

16-CHEM-A3, HEAT and MASS TRANSFER

MAY 2017

Three Hours Duration

NOTES:

- 1) If doubt exists as to the interpretation of any question, you are urged to submit a clear statement of any assumptions made along with the answer paper.
- 2) Property data required to solve a given problem are provided in the problem statement or are available in the recommended texts. If you are unable to locate the required data, do not let this prevent you from solving the rest of the problem. Even in the absence of property data, you still have the opportunity to provide a solution methodology.
- 3) This is an **open-book exam**. One textbook of your choice with notations listed on the margins etc., but no loose notes are permitted into the exam. Candidates may use any **non-communicating** scientific calculator.
- 4) All problems are worth **25 points**. At least **two problems** from **each part** must be attempted.
- 5) **Only the first two** questions as they appear in the answer book from each section will be marked.

PART A – HEAT TRANSFER

- 1) A 1 meter pipeline of 25 mm outside diameter is to be thermally insulated with a material whose thermal conductivity (k) is 0.25 W/m.K. Heat transfer coefficient from the pipe to the surroundings is 12 W/m².K.
- (a) [4 points] Check whether the insulation would be effective or not.
- (b) [4 points] What should be the maximum value of k for the insulating material to effectively reduce the heat transfer?
- (c) [17 points] Find the thickness of insulation if an alternative material with $k = 0.04$ W/m.K is used and it is desired to reduce the heat transfer to 20.7% of that of bare pipe.
- 2) Air at a flow rate of 18 kg/hr is heated from 40°C to 360°C in a heat exchanger by passing it through a 10 cm diameter pipe packed with 6.45 mm long cubes. The pipe surface is maintained at 400°C. Determine the length of packed bed pipe required to perform this operation.

- 3) Water at a mean temperature of 40°C and a mean velocity of 10 cm/s flows inside a 1 meter long thin-walled copper tube (ID = 2.5 cm, $k = 380$ W/m.K). The outside surface of the tube dissipates heat to the atmosphere air at 20°C by free convection. The following simplified expression can be used for air to determine heat transfer coefficient by free convection (h_a):

$$h_a = 1.32 \{(T_s - T_a)/D\}^{0.25}$$

where $T_s \rightarrow$ Mean temperature of the outer surface of copper tube
 $T_a \rightarrow$ Temperature of air
 $D \rightarrow$ Diameter of copper tube

- (a) [4 points] Calculate the overall heat transfer coefficient.
(b) [7 points] Calculate the mean temperature of the tube wall.
(c) [3 points] Calculate the heat loss.

We desire to increase the value of the overall heat transfer coefficient by introducing 8 rectangular radial fins (2 mm thick and 20 mm height), each with an adiabatic tip. The fins are made of the same copper material as the tube.

- (d) [8 points] Calculate the overall heat transfer coefficient.
(e) [3 points] Calculate the rate of heat transfer.

DATA: Density of water = 965.3 kg/m³
 Thermal conductivity of water = 0.675 W/m°C
 Viscosity of water = 3.15 x 10⁻⁴ kg/m.s

PART B – MASS TRANSFER

- 1) It is desired to separate a feed mixture containing 40% heptane and 60% ethyl benzene, such that 60% of the feed is distilled out. The equilibrium data for mole fraction of heptane in the liquid and vapor phase is given below:

Liquid Mole Fraction (x)	Vapor Mole Fraction (y)
0.000	0.000
0.080	0.233
0.185	0.428
0.251	0.514
0.335	0.608
0.489	0.729
0.651	0.814
0.790	0.910
0.914	0.963
1.000	1.000

Estimate the composition of the residue and distillate for the following process:

- (a) [10 points] Equilibrium distillation.
(b) [15 points] Differential distillation.

- 2) For flow of a fluid at right angle to a circular cylinder, the average Sherwood number (averaged around the periphery of the cylinder) can be written as a function of Reynolds and Schmidt numbers by the following equation:

$$\mathbf{Sh_{av} = 0.43 + 0.532 Re^{0.5} Sc^{0.31}} \quad \text{for } 1 \leq Re \leq 4000$$

A 10-cm long, 1-cm diameter cylinder of uranium hexafluoride (UF_6) is exposed to an airstream that flows normal to the cylinder axis at a velocity of 1 m/s. The surface temperature of the solid is 303 K, at which the vapor pressure of UF_6 is 27 kPa. The bulk air is at 1 atm and 325 K. Estimate the rate of sublimation of the cylinder.

