

NATIONAL EXAMINATIONS

December 2014

07-MEC-B3 ENERGY CONVERSION AND POWER GENERATION

Three hours duration

Notes to Candidates

1. This is a **Closed Book** examination.
2. Examination paper consists of two Sections. **Section A is Calculative** with four (4) questions and **Section B is Descriptive** with two (2) questions.
3. Note that Question 2 is on two pages.
3. **Do three (3) questions (including all parts of each question) from Section A (Calculative) and one (1) question from Section B (Descriptive).**
4. **Four questions constitute a complete paper.** (Total 60 marks).
5. **All questions are of equal value.** (Each 15 marks).
6. If doubt exists as to the interpretation of any question or in the event of missing data, the candidate is urged to submit, with the answer paper, a clear statement of any assumptions made.
7. Candidates may use one of the approved **Casio** or **Sharp** calculators.
8. **Reference data** for particular questions are given on pages 9 to 13. **All pages used are to be returned with the answer booklet showing where data has been obtained.**
9. **Reference formulae and constants** are given on pages 14 to 17.
10. **Steam Tables** from "Thermodynamics and Heat Power" are provided.

SECTION A CALCULATIVE QUESTIONS**QUESTION 1 GAS TURBINE MODULAR HELIUM REACTOR**

Refer to the Examination Paper Attachments Page 9 **Gas Turbine Modular Helium Reactor**. Refer to General Constants on Page 15 for specific heats.

The diagram shows a schematic of the gas circuit of a high temperature nuclear reactor of the Gas Turbine Modular type. The following terminal conditions apply:

Helium pressure at compressor inlet	2 MPa
Helium pressure at intercooler	4 MPa
Helium pressure at compressor outlet	7 MPa
Helium temperature at compressor inlet	30°C
Helium temperature after intercooler	30°C
Helium temperature at turbine inlet	850°C
Terminal temperature differences in recuperating heat exchanger	20°C
Terminal temperature differences in heat rejection heat exchangers	15°C
Compressor efficiency	90%
Turbine efficiency	85%
Electrical power output	250 MW

The differences in the terminal temperatures are the same at each end of the respective heat exchangers.

Assume negligible pressure loss in the gas circuit and no mechanical nor electrical losses.

- Sketch a temperature-entropy diagram for the gas circuit in the space provided on Page 9. Identify key points by number to correspond with the flow diagram. Show terminal temperature differences. (3)
- Calculate the temperatures at all key points in the circuit as identified in the diagram on Page 9. (7)
- Calculate the thermodynamic cycle efficiency. (2)
- Calculate the required flow rate of helium to give the specified power output. (1)
- Calculate the required flow rate of cooling water to give the necessary rate of heat rejection. (2)

[15 marks]

QUESTION 2 STEAM CYCLE AND COAL FIRED PLANT

PART I STEAM CYCLE EFFICIENCY

Refer to the Examination Paper Attachments Page 10 **Regenerative Feedwater Heating**.

An ideal Rankine Cycle operates between a pressure of 6 MPa and 0.004 MPa with superheating to 400°C. Steam is extracted from the turbine at 0.6 MPa for feedwater heating in a direct contact feedwater heater which operates at this pressure. Complete mixing of the steam and water occurs. A condensate extraction pump is required to pump from the condenser pressure of 0.004 MPa to 0.6 MPa and a boiler feedwater pump to pump from 0.6 MPa to the boiler pressure of 6 MPa. Isentropic conditions prevail in the pumps and turbine. Use the enthalpies given in the table in the attachments.

- (a) Sketch the process on the T-s diagram provided in the attachments. Label all key points by number to correspond with the flow diagram.
(4)
- (b) Determine the fractional mass flow of steam required for feedwater heating.
(2)
- (c) Calculate the cycle efficiency with the feedwater heater in operation.
(4)

(10 marks)

This question is continued on the next page

Question 2 Continued

PART II COAL FIRED PLANT

A coal fired power plant with an electrical output of 600 MW has the following operating parameters:

Steam cycle efficiency	41%
Boiler thermal efficiency	94%
Electrical generation efficiency	96%
Coal calorific value (as received)	35 000 kJ/kg
Coal ash content	6%
Cooling water inlet temperature	13°C
Cooling water temperature rise	11°C (maximum)
Cooling water specific heat	4.19 kJ/kg°C
Cooling water density	1025 kg/m ³

Under full load conditions determine the following:

- (a) Required mass flow rate and volume flow rate of cooling water so as not to exceed the maximum permitted cooling water temperature rise.
(2)
- (b) Required mass flow rate of coal and amount of ash produced per day.
(3)

(5 marks)

[15 marks]

QUESTION 3 FEEDWATER HEATERS AND CONDENSERS**PART I BELLEDUNE FEEDWATER HEATER**

In a boiler plant the feedwater entering the boiler is progressively preheated in a series of feedwater heaters which draw heating steam from the steam turbine. At Belledune Generating Station in the last stage of feedwater heating the feedwater temperature is increased from 230°C to 280°C while the pressure remains constant at 20 MPa. The heating steam enters at 400°C (superheated), is condensed and leaves as water at 240°C (subcooled) while the pressure remains constant at 5 MPa. If the feedwater flow is 350 kg/s calculate the required steam flow. Use Steam Tables as provided. The values given in this question have been rounded to facilitate the use of steam tables. Note that a sketch to properly identify the key points around the heater is required.

(5 marks)

PART II CONDENSER PERFORMANCE

Refer to the Examination Paper Attachments Page 11 **Koeberg Condenser** and Page 12 **Temperature Profiles**. Note that 1 bar = 0.1 MPa.

Consider the condenser to be operating under the given conditions. Sketch, in dotted lines on each of the given axes, the design temperature profile, with specified temperatures for both cooling water and steam, along the condenser tubes (from inlet to outlet). Show clearly the change in cooling water temperature ΔT and the difference between the average cooling water temperature and the condensing steam temperature θ .

For the following no detailed calculations are required and temperatures should be rounded to the nearest 1°C. The estimates should be based on average temperature differences (not log mean temperature differences) and in each case the new values for ΔT and θ should be stated.

If the conditions are changed as indicated below, sketch, in solid lines on the given axes, the anticipated temperature profiles, with numerical values for both cooling water and steam, across the condenser for each of the following conditions:

- (a) Cooling water inlet temperature increased to 18°C.
- (b) Turbine load reduced to one quarter of its original value.
- (c) Cooling water flow reduced to one half of its original value which also results in the overall heat transfer coefficient being reduced to 70% of its original value.
- (d) Overall heat transfer coefficient reduced by 20% due to fouling of tubes.

(10 marks)

[15 marks]

QUESTION 4 BELLEDUNE HEAT BALANCE DIAGRAM

Refer to the Examination Paper Attachments Page 13 **Heat Balance Diagram for Belledune Generating Station.**

At the rated electrical output of 430 MW determine the following:

- (a) Steam cycle efficiency based on boiler heat input and electrical output. (3)
- (b) Shaft power output of high pressure turbine. (4)
- (c) Steam power input to boiler feed-water pump turbine based on steam... conditions. (2)
- (d) Shaft power input to boiler feedwater pump based on enthalpy rise (Δh) in the pump. (2)
- (e) Hydraulic power output of the boiler feedwater pump based on pressure rise P_D in the pump. The density of water at the pump is 912 kg/m^3 . (3)
- (f) Feedwater pump efficiency. (1)

[15 marks]

SECTION B DESCRIPTIVE QUESTIONS

Descriptive questions should be answered in essay form with sketches, if appropriate, and taking approximately one full page for every 5 marks. A full page means approximately 250 words unless diagrams take the place of some words.

While Question 5 lists several aspects, more emphasis may be put on some aspects and less on others provided an overall comprehensive answer is given as required by the above.

QUESTION 5 NUCLEAR AND WIND POWER

Generation of electric power without the emission of carbon dioxide is possible by the use of nuclear energy or wind energy both of which are proven technologies. Suppose a large power utility has to increase its generation capacity by installing approximately 2000 MW to meet the anticipated electricity demand in 2024. Both nuclear power and wind power are options in this particular circumstance. Discuss the suitability of each for this application by addressing the following aspects:

- Number of generating units required
- Land and space requirements
- Impact on the environment
- Reliability of power supply
- Likely capacity factor
- Ability to meet varying daily load demand
- Flexibility of operation (load variation)
- Effluents and emissions
- Construction benefits and constraints
- Connections with grid system
- Maintenance requirements

As a conclusion make an appropriate recommendation. Relative costs do not have to be considered.

This question should be answered in essay form in approximately 800 words.

