 0.040 911 | 217.484 | 0.7667 | 0.033 450 | 216.141 | 0.7511 |
| 60.0 | 0.054 059 | 225.488 | 0.8054 | 0.042 565 | 224.315 | 0.7875 | 0.034 887 | 223.104 | 0.7723 |
| 70.0 | 0.056 014 | 232.230 | 0.8253 | 0.044 184 | 231.161 | 0.8077 | 0.036 285 | 230.062 | 0.7929 |
| 80.0 | 0.057 941 | 239.012 | 0.8448 | 0.045 774 | 238.031 | 0.8275 | 0.037 653 | 237.027 | 0.8129 |
| 90.0 | 0.059 846 | 245.837 | 0.8638 | 0.047 340 | 244.932 | 0.8467 | 0.038 995 | 244.009 | 0.8324 |
| 100.0 | 0.061 731 | 252.707 | 0.8825 | 0.048 886 | 251.869 | 0.8656 | 0.040 316 | 251.016 | 0.8514 |
| 110.0 | 0.063 600 | 259.624 | 0.9008 | 0.050 415 | 258.845 | 0.8840 | 0.041 619 | 258.053 | 0.8700 |
| 120.0 | 0.065 455 | 266.590 | 0.9187 | 0.051 929 | 265.862 | 0.9021 | 0.042 907 | 265.124 | 0.8882 |
| 130.0 | 0.067 298 | 273.605 | 0.9364 | 0.053 430 | 272.923 | 0.9198 | 0.044 181 | 272.231 | 0.9061 |
| 0.70 MPa | | | 0.80 MPa | | | 0.90 MPa | | | |
| 40.0 | 0.026 761 | 207.580 | 0.7148 | 0.022 830 | 205.924 | 0.7016 | 0.019 744 | 204.170 | 0.6982 |
| 50.0 | 0.028 100 | 214.745 | 0.7373 | 0.024 068 | 213.290 | 0.7248 | 0.020 912 | 211.765 | 0.7131 |
| 60.0 | 0.029 387 | 221.854 | 0.7590 | 0.025 247 | 220.558 | 0.7469 | 0.022 012 | 219.212 | 0.7358 |
| 70.0 | 0.030 632 | 228.931 | 0.7799 | 0.026 380 | 227.766 | 0.7682 | 0.023 062 | 226.564 | 0.7575 |
| 80.0 | 0.031 843 | 235.997 | 0.8002 | 0.027 477 | 234.941 | 0.7888 | 0.024 072 | 233.856 | 0.7785 |
| 90.0 | 0.033 027 | 243.066 | 0.8199 | 0.028 545 | 242.101 | 0.8088 | 0.025 051 | 241.113 | 0.7987 |
| 100.0 | 0.034 189 | 250.146 | 0.8392 | 0.029 588 | 249.260 | 0.8283 | 0.026 005 | 248.355 | 0.8184 |
| 110.0 | 0.035 332 | 257.247 | 0.8579 | 0.030 612 | 256.428 | 0.8472 | 0.026 937 | 255.593 | 0.8376 |
| 120.0 | 0.036 458 | 264.374 | 0.8763 | 0.031 619 | 263.613 | 0.8657 | 0.027 851 | 262.839 | 0.8562 |
| 130.0 | 0.037 572 | 271.531 | 0.8943 | 0.032 612 | 270.820 | 0.8838 | 0.028 751 | 270.100 | 0.8745 |
| 140.0 | 0.038 673 | 278.720 | 0.9119 | 0.033 592 | 278.055 | 0.9016 | 0.029 639 | 277.381 | 0.8923 |
| 150.0 | 0.039 764 | 285.946 | 0.9292 | 0.034 563 | 285.320 | 0.9189 | 0.030 515 | 284.687 | 0.9098 |
| 1.00 MPa | | | 1.20 MPa | | | 1.40 MPa | | | |
| 50.0 | 0.018 366 | 210.162 | 0.7021 | 0.014 483 | 206.661 | 0.6812 | | | |
| 60.0 | 0.019 410 | 217.810 | 0.7254 | 0.015 463 | 214.805 | 0.7060 | 0.012 579 | 211.457 | 0.6876 |
| 70.0 | 0.020 397 | 225.319 | 0.7476 | 0.016 368 | 222.687 | 0.7293 | 0.013 448 | 219.822 | 0.7123 |
| 80.0 | 0.021 341 | 232.739 | 0.7689 | 0.017 221 | 230.398 | 0.7514 | 0.014 247 | 227.891 | 0.7355 |
| 90.0 | 0.022 251 | 240.101 | 0.7895 | 0.018 032 | 237.995 | 0.7727 | 0.014 997 | 235.766 | 0.7575 |
| 100.0 | 0.023 133 | 247.430 | 0.8094 | 0.018 812 | 245.518 | 0.7931 | 0.015 710 | 243.512 | 0.7785 |
| 110.0 | 0.023 993 | 254.743 | 0.8287 | 0.019 567 | 252.993 | 0.8129 | 0.016 393 | 251.170 | 0.7988 |
| 120.0 | 0.024 835 | 262.053 | 0.8475 | 0.020 301 | 260.441 | 0.8320 | 0.017 053 | 258.770 | 0.8183 |
| 130.0 | 0.025 661 | 269.369 | 0.8659 | 0.021 018 | 267.875 | 0.8507 | 0.017 695 | 266.334 | 0.8373 |
| 140.0 | 0.026 474 | 276.699 | 0.8839 | 0.021 721 | 275.307 | 0.8689 | 0.018 321 | 273.877 | 0.8558 |
| 150.0 | 0.027 275 | 284.047 | 0.9015 | 0.022 412 | 282.745 | 0.8867 | 0.018 934 | 281.411 | 0.8738 |
| 160.0 | 0.028 068 | 291.419 | 0.9187 | 0.023 093 | 290.195 | 0.9041 | 0.019 535 | 288.946 | 0.8914 |
| 1.60 MPa | | | 1.80 MPa | | | 2.00 MPa | | | |
| 70.0 | 0.011 208 | 216.650 | 0.6959 | 0.009 406 | 213.049 | 0.6794 | | | |
| 80.0 | 0.011 984 | 225.177 | 0.7204 | 0.010 187 | 222.198 | 0.7057 | 0.008 704 | 218.859 | 0.6909 |
| 90.0 | 0.012 698 | 233.390 | 0.7433 | 0.010 884 | 230.835 | 0.7298 | 0.009 406 | 228.056 | 0.7166 |
| 100.0 | 0.013 366 | 241.397 | 0.7651 | 0.011 526 | 239.155 | 0.7524 | 0.010 035 | 236.760 | 0.7402 |
| 110.0 | 0.014 000 | 249.264 | 0.7859 | 0.012 126 | 247.264 | 0.7739 | 0.010 615 | 245.154 | 0.7624 |
| 120.0 | 0.014 608 | 257.035 | 0.8059 | 0.012 697 | 255.228 | 0.7944 | 0.011 159 | 253.341 | 0.7835 |
| 130.0 | 0.015 195 | 264.742 | 0.8253 | 0.013 244 | 263.094 | 0.8141 | 0.011 676 | 261.384 | 0.8037 |
| 140.0 | 0.015 765 | 272.406 | 0.8440 | 0.013 772 | 270.891 | 0.8332 | 0.012 172 | 269.327 | 0.8232 |
| 150.0 | 0.016 320 | 280.044 | 0.8623 | 0.014 284 | 278.642 | 0.8518 | 0.012 651 | 277.201 | 0.8420 |