DATA: Binary diffusivity of UF_6 -air gas mixture = $9.04 \times 10^{-2} \text{ cm}^2/\text{s}$
Viscosity of UF_6 -air gas mixture = $2.29 \times 10^{-5} \text{ kg/m.s}$

- 3) Nitrogen dioxide is to be removed from a dilute mixture with air by adsorption on silica gel in a continuous adsorber at 298 K and 1 atm. The gas mixture, containing 1.5% NO_2 by volume, enters the adsorber at a rate of 0.50 kg/s. The silica gel entering the adsorber is free of NO_2 . The equilibrium adsorption data at 298 K is given below:

Partial Pressure of NO_2 (in mmHg)	Solid Concentration (in kg NO_2 /kg gel)
2	0.40
4	0.90
6	1.65
8	2.60
10	3.65
12	4.85

If twice the minimum gel rate is used and 85% of NO_2 is to be removed in the adsorber, calculate the following:

- (c) [15 points] Mass flow rate and composition of the gel leaving the process for countercurrent contact between the gas mixture and the silica gel.
- (d) [10 points] Mass flow rate and composition of the gel leaving the process for cocurrent contact between the gas mixture and the silica gel.

TABLE A-9

Properties of air at 1 atm pressure

Temp. $T, ^\circ\text{C}$	Density $\rho, \text{kg/m}^3$	Specific Heat c_p $\text{J/kg}\cdot\text{K}$	Thermal Conductivity $k, \text{W/m}\cdot\text{K}$	Thermal Diffusivity $\alpha, \text{m}^2/\text{s}$	Dynamic Viscosity $\mu, \text{kg/m}\cdot\text{s}$	Kinematic Viscosity $\nu, \text{m}^2/\text{s}$	Prandtl Number Pr
-150	2.866	983	0.01171	4.158×10^{-6}	8.636×10^{-6}	3.013×10^{-6}	0.7246
-100	2.038	966	0.01582	8.036×10^{-6}	1.189×10^{-5}	5.837×10^{-6}	0.7263
-50	1.582	999	0.01979	1.252×10^{-5}	1.474×10^{-5}	9.319×10^{-6}	0.7440
-40	1.514	1002	0.02057	1.356×10^{-5}	1.527×10^{-5}	1.008×10^{-5}	0.7436
-30	1.451	1004	0.02134	1.465×10^{-5}	1.579×10^{-5}	1.087×10^{-5}	0.7425
-20	1.394	1005	0.02211	1.578×10^{-5}	1.630×10^{-5}	1.169×10^{-5}	0.7408
-10	1.341	1006	0.02288	1.696×10^{-5}	1.680×10^{-5}	1.252×10^{-5}	0.7387
0	1.292	1006	0.02364	1.818×10^{-5}	1.729×10^{-5}	1.338×10^{-5}	0.7362
5	1.269	1006	0.02401	1.880×10^{-5}	1.754×10^{-5}	1.382×10^{-5}	0.7350
10	1.246	1006	0.02439	1.944×10^{-5}	1.778×10^{-5}	1.426×10^{-5}	0.7336
15	1.225	1007	0.02476	2.009×10^{-5}	1.802×10^{-5}	1.470×10^{-5}	0.7323
20	1.204	1007	0.02514	2.074×10^{-5}	1.825×10^{-5}	1.516×10^{-5}	0.7309
25	1.184	1007	0.02551	2.141×10^{-5}	1.849×10^{-5}	1.562×10^{-5}	0.7296
30	1.164	1007	0.02588	2.208×10^{-5}	1.872×10^{-5}	1.608×10^{-5}	0.7282
35	1.145	1007	0.02625	2.277×10^{-5}	1.895×10^{-5}	1.655×10^{-5}	0.7268