[15 marks]

QUESTION 6 CYCLE PERFORMANCE ENHANCEMENT

Basic thermodynamic cycles such as the Rankine, Brayton and Otto do not convert heat into work at the optimum level and their performance can be improved by certain enhancements, either to the cycle itself or to the output from the cycle, which ultimately result in better fuel economy. For each of the following explain in detail the fundamental principles which enhance the performance of the cycle or engine.

Where appropriate cycle diagrams or flow diagrams should be included to illustrate the enhancement.

- (a) Feedwater heating in a steam cycle as used in a large scale electric power generating plant.
(5 marks)

- (b) Recuperative heating in a gas turbine where exhaust gas is used to preheat combustion air.
(5 marks)

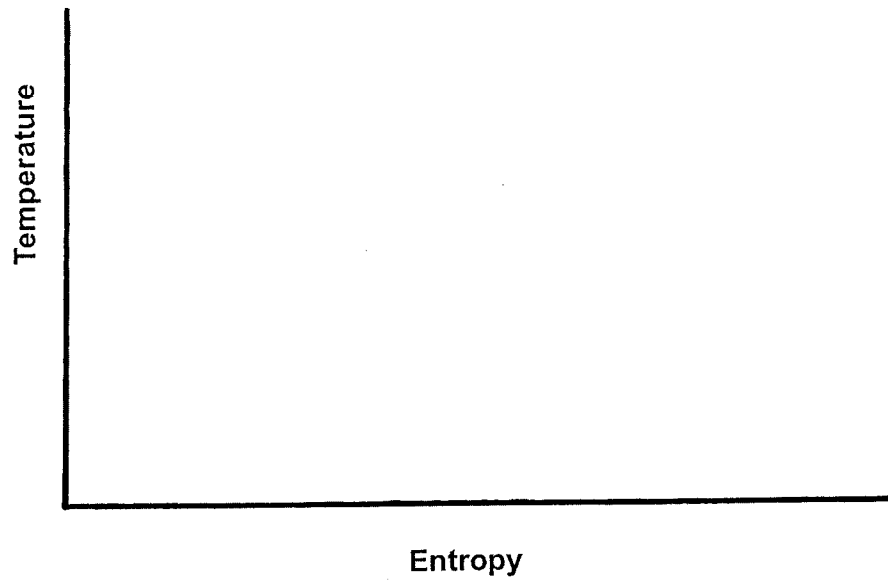
- (c) Turbocharging in a gasoline powered spark ignition automotive engine or a large diesel powered compression ignition engine (compared with a conventional or naturally aspirated engine).
(5 marks)

[15 marks]

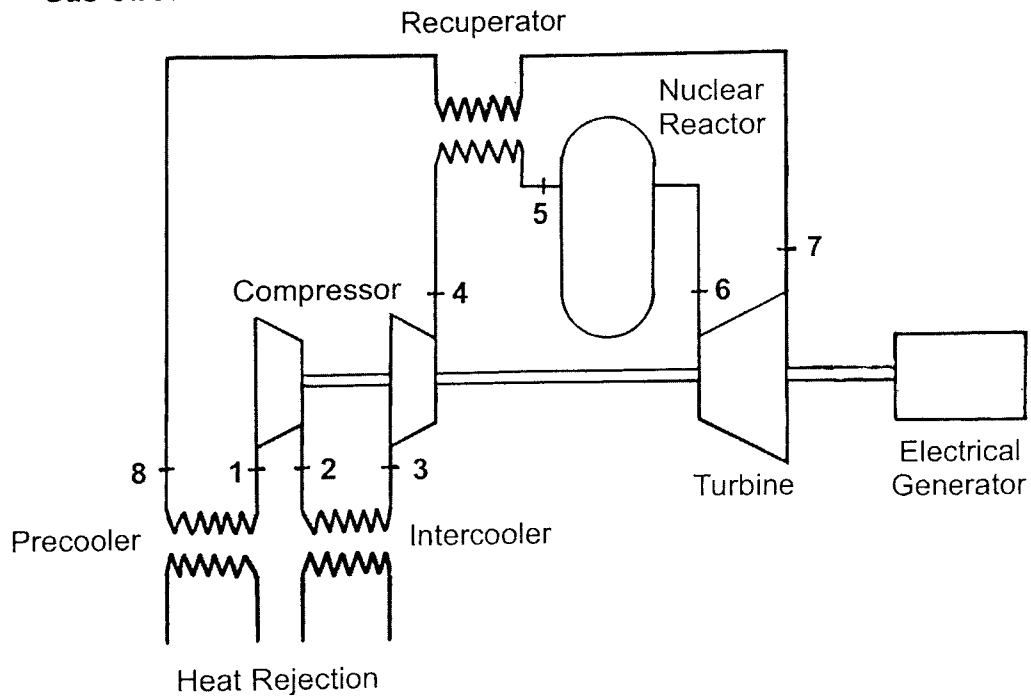
NAME

EXAMINATION PAPER ATTACHMENTS

QUESTION 1 GAS TURBINE MODULAR HELIUM REACTOR

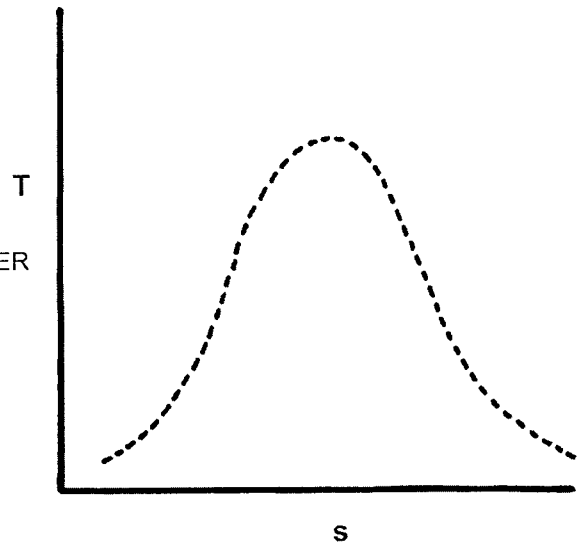
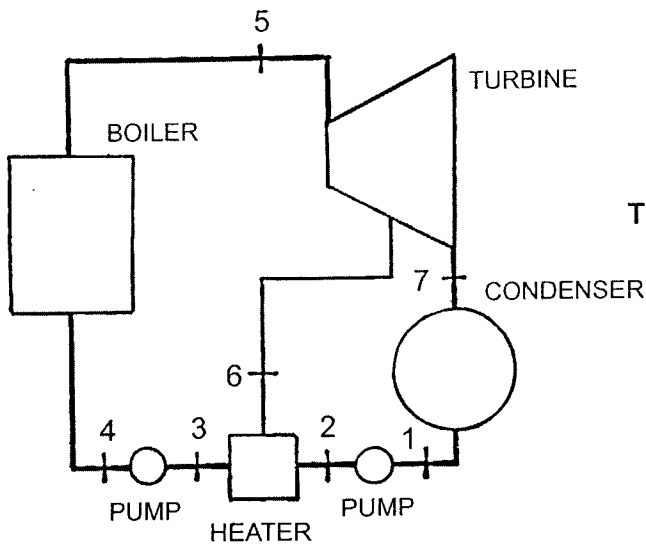


Gas Circuit



NAME

QUESTION 2 PART I REGENERATIVE FEEDWATER HEATING



Point	Pressure (MPa)	Temperature (°C)	Enthalpy (kJ/kg)	Conditions
1	0.004	29	121	saturated water
2	0.6	29	122	subcooled water
3	0.6	159	671	saturated water
4	6	160	677	subcooled water
5	6	400	3177	superheated steam
6	0.6	159	2662	wet mixture
7	0.004	29	1970	wet mixture

QUESTION 3 PART II KOEBERG CONDENSER

NAME

Steam flow rate	2996 t/h
Water make-up flow rate	9 t/h
Cooling water flow rate	141 000 t/h
Cooling water inlet temperature	13°C
Cooling water outlet temperature	24°C
Cooling water density	1.025
Cooling water friction head loss	4.7 m
Mean steam velocity at tube bank	92 m/s
Cooling water velocity inside tubes	2 m/s
Number of tubes	76968
Number of support plates	14 (per bundle)
Tube material	titanium
Cooling surface area	57 426 m ²
Tube overall length	12.84 m
Tube effective length	12.50 m
Tube diameter (OD)	19 mm
Tube wall thickness (normal tubes)	0.5 mm
Tube wall thickness (impact tubes)	0.6 mm
Tube configuration	diagonal array
Tube pitch across array	26 mm
Tube pitch along array	45 mm
Tube fixing method	expanding
Tube mass	132 t
Total volume under vacuum	7500 m ³
Steam inlet pressure	0.043 bar abs
Steam inlet temperature	30°C
Terminal temperature difference	6°C
Condenser hotwell capacity	700 m ³ (approx.)
Number of water boxes (inlet and outlet)	12
Water box internal lining	neoprene
Condenser shell thickness	18 mm
Tube plate thickness	25 mm
Support plate thickness	12 mm
Condenser length	43 m (approx.)
Condenser width	25 m (approx.)
Condenser mass without LP Heaters	1267 t

QUESTION 3 PART II TEMPERATURE PROFILES

NAME

Show initial conditions as dotted lines on each diagram

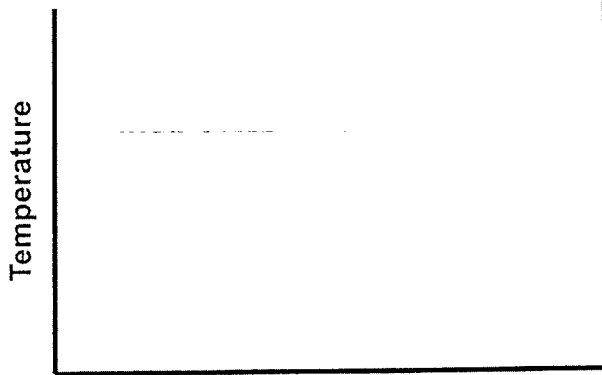
Show new conditions for each case as solid lines

Give temperatures on axes

Show basic calculations and new values for ΔT and θ below each diagram

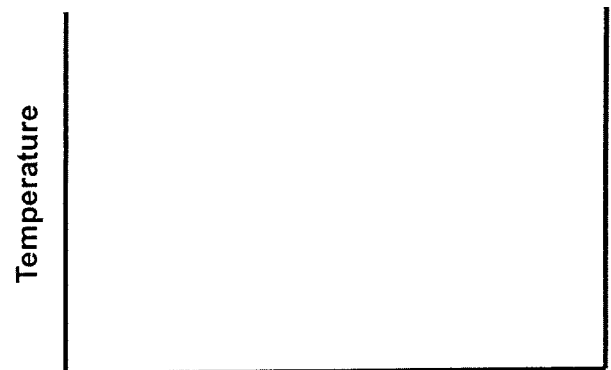
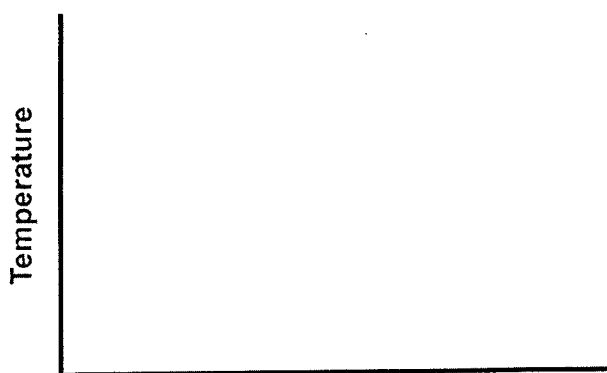
(a) Increase in cooling water temperature

(b) Reduction in turbine load

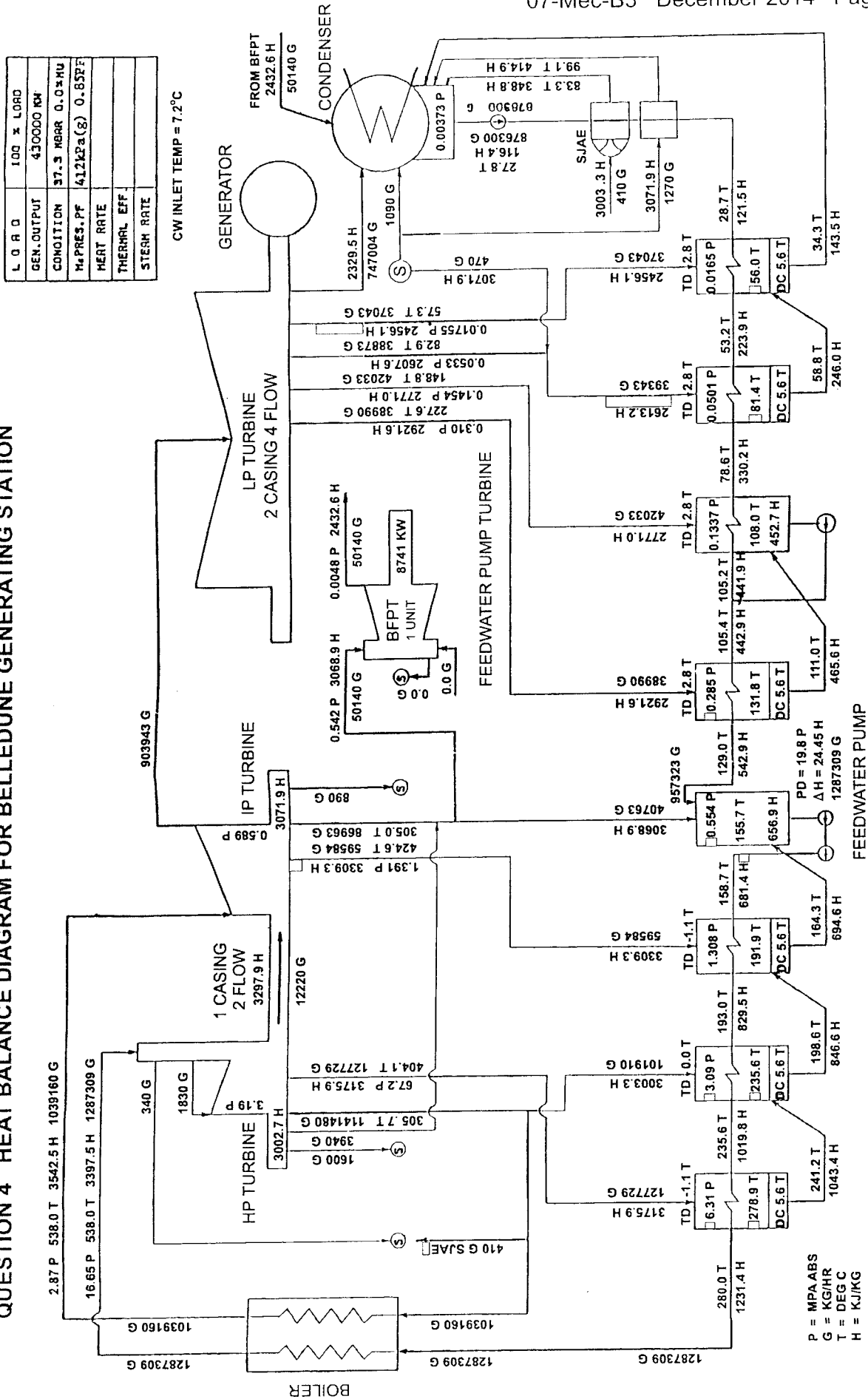


(c) Reduction in cooling water flow

(d) Reduction in heat transfer coefficient



QUESTION 4 HEAT BALANCE DIAGRAM FOR BELLEDUNE GENERATING STATION



LOAD	100 % LOAD
GEN. OUTPUT	430000 KW
CONDITION	37.5 MBR 0.0 MHR
Ma PRES. PF	412 kPa (g) 0.85 FF
MERT RATE	
THERMAL EFF	
STEAM RATE	

CW INLET TEMP = 7.2°C

P = MPA ABS
G = KG/HR
T = DEG C
H = KJ/KG

APPROVED BY	MESSERS	REHEAT TURBINE
ED BY	130000 KW	TURBINE
CHECKED BY	HEAT BALANCE DIAGRAM	
DESIGNED BY	TOSHIBA CORPORATION	
ED BY		

NOMENCLATURE FOR REFERENCE EQUATIONS (SI UNITS)