40	1.127	1007	0.02662	2.346×10^{-5}	1.918×10^{-5}	1.702×10^{-5}	0.7255
45	1.109	1007	0.02699	2.416×10^{-5}	1.941×10^{-5}	1.750×10^{-5}	0.7241
50	1.092	1007	0.02735	2.487×10^{-5}	1.963×10^{-5}	1.798×10^{-5}	0.7228
60	1.059	1007	0.02808	2.632×10^{-5}	2.008×10^{-5}	1.896×10^{-5}	0.7202
70	1.028	1007	0.02881	2.780×10^{-5}	2.052×10^{-5}	1.995×10^{-5}	0.7177
80	0.9994	1008	0.02953	2.931×10^{-5}	2.096×10^{-5}	2.097×10^{-5}	0.7154
90	0.9718	1008	0.03024	3.086×10^{-5}	2.139×10^{-5}	2.201×10^{-5}	0.7132
100	0.9458	1009	0.03095	3.243×10^{-5}	2.181×10^{-5}	2.306×10^{-5}	0.7111
120	0.8977	1011	0.03235	3.565×10^{-5}	2.264×10^{-5}	2.522×10^{-5}	0.7073
140	0.8542	1013	0.03374	3.898×10^{-5}	2.345×10^{-5}	2.745×10^{-5}	0.7041
160	0.8148	1016	0.03511	4.241×10^{-5}	2.420×10^{-5}	2.975×10^{-5}	0.7014
180	0.7788	1019	0.03646	4.593×10^{-5}	2.504×10^{-5}	3.212×10^{-5}	0.6992
200	0.7459	1023	0.03779	4.954×10^{-5}	2.577×10^{-5}	3.455×10^{-5}	0.6974
250	0.6746	1033	0.04104	5.890×10^{-5}	2.760×10^{-5}	4.091×10^{-5}	0.6946
300	0.6158	1044	0.04418	6.871×10^{-5}	2.934×10^{-5}	4.765×10^{-5}	0.6935
350	0.5664	1056	0.04721	7.892×10^{-5}	3.101×10^{-5}	5.475×10^{-5}	0.6937
400	0.5243	1069	0.05015	8.951×10^{-5}	3.261×10^{-5}	6.219×10^{-5}	0.6948
450	0.4880	1081	0.05298	1.004×10^{-4}	3.415×10^{-5}	6.997×10^{-5}	0.6965
500	0.4565	1093	0.05572	1.117×10^{-4}	3.563×10^{-5}	7.806×10^{-5}	0.6986
600	0.4042	1115	0.06093	1.352×10^{-4}	3.846×10^{-5}	9.515×10^{-5}	0.7037
700	0.3627	1135	0.06581	1.598×10^{-4}	4.111×10^{-5}	1.133×10^{-4}	0.7092
800	0.3289	1153	0.07037	1.855×10^{-4}	4.362×10^{-5}	1.326×10^{-4}	0.7149
900	0.3008	1169	0.07465	2.122×10^{-4}	4.600×10^{-5}	1.529×10^{-4}	0.7206
1000	0.2772	1184	0.07868	2.398×10^{-4}	4.826×10^{-5}	1.741×10^{-4}	0.7260
1500	0.1990	1234	0.09599	3.908×10^{-4}	5.817×10^{-5}	2.922×10^{-4}	0.7478
2000	0.1553	1264	0.11113	5.664×10^{-4}	6.630×10^{-5}	4.270×10^{-4}	0.7539

Note: For ideal gases, the properties c_p , k , μ , and Pr are independent of pressure. The properties ρ , ν , and α at a pressure P (in atm) other than 1 atm are determined by multiplying the values of ρ at the given temperature by P and by dividing ν and α by P .

Source: Data generated from the EES software developed by S. A. Klein and F. L. Alvarado. Original sources: Keenan, Chao, Keyes, Gas Tables, Wiley, 198; and Thermophysical Properties of Matter, Vol. 3: Thermal Conductivity, Y. S. Touloukian, P. E. Liley, S. C. Saxena, Vol. 11: Viscosity, Y. S. Touloukian, S. C. Saxena, and P. Hestermans, IFI/Plenum, NY, 1970, ISBN 0-306067020-8.