A	Flow area, Surface area	m^2
c_p	Specific heat at constant pressure	$J/kg^\circ C$
c_v	Specific heat at constant volume	$J/kg^\circ C$
D	Diameter	m
E	Energy	J
g	Gravitational acceleration	m/s^2
h	Specific enthalpy	J/kg
k	Ratio of specific heats	
L	Length	m
m	Fractional mass flow rate	
m	Mass	kg
M	Mass flow rate	kg/s
P	Pressure	Pa (N/m^2)
q	Heat transferred	J/kg
Q	Heat	J
Q	Volume flow rate	m^3/s
R	Specific gas constant	$J/kg K$
s	Entropy	$J/kg K$
T	Temperature	K
u	Specific internal energy	J/kg
U	Overall heat transfer coefficient	$W/m^2^\circ C$ ($J/sm^2^\circ C$)
v	Specific volume	m^3/kg
V	Velocity	m/s
w	Specific work	J/kg
W	Work	J
x	Length	m
z	Elevation	m
η	Efficiency	°
θ	Nozzle angle	°
θ	Temperature difference between fluids	$^\circ C$
μ	Dynamic viscosity	Ns/m^2
ν	Kinematic viscosity	m^2/s
ρ	Density	kg/m^3
T	Thrust	N
Ω	Heat transfer rate	J/s

GENERAL CONSTANTS

Acceleration due to gravity: $g = 9.81 \text{ m/s}^2$	Specific heat of air: $c_p = 1.005 \text{ kJ/kg}^\circ\text{C}$
Atmospheric pressure: $p_{\text{atm}} = 100 \text{ kPa}$	Specific heat of air: $c_v = 0.718 \text{ kJ/kg}^\circ\text{C}$
Density of water: $\rho_{\text{water}} = 1000 \text{ kg/m}^3$	Specific heat of helium: $c_p = 5.193 \text{ kJ/kg}^\circ\text{C}$
Specific heat of water: $c_p = 4.190 \text{ kJ/kg}^\circ\text{C}$	Specific heat of helium: $c_v = 3.117 \text{ kJ/kg}^\circ\text{C}$

THERMODYNAMICS REFERENCE EQUATIONS**Basic Thermodynamics**

First Law:	$dE = \delta Q - \delta W$
Enthalpy:	$h = u + pv$
Continuity:	$\rho VA = \text{constant}$
Flow Work:	$w = \Delta(pv)$
Energy Equation:	$zg + V^2/2 + u + pv + \Delta w + \Delta q = \text{constant}$
Entropy:	$\Delta s = \Sigma \delta q / T$ (reversible conditions)

Ideal Gas Relationships

Gas Law:	$pv = RT$
Specific Heat at Constant Pressure:	$c_p = \Delta h / \Delta T$
Specific Heat at Constant Volume:	$c_v = \Delta u / \Delta T$
Gas Constant:	$R = c_p - c_v$
Specific Heat Ratio:	$k = c_p / c_v$
Isentropic Relations:	$p_1 / p_2 = (v_2 / v_1)^k = (T_1 / T_2)^{k/(k-1)}$

FLUID MECHANICS REFERENCE EQUATIONS**Fluid Mechanics**

Continuity Equation: $\rho_1 V_1 A_1 = \rho_2 V_2 A_2 = M$

Bernoulli's Equation: $p_1/\rho g + z_1 + V_1^2/2g = p_2/\rho g + z_2 + V_2^2/2g$

Momentum Equation: $F = p_1 A_1 - p_2 A_2 - \rho V A (V_2 - V_1)$ (one dimensional)

Steam Turbines

Nozzle Equation: $h_1 - h_2 = (V_2^2 - V_1^2) / 2$

Work: $w = [(V_{1\text{ absolute}}^2 - V_{2\text{ absolute}}^2) + (V_{2\text{ relative}}^2 - V_{1\text{ relative}}^2)] / 2$

Gas Turbines

State Equation: $p v = R T$

Isentropic Equation: $(T_2/T_1) = (p_2/p_1)^{(k-1)/k}$

Enthalpy Change: $h_1 - h_2 = c_p(T_1 - T_2)$ (ideal gas)

Nozzle Equation: $h_1 - h_2 = (V_2^2 - V_1^2) / 2$

Jet Propulsion

Thrust: $T = M(V_{\text{jet}} - V_{\text{aircraft}})$

Thrust Power: $T V_{\text{aircraft}} = M(V_{\text{jet}} - V_{\text{aircraft}}) V_{\text{aircraft}}$

Jet Power: $P = M(V_{\text{jet}}^2 - V_{\text{aircraft}}^2) / 2$

Propulsion Efficiency: $\eta_p = 2V_{\text{aircraft}} / (V_{\text{jet}} + V_{\text{aircraft}})$

Wind Turbine

Maximum Ideal Power: $P_{\text{max}} = 8 \rho A V_1^3 / 27$

HEAT EXCHANGER REFERENCE EQUATIONS

Heat transferred between fluids

$$\Omega = U A \theta$$

Heat gained or lost by fluids

$$\Omega = M \Delta h$$

$$\Omega = M c_p \Delta T$$

$$\Omega = \rho Q \Delta T$$

NUCLEAR REFERENCE EQUATIONS

Number of nuclei per gram of material

$$N = N_A / M$$

Number of fissile nuclei per cm³ of material

$$N_f = \gamma (N_A / M) \rho$$

Heat release rate in nuclear fuel

$$q^* = \phi N_f \sigma_f E_f$$

Nomenclature

N	=	number of nuclei (number/g)
N _A	=	Avogadro's Number
M	=	molecular weight
γ	=	fuel enrichment
ρ	=	density (g/cm ³)
q*	=	heat release rate (J/cm ³)
φ	=	neutron flux (neutrons/cm ² s)
N _f	=	number of fissile nuclei (number/cm ³)
σ _f	=	cross section (barn) (1 barn = 10 ⁻²⁴ cm ²)
E _f	=	energy release per fission of one atom

Avogadro's Number

$$N_A = 0.602 \times 10^{24} \text{ atoms/mole}$$

December 2014 - 07-Mec-B3

Thermodynamics and Heat Power

SIXTH EDITION

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TABLE A.1 (SI)
Saturation: Temperature (Steam)

Temp. °C T	Press. kPa P	Specific Volume (m ³ /kg)		Internal Energy (kJ/kg)			Enthalpy (kJ/kg)			Entropy (kJ/kg·°K)		
		Sat. Liquid v_f	Sat. Vapor v_g	Sat. Liquid u_f	Evap. u_{fg}	Sat. Vapor u_g	Sat. Liquid h_f	Evap. h_{fg}	Sat. Vapor h_g	Sat. Liquid s_f	Evap. s_{fg}	Sat. Vapor s_g
0.01	0.6113	0.001 000	206.14	.00	2375.3	2375.3	.01	2501.3	2501.4	.0000	9.1562	9.1562
5	0.8721	0.001 000	147.12	20.97	2361.3	2382.3	20.98	2489.6	2510.6	.0761	8.9496	9.0257
10	1.2276	0.001 000	106.38	42.00	2347.2	2389.2	42.01	2477.7	2519.8	.1510	8.7498	8.9008
15	1.7051	0.001 001	77.93	62.99	2333.1	2396.1	62.99	2465.9	2528.9	.2245	8.5569	8.7814
20	2.339	0.001 002	57.79	83.95	2319.0	2402.9	83.96	2454.1	2538.1	.2966	8.3706	8.6672
25	3.169	0.001 003	43.36	104.88	2304.9	2409.8	104.89	2442.3	2547.2	.3674	8.1905	8.5580
30	4.246	0.001 004	32.89	125.78	2290.8	2416.6	125.79	2430.5	2556.3	.4369	8.0164	8.4533
35	5.628	0.001 006	25.22	146.67	2276.7	2423.4	146.68	2418.6	2565.3	.5053	7.8478	8.3531
40	7.384	0.001 008	19.52	167.56	2262.6	2430.1	167.57	2406.7	2574.3	.5725	7.6845	8.2570
45	9.593	0.001 010	15.26	188.44	2248.4	2436.8	188.45	2394.8	2583.2	.6387	7.5261	8.1648
50	12.349	0.001 012	12.03	209.32	2234.2	2443.5	209.33	2382.7	2592.1	.7038	7.3725	8.0763
55	15.758	0.001 015	9.568	230.21	2219.9	2450.1	230.23	2370.7	2600.9	.7679	7.2234	7.9913
60	19.940	0.001 017	7.671	251.11	2205.5	2456.6	251.13	2358.5	2609.6	.8312	7.0784	7.9096
65	25.03	0.001 020	6.197	272.02	2191.1	2463.1	272.06	2346.2	2618.3	.8935	6.9375	7.8310
70	31.19	0.001 023	5.042	292.95	2176.6	2469.6	292.98	2333.8	2626.8	.9549	6.8004	7.7553
75	38.58	0.001 026	4.131	313.90	2162.0	2475.9	313.93	2321.4	2635.3	1.0155	6.6669	7.6824
80	47.39	0.001 029	3.407	334.86	2147.4	2482.2	334.91	2308.8	2643.7	1.0753	6.5369	7.6122
85	57.83	0.001 033	2.828	355.84	2132.6	2488.4	355.90	2296.0	2651.9	1.1343	6.4102	7.5445
90	70.14	0.001 036	2.361	376.85	2117.7	2494.5	376.92	2283.2	2660.1	1.1925	6.2866	7.4791
95	84.55	0.001 040	1.982	397.88	2102.7	2500.6	397.96	2270.2	2668.1	1.2500	6.1659	7.4159

TABLE A.1 (SI) (cont'd.)

Temp. °C T	Press. kPa P	Specific Volume (m ³ /kg)				Internal Energy (kJ/kg)				Enthalpy (kJ/kg)				Entropy (kJ/kg·°K)			
		Sat. Liquid v _f	Sat. Vapor v _g	Sat. Liquid u _f	Sat. Vapor u _g	Sat. Liquid h _f	Sat. Vapor h _g	Sat. Liquid s _f	Sat. Vapor s _g	Sat. Liquid h _f	Sat. Vapor h _g	Sat. Liquid s _f	Sat. Vapor s _g	Sat. Liquid h _f	Sat. Vapor h _g	Sat. Liquid s _f	Sat. Vapor s _g
		MPa															
100	0.101 35	0.001 044	1.6729	418.94	2087.6	2506.5	419.04	2257.0	2676.1	1.3069	6.0480	7.3549					
105	0.120 82	0.001 048	1.4194	440.02	2072.3	2512.4	440.15	2243.7	2683.8	1.3630	5.9328	7.2958					
110	0.143 27	0.001 052	1.2102	461.14	2057.0	2518.1	461.30	2230.2	2691.5	1.4185	5.8202	7.2387					
115	0.169 06	0.001 056	1.0366	482.30	2041.4	2523.7	482.48	2216.5	2699.0	1.4734	5.7100	7.1833					
120	0.198 53	0.001 060	0.8919	503.50	2025.8	2529.3	503.71	2202.6	2706.3	1.5276	5.6020	7.1296					
125	0.2321	0.001 065	0.7706	524.74	2009.9	2534.6	524.99	2188.5	2713.5	1.5813	5.4962	7.0775					
130	0.2701	0.001 070	0.6685	546.02	1993.9	2539.9	546.31	2174.2	2720.5	1.6344	5.3925	7.0269					
135	0.3130	0.001 075	0.5822	567.35	1977.7	2545.0	567.69	2159.6	2727.3	1.6870	5.2907	6.9777					
140	0.3613	0.001 080	0.5089	588.74	1961.3	2550.0	589.13	2144.7	2733.9	1.7391	5.1908	6.9299					
145	0.4154	0.001 085	0.4463	610.18	1944.7	2554.9	610.63	2129.6	2740.3	1.7907	5.0926	6.8833					
150	0.4758	0.001 091	0.3928	631.68	1927.9	2559.5	632.20	2114.3	2746.5	1.8418	4.9960	6.8379					
155	0.5431	0.001 096	0.3468	653.24	1910.8	2564.1	653.84	2098.6	2752.4	1.8925	4.9010	6.7935					
160	0.6178	0.001 102	0.3071	674.87	1893.5	2568.4	675.55	2082.6	2758.1	1.9427	4.8075	6.7502					
165	0.7005	0.001 108	0.2727	696.56	1876.0	2572.5	697.34	2066.2	2763.5	1.9925	4.7153	6.7078					
170	0.7917	0.001 114	0.2428	718.33	1858.1	2576.5	719.21	2049.5	2768.7	2.0419	4.6244	6.6663					
175	0.8920	0.001 121	0.2168	740.17	1840.0	2580.2	741.17	2032.4	2773.6	2.0909	4.5347	6.6256					
180	1.0021	0.001 127	0.194 05	762.09	1821.6	2583.7	763.22	2015.0	2778.2	2.1396	4.4461	6.5857					
185	1.1227	0.001 134	0.174 09	784.10	1802.9	2587.0	785.37	1997.1	2782.4	2.1879	4.3586	6.5465					
190	1.2544	0.001 141	0.156 54	806.19	1783.8	2590.0	807.62	1978.8	2786.4	2.2359	4.2720	6.5079					
195	1.3978	0.001 149	0.141 05	828.37	1764.4	2592.8	829.98	1960.0	2790.0	2.2835	4.1863	6.4698					
200	1.5538	0.001 157	0.127 36	850.65	1744.7	2595.3	852.45	1940.7	2793.2	2.3309	4.1014	6.4323					
205	1.7230	0.001 164	0.115 21	873.04	1724.5	2597.5	875.04	1921.0	2796.0	2.3780	4.0172	6.3952					
210	1.9062	0.001 173	0.104 41	895.53	1703.9	2599.5	897.76	1900.7	2798.5	2.4248	3.9337	6.3585					
215	2.104	0.001 181	0.094 79	918.14	1682.9	2601.1	920.62	1879.9	2800.5	2.4714	3.8507	6.3221					
220	2.318	0.001 190	0.086 19	940.87	1661.5	2602.4	943.62	1858.5	2802.1	2.5178	3.7683	6.2861					
225	2.548	0.001 199	0.078 49	963.73	1639.6	2603.3	966.78	1836.5	2803.3	2.5639	3.6863	6.2503					
230	2.795	0.001 209	0.071 58	986.74	1617.2	2603.9	990.12	1813.8	2804.0	2.6099	3.6047	6.2146					
235	3.060	0.001 219	0.065 37	1009.89	1594.2	2604.1	1013.62	1790.5	2804.2	2.6558	3.5233	6.1791					
240	3.344	0.001 229	0.059 76	1033.21	1570.8	2604.0	1037.32	1766.5	2803.8	2.7015	3.4422	6.1437					
245	3.648	0.001 240	0.054 71	1056.71	1546.7	2603.4	1061.23	1741.7	2803.0	2.7472	3.3612	6.1083					

TABLE A.1 (SI) (cont'd.)

Temp. °C <i>T</i>	Press. MPa <i>P</i>	Specific Volume (m³/kg)				Internal Energy (kJ/kg)				Enthalpy (kJ/kg)				Entropy (kJ/kg · °K)			
		Sat. Liquid <i>v_f</i>	Sat. Vapor <i>v_g</i>	Sat. Liquid <i>u_f</i>	Sat. Vapor <i>u_g</i>	Evap. <i>u_{fg}</i>	Sat. Vapor <i>u_g</i>	Sat. Liquid <i>h_f</i>	Sat. Vapor <i>h_g</i>	Evap. <i>h_{fg}</i>	Sat. Vapor <i>h_g</i>	Sat. Liquid <i>s_f</i>	Sat. Vapor <i>s_g</i>	Evap. <i>s_{fg}</i>	Sat. Vapor <i>s_g</i>		
250	3.973	0.001 251	0.050 13	1080.39	1522.0	2602.4	1085.36	2801.5	1716.2	2801.5	2.7927	3.2802	3.2802	6.0730			
255	4.319	0.001 263	0.045 98	1104.28	1496.7	2600.9	1109.73	2799.5	1689.8	2799.5	2.8383	3.1992	3.1992	6.0375			
260	4.688	0.001 276	0.042 21	1128.39	1470.6	2599.0	1134.37	2796.9	1662.5	2796.9	2.8838	3.1181	3.1181	6.0019			
265	5.081	0.001 289	0.038 77	1152.74	1443.9	2596.6	1159.28	2793.6	1634.4	2793.6	2.9294	3.0368	3.0368	5.9662			
270	5.499	0.001 302	0.035 64	1177.36	1416.3	2593.7	1184.51	2789.7	1605.2	2789.7	2.9751	2.9551	2.9551	5.9301			
275	5.942	0.001 317	0.032 79	1202.25	1387.9	2590.2	1210.07	2785.0	1574.9	2785.0	3.0208	2.8730	2.8730	5.8938			
280	6.412	0.001 332	0.030 17	1227.46	1358.7	2586.1	1235.99	2779.6	1543.6	2779.6	3.0668	2.7903	2.7903	5.8571			
285	6.909	0.001 348	0.027 77	1253.00	1328.4	2581.4	1262.31	2773.3	1511.0	2773.3	3.1130	2.7070	2.7070	5.8199			
290	7.436	0.001 366	0.025 57	1278.92	1297.1	2576.0	1289.07	2766.2	1477.1	2766.2	3.1594	2.6227	2.6227	5.7821			
295	7.993	0.001 384	0.023 54	1305.2	1264.7	2569.9	1316.3	2758.1	1441.8	2758.1	3.2062	2.5375	2.5375	5.7437			
300	8.581	0.001 404	0.021 67	1332.0	1231.0	2563.0	1344.0	2749.0	1404.9	2749.0	3.2534	2.4511	2.4511	5.7045			
305	9.202	0.001 425	0.019 948	1359.3	1195.9	2555.2	1372.4	2738.7	1366.4	2738.7	3.3010	2.3633	2.3633	5.6643			
310	9.856	0.001 447	0.018 350	1387.1	1159.4	2546.4	1401.3	2727.3	1326.0	2727.3	3.3493	2.2737	2.2737	5.6230			
315	10.547	0.001 472	0.016 867	1415.5	1121.1	2536.6	1431.0	2714.5	1283.5	2714.5	3.3982	2.1821	2.1821	5.5804			
320	11.274	0.001 499	0.015 488	1444.6	1080.9	2525.5	1461.5	2700.1	1238.6	2700.1	3.4480	2.0882	2.0882	5.5362			
330	12.845	0.001 561	0.012 996	1505.3	993.7	2498.9	1525.3	2665.9	1140.6	2665.9	3.5507	1.8909	1.8909	5.4417			
340	14.586	0.001 638	0.010 797	1570.3	894.3	2464.6	1594.2	2622.0	1027.9	2622.0	3.6594	1.6763	1.6763	5.3357			
350	16.513	0.001 740	0.008 813	1641.9	776.6	2418.4	1670.6	2563.9	893.4	2563.9	3.7777	1.4335	1.4335	5.2112			
360	18.651	0.001 893	0.006 945	1725.2	626.3	2351.5	1760.5	2481.0	720.5	2481.0	3.9147	1.1379	1.1379	5.0526			
370	21.03	0.002 213	0.004 925	1844.0	384.5	2228.5	1890.5	2332.1	441.6	2332.1	4.1106	.6865	.6865	4.7971			
374.14	22.09	0.003 155	0.003 155	2029.6	0	2029.6	2099.3	2099.3	0	2099.3	4.4298	0	0	4.4298			

TABLE A.2 (SI) (cont'd.)

Press. MPa <i>P</i>	Temp. °C <i>T</i>	Specific Volume		Internal Energy			Enthalpy			Entropy		
		Sat. Liquid <i>v_f</i>	Sat. Vapor <i>v_g</i>	Sat. Liquid <i>u_f</i>	Evap. <i>u_{fg}</i>	Sat. Vapor <i>u_g</i>	Sat. Liquid <i>h_f</i>	Evap. <i>h_{fg}</i>	Sat. Vapor <i>h_g</i>	Sat. Liquid <i>s_f</i>	Evap. <i>s_{fg}</i>	Sat. Vapor <i>s_g</i>
0.250	127.44	0.001 067	0.7187	535.10	2002.1	2537.2	535.37	2181.5	2716.9	1.6072	5.4455	7.0527
0.275	130.60	0.001 070	0.6573	548.59	1991.9	2540.5	548.89	2172.4	2721.3	1.6408	5.3801	7.0209
0.300	133.55	0.001 073	0.6058	561.15	1982.4	2543.6	561.47	2163.8	2725.3	1.6718	5.3201	6.9919
0.325	136.30	0.001 076	0.5620	572.90	1973.5	2546.4	573.25	2155.8	2729.0	1.7006	5.2646	6.9652
0.350	138.88	0.001 079	0.5243	583.95	1965.0	2548.9	584.33	2148.1	2732.4	1.7275	5.2130	6.9405
0.375	141.32	0.001 081	0.4914	594.40	1956.9	2551.3	594.81	2140.8	2735.6	1.7528	5.1647	6.9175
0.40	143.63	0.001 084	0.4625	604.31	1949.3	2553.6	604.74	2133.8	2738.6	1.7766	5.1193	6.8959
0.45	147.93	0.001 088	0.4140	622.77	1934.9	2557.6	623.25	2120.7	2743.9	1.8207	5.0359	6.8565
0.50	151.86	0.001 093	0.3749	639.68	1921.6	2561.2	640.23	2108.5	2748.7	1.8607	4.9606	6.8213
0.55	155.48	0.001 097	0.3427	655.32	1909.2	2564.5	655.93	2097.0	2753.0	1.8973	4.8920	6.7893
0.60	158.85	0.001 101	0.3157	669.90	1897.5	2567.4	670.56	2086.3	2756.8	1.9312	4.8288	6.7600
0.65	162.01	0.001 104	0.2927	683.56	1886.5	2570.1	684.28	2076.0	2760.3	1.9627	4.7703	6.7331
0.70	164.97	0.001 108	0.2729	696.44	1876.1	2572.5	697.22	2066.3	2763.5	1.9922	4.7158	6.7080
0.75	167.78	0.001 112	0.2556	708.64	1866.1	2574.7	709.47	2057.0	2766.4	2.0200	4.6647	6.6847
0.80	170.43	0.001 115	0.2404	720.22	1856.6	2576.8	721.11	2048.0	2769.1	2.0462	4.6166	6.6628
0.85	172.96	0.001 118	0.2270	731.27	1847.4	2578.7	732.22	2039.4	2771.6	2.0710	4.5711	6.6421
0.90	175.38	0.001 121	0.2150	741.83	1838.6	2580.5	742.83	2031.1	2773.9	2.0946	4.5280	6.6226
0.95	177.69	0.001 124	0.2042	751.95	1830.2	2582.1	753.02	2023.1	2776.1	2.1172	4.4869	6.6041
1.00	179.91	0.001 127	0.194 44	761.68	1822.0	2583.6	762.81	2015.3	2778.1	2.1387	4.4478	6.5865
1.10	184.09	0.001 133	0.177 53	780.09	1806.3	2586.4	781.34	2000.4	2781.7	2.1792	4.3744	6.5536
1.20	187.99	0.001 139	0.163 33	797.29	1791.5	2588.8	798.65	1986.2	2784.8	2.2166	4.3067	6.5233
1.30	191.64	0.001 144	0.151 25	813.44	1777.5	2591.0	814.93	1972.7	2787.6	2.2515	4.2438	6.4953
1.40	195.07	0.001 149	0.140 84	828.70	1764.1	2592.8	830.30	1959.7	2790.0	2.2842	4.1850	6.4693

TABLE A.2 (SI) (cont'd.)

Press. MPa <i>P</i>	Temp. °C <i>T</i>	Specific Volume (m ³ /kg)		Internal Energy (kJ/kg)			Enthalpy (kJ/kg)			Entropy (kJ/kg · °K)		
		Sat. Liquid <i>v_f</i>	Sat. Vapor <i>v_g</i>	Sat. Liquid <i>u_f</i>	Evap. <i>u_{fg}</i>	Sat. Vapor <i>u_g</i>	Sat. Liquid <i>h_f</i>	Evap. <i>h_{fg}</i>	Sat. Vapor <i>h_g</i>	Sat. Liquid <i>s_f</i>	Evap. <i>s_{fg}</i>	Sat. Vapor <i>s_g</i>
1.50	198.32	0.001 154	0.131 77	843.16	1751.3	2594.5	844.89	1947.3	2792.2	2.3150	4.1298	6.4448
1.75	205.76	0.001 166	0.113 49	876.46	1721.4	2597.8	878.50	1917.9	2796.4	2.3851	4.0044	6.3896
2.00	212.42	0.001 177	0.099 63	906.44	1693.8	2600.3	908.79	1890.7	2799.5	2.4474	3.8935	6.3409
2.25	218.45	0.001 187	0.088 75	933.83	1668.2	2602.0	936.49	1865.2	2801.7	2.5035	3.7937	6.2972
2.5	223.99	0.001 197	0.079 98	959.11	1644.0	2603.1	962.11	1841.0	2803.1	2.5547	3.7028	6.2575
3.0	233.90	0.001 217	0.066 68	1004.78	1599.3	2604.1	1008.42	1795.7	2804.2	2.6457	3.5412	6.1869
3.5	242.60	0.001 235	0.057 07	1045.43	1558.3	2603.7	1049.75	1753.7	2803.4	2.7253	3.4000	6.1253
4	250.40	0.001 252	0.049 78	1082.31	1520.0	2602.3	1087.31	1714.1	2801.4	2.7964	3.2737	6.0701
5	263.99	0.001 286	0.039 44	1147.81	1449.3	2597.1	1154.23	1640.1	2794.3	2.9202	3.0532	5.9734
6	275.64	0.001 319	0.032 44	1205.44	1384.3	2589.7	1213.35	1571.0	2784.3	3.0267	2.8625	5.8892
7	285.88	0.001 351	0.027 37	1257.55	1323.0	2580.5	1267.00	1505.1	2772.1	3.1211	2.6922	5.8133
8	295.06	0.001 384	0.023 52	1305.57	1264.2	2569.8	1316.64	1441.3	2758.0	3.2068	2.5364	5.7432
9	303.40	0.001 418	0.020 48	1350.51	1207.3	2557.8	1363.26	1378.9	2742.1	3.2858	2.3915	5.6772
10	311.06	0.001 452	0.018 026	1393.04	1151.4	2544.4	1407.56	1317.1	2724.7	3.3596	2.2544	5.6141
11	318.15	0.001 489	0.015 987	1433.7	1096.0	2529.8	1450.1	1255.5	2705.6	3.4295	2.1233	5.5527
12	324.75	0.001 527	0.014 263	1473.0	1040.7	2513.7	1491.3	1193.6	2684.9	3.4962	1.9962	5.4924
13	330.93	0.001 567	0.012 780	1511.1	985.0	2496.1	1531.5	1130.7	2662.2	3.5606	1.8718	5.4323
14	336.75	0.001 611	0.011 485	1548.6	928.2	2476.8	1571.1	1066.5	2637.6	3.6232	1.7485	5.3717
15	342.24	0.001 658	0.010 337	1585.6	869.8	2455.5	1610.5	1000.0	2610.5	3.6848	1.6249	5.3098
16	347.44	0.001 711	0.009 306	1622.7	809.0	2431.7	1650.1	930.6	2580.6	3.7461	1.4994	5.2455
17	352.37	0.001 770	0.008 364	1660.2	744.8	2405.0	1690.3	856.9	2547.2	3.8079	1.3698	5.1777
18	357.06	0.001 840	0.007 489	1698.9	675.4	2374.3	1732.0	777.1	2509.1	3.8715	1.2329	5.1044
19	361.54	0.001 924	0.006 657	1739.9	598.1	2338.1	1776.5	688.0	2469.5	3.9388	1.0839	5.0228
20	365.81	0.002 036	0.005 834	1785.6	507.5	2293.0	1826.3	583.4	2403.7	4.0139	.9130	4.9269
21	369.89	0.002 207	0.004 952	1842.1	388.5	2230.6	1888.4	446.2	2334.6	4.1075	.6938	4.8013
22	373.80	0.002 742	0.003 568	1961.9	125.2	2087.1	2022.2	143.4	2165.6	4.3110	.2216	4.5327
22.09	374.14	0.003 155	0.003 155	2029.6	0	2029.6	2099.3	0	2099.3	4.4298	0	4.4298

TABLE A.3 (SI)
Properties of Superheated Steam

T	P = .010 MPa (45.81)					P = .050 MPa (81.33)					P = .10 MPa (99.63)					
	v	u	h	s	v	u	h	s	v	u	h	s	v	u	h	s
Sat.	14.674	2437.9	2584.7	8.1502	3.240	2483.9	2645.9	7.5939	1.6940	2506.1	2675.5	7.3594	1.6940	2506.1	2675.5	7.3594
50	14.869	2443.9	2592.6	8.1749	3.418	2511.6	2682.5	7.6947	1.6958	2506.7	2676.2	7.3614	1.6958	2506.7	2676.2	7.3614
100	17.196	2515.5	2687.5	8.4479	3.889	2585.6	2780.1	7.9401	1.9364	2582.8	2776.4	7.6134	1.9364	2582.8	2776.4	7.6134
150	19.512	2587.9	2783.0	8.6882	4.356	2659.9	2877.7	8.1580	2.172	2658.1	2875.3	7.8343	2.172	2658.1	2875.3	7.8343
200	21.825	2661.3	2879.5	8.9038	4.820	2735.0	2976.0	8.3556	2.406	2733.7	2974.3	8.0333	2.406	2733.7	2974.3	8.0333
250	24.136	2736.0	2977.3	9.1002	5.284	2811.3	3075.5	8.5373	2.639	2810.4	3074.3	8.2158	2.639	2810.4	3074.3	8.2158
300	26.445	2812.1	3076.5	9.2813	6.209	2968.5	3278.9	8.8642	3.103	2967.9	3278.2	8.5435	3.103	2967.9	3278.2	8.5435
400	31.063	2968.9	3279.6	9.6077	7.134	3132.0	3488.7	9.1546	3.565	3131.6	3488.1	8.8342	3.565	3131.6	3488.1	8.8342
500	35.679	3132.3	3489.1	9.8978	8.057	3302.2	3705.1	9.4178	4.028	3301.9	3704.7	9.0976	4.028	3301.9	3704.7	9.0976
600	40.295	3302.5	3705.4	10.1608	8.981	3479.4	3928.5	9.6599	4.490	3479.2	3928.2	9.3398	4.490	3479.2	3928.2	9.3398
700	44.911	3479.6	3928.7	10.4028	9.904	3663.6	4158.9	9.8852	4.952	3663.5	4158.6	9.5652	4.952	3663.5	4158.6	9.5652
800	49.526	3663.8	4159.0	10.6281	10.828	3854.9	4396.3	10.0967	5.414	3854.8	4396.1	9.7767	5.414	3854.8	4396.1	9.7767
900	54.141	3855.0	4396.4	10.8396	11.751	4052.9	4640.5	10.2964	5.875	4052.8	4640.3	9.9764	5.875	4052.8	4640.3	9.9764
1000	58.757	4053.0	4640.6	11.0393	12.674	4257.4	4891.1	10.4859	6.337	4257.3	4891.0	10.1659	6.337	4257.3	4891.0	10.1659
1100	63.372	4257.5	4891.2	11.2287	13.597	4467.8	5147.7	10.6662	6.799	4467.7	5147.6	10.3463	6.799	4467.7	5147.6	10.3463
1200	67.987	4467.9	5147.8	11.4091	14.521	4683.6	5409.6	10.8382	7.260	4683.5	5409.5	10.5183	7.260	4683.5	5409.5	10.5183
1300	72.602	4683.7	5409.7	11.5811												
P = .20 MPa (120.23)																
Sat.	.8857	2529.5	2706.7	7.1272	.6058	2543.6	2725.3	6.9919	.4625	2553.6	2738.6	6.8959	.4625	2553.6	2738.6	6.8959
150	.9596	2576.9	2768.8	7.2795	.6339	2570.8	2761.0	7.0778	.4708	2564.5	2752.8	6.9299	.4708	2564.5	2752.8	6.9299
200	1.0803	2654.4	2870.5	7.5066	.7163	2650.7	2865.6	7.3115	.5342	2646.8	2860.5	7.1706	.5342	2646.8	2860.5	7.1706
250	1.1988	2731.2	2971.0	7.7086	.7964	2728.7	2967.6	7.5166	.5951	2726.1	2964.2	7.3789	.5951	2726.1	2964.2	7.3789
300	1.3162	2808.6	3071.8	7.8926	.8753	2806.7	3069.3	7.7022	.6548	2804.8	3066.8	7.5662	.6548	2804.8	3066.8	7.5662
400	1.5493	2966.7	3276.6	8.2218	1.0315	2965.6	3275.0	8.0330	.7726	2964.4	3273.4	7.8985	.7726	2964.4	3273.4	7.8985
P = .40 MPa (143.63)																

TABLE 4

<i>p</i> (t Sat.) MPa		Liquid											
		0			2.5 (223.99)			5.0 (263.99)					
<i>t</i>	$10^3 v$	<i>u</i>	<i>h</i>	<i>s</i>	$10^3 v$	<i>u</i>	<i>h</i>	<i>s</i>	$10^3 v$	<i>u</i>	<i>h</i>	<i>s</i>	
Sat.													
0	1.0002	-0.03	-0.03	-0.0001	0.9990	-0.00	2.50	-0.0000	0.9977	0.04	5.04	0.0001	
20	1.0018	83.95	83.95	0.2966	1.0006	83.80	86.30	0.2961	0.9995	83.65	88.65	0.2956	
40	1.0078	167.56	167.56	0.5725	1.0067	167.25	169.77	0.5715	1.0056	166.95	171.97	0.5705	
60	1.0172	251.12	251.12	0.8312	1.0160	250.67	253.21	0.8298	1.0149	250.23	255.30	0.8285	
80	1.1291	334.87	334.87	1.0753	1.0280	334.29	336.86	1.0737	1.0268	333.72	338.85	1.0720	
100	1.0436	418.96	418.96	1.3069	1.0423	418.24	420.85	1.3050	1.0410	417.52	422.72	1.3030	
120	1.0604	503.57	503.57	1.5278	1.0590	502.68	505.33	1.5255	1.0576	501.80	507.09	1.5233	
140	1.0800	588.89	588.89	1.7395	1.0784	587.82	590.52	1.7369	1.0768	586.76	592.15	1.7343	
160	1.1024	675.19	675.19	1.9434	1.1006	673.90	676.65	1.9404	1.0988	672.62	678.12	1.9375	
180	1.1283	762.72	762.72	2.1410	1.1261	761.16	763.97	2.1375	1.1240	759.63	765.25	2.1341	
200	1.1581	851.8	851.8	2.3334	1.1555	849.9	852.8	2.3294	1.1530	848.1	853.9	2.3255	
210	1.1749	897.1	897.1	2.4281	1.1720	895.0	898.0	2.4238	1.1691	893.0	898.8	2.4195	
220	1.1930	943.0	943.0	2.5221	1.1898	940.7	943.7	2.5174	1.1866	938.4	944.4	2.5128	
230	1.2129	989.6	989.6	2.6157	1.2092	987.0	990.1	2.6105	1.2056	984.5	990.6	2.6055	
240	1.2347	1037.1	1037.1	2.7091	1.2305	1034.2	1037.2	2.7034	1.2264	1031.4	1037.5	2.6979	
250	1.2590	1085.6	1085.6	2.8027	1.2540	1082.3	1085.4	2.7964	1.2493	1079.1	1085.3	2.7902	
260	1.2862	1135.4	1135.4	2.8970	1.2804	1131.6	1134.8	2.8898	1.2749	1127.9	1134.3	2.8830	
270	1.3173	1186.8	1186.8	2.9926	1.3102	1182.4	1185.7	2.9844	1.3036	1178.2	1184.3	2.9766	
280	1.3535	1240.4	1240.4	3.0904	1.3447	1235.1	1238.5	3.0808	1.3365	1230.2	1236.8	3.0717	
290	1.3971	1297.0	1297.0	3.1918	1.3855	1290.5	1294.0	3.1801	1.3750	1284.4	1291.3	3.1693	
300	1.4520	1358.1	1358.1	3.2992	1.4357	1349.6	1353.2	3.2843	1.4214	1341.9	1349.0	3.2708	
310					1.4803	1404.1	1411.5					3.3789	

FIGURE 5.11a Extract from subcooled table (SI units).

TABLE A.4 (SI)
Properties of Compressed Liquid (Steam)

T	P = 5 MPa (263.99)					P = 10 MPa (311.06)					P = 15 MPa (342.24)				
	v	u	h	s		v	u	h	s		v	u	h	s	
Sat.	.001 285 9	1147.8	1154.2	2.9202		.001 452 4	1393.0	1407.6	3.3596		.001 658 1	1585.6	1610.5	3.6848	
0	.000 997 7	.04	5.04	.0001		.000 995 2	.09	10.04	.0002		.000 992 8	.15	15.05	.0004	
20	.000 999 5	83.65	88.65	.2956		.000 997 2	83.36	93.33	.2945		.000 995 0	83.06	97.99	.2934	
40	.001 005 6	166.95	171.97	.5705		.001 003 4	166.35	176.38	.5686		.001 001 3	165.76	180.78	.5666	
60	.001 014 9	250.23	255.30	.8285		.001 012 7	249.36	259.49	.8258		.001 010 5	248.51	263.67	.8232	
80	.001 026 8	333.72	338.85	1.0720		.001 024 5	332.59	342.83	1.0688		.001 022 2	331.48	346.81	1.0656	
100	.001 041 0	417.52	422.72	1.3030		.001 038 5	416.12	426.50	1.2992		.001 036 1	414.74	430.28	1.2955	
120	.001 057 6	501.80	507.09	1.5233		.001 054 9	500.08	510.64	1.5189		.001 052 2	498.40	514.19	1.5145	
140	.001 076 8	586.76	592.15	1.7343		.001 073 7	584.68	595.42	1.7292		.001 070 7	582.66	598.72	1.7242	
160	.001 098 8	672.62	678.12	1.9375		.001 095 3	670.13	681.08	1.9317		.001 091 8	667.71	684.09	1.9260	
180	.001 124 0	759.63	765.25	2.1341		.001 119 9	756.65	767.84	2.1275		.001 115 9	753.76	770.50	2.1210	
200	.001 153 0	848.1	853.9	2.3255		.001 148 0	844.5	856.0	2.3178		.001 143 3	841.0	858.2	2.3104	
220	.001 186 6	938.4	944.4	2.5128		.001 180 5	934.1	945.9	2.5039		.001 174 8	929.9	947.5	2.4953	
240	.001 226 4	1031.4	1037.5	2.6979		.001 218 7	1026.0	1038.1	2.6872		.001 211 4	1020.8	1039.0	2.6771	
260	.001 274 9	1127.9	1134.3	2.8830		.001 264 5	1121.1	1133.7	2.8699		.001 255 0	1114.6	1133.4	2.8576	
280						.001 321 6	1220.9	1234.1	3.0548		.001 308 4	1212.5	1232.1	3.0393	
300						.001 397 2	1328.4	1342.3	3.2469		.001 377 0	1316.6	1337.3	3.2260	
320											.001 472 4	1431.1	1453.2	3.4247	
340											.001 631 1	1567.5	1591.9	3.6546	

TABLE A.4 (SI) (cont'd.)

T	P = 20 MPa (365.81)					P = 30 MPa					P = 50 MPa				
	v	u	h	s		v	u	h	s		v	u	h	s	
Sat.	.002 036	1785.6	1826.3	4.0139		.000 985 6	.25	29.82	.0001		.000 976 6	.20	49.03	.0014	
0	.000 990 4	.19	20.01	.0004		.000 988 6	82.17	111.84	.2899		.000 980 4	81.00	130.02	.2848	
20	.000 992 8	82.77	102.62	.2923		.000 995 1	164.04	193.89	.5607		.000 987 2	161.86	211.21	.5527	
40	.000 999 2	165.17	185.16	.5646		.001 004 2	246.06	276.19	.8154		.000 996 2	242.98	292.79	.8052	
60	.001 008 4	247.68	267.85	.8206		.001 015 6	328.30	358.77	1.0561		.001 007 3	324.34	374.70	1.0440	
80	.001 019 9	330.40	350.80	1.0624		.001 029 0	410.78	441.66	1.2844		.001 020 1	405.88	456.89	1.2703	
100	.001 033 7	413.39	434.06	1.2917		.001 044 5	493.59	524.93	1.5018		.001 034 8	487.65	539.39	1.4857	
120	.001 049 6	496.76	517.76	1.5102		.001 062 1	576.88	608.75	1.7098		.001 051 5	569.77	622.35	1.6915	
140	.001 067 8	580.69	602.04	1.7193		.001 082 1	660.82	693.28	1.9096		.001 070 3	652.41	705.92	1.8891	
160	.001 088 5	665.35	687.12	1.9204		.001 104 7	745.59	778.73	2.1024		.001 091 2	735.69	790.25	2.0794	
180	.001 112 0	750.95	773.20	2.1147		.001 130 2	831.4	865.3	2.2893		.001 114 6	819.7	875.5	2.2634	
200	.001 138 8	837.7	860.5	2.3031		.001 159 0	918.3	953.1	2.4711		.001 140 8	904.7	961.7	2.4419	
220	.001 169 3	925.9	949.3	2.4870		.001 192 0	1006.9	1042.6	2.6490		.001 170 2	990.7	1049.2	2.6158	
240	.001 204 6	1016.0	1040.0	2.6674		.001 230 3	1097.4	1134.3	2.8243		.001 203 4	1078.1	1138.2	2.7860	
260	.001 246 2	1108.6	1133.5	2.8459		.001 275 5	1190.7	1229.0	2.9986		.001 241 5	1167.2	1229.3	2.9537	
280	.001 296 5	1204.7	1230.6	3.0248		.001 330 4	1287.9	1327.8	3.1741		.001 286 0	1258.7	1323.0	3.1200	
300	.001 359 6	1306.1	1333.3	3.2071		.001 399 7	1390.7	1432.7	3.3539		.001 338 8	1353.3	1420.2	3.2868	
320	.001 443 7	1415.7	1444.6	3.3979		.001 492 0	1501.7	1546.5	3.5426		.001 403 2	1452.0	1522.1	3.4557	
340	.001 568 4	1539.7	1571.0	3.6075		.001 626 5	1626.6	1675.4	3.7494		.001 483 8	1556.0	1630.2	3.6291	
360	.001 822 6	1702.8	1739.3	3.8772		.001 869 1	1781.4	1837.5	4.0012		.001 588 4	1667.2	1746.6	3.8101	
380